



CONJUGATE FLUID FLOW/ SOLID HEAT TRANSFER SIMULATIONS OF THE FLAME DEFLECTOR THERMAL ENVIRONMENT

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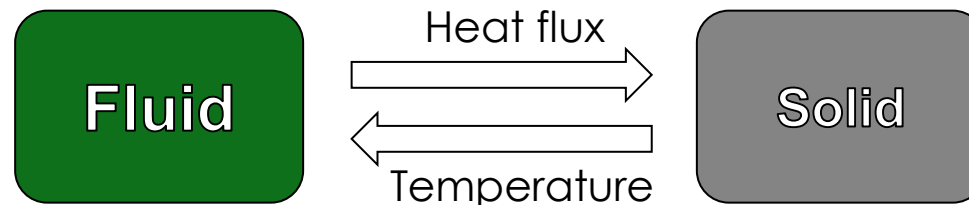
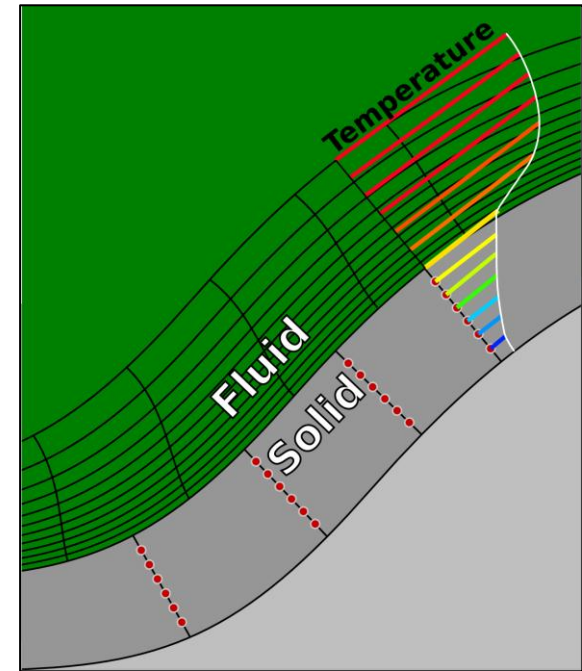
- Main Flame Deflector (MFD) re-directs the plume
 - Direct plume impingement → harsh stress and thermal loads
 - Coated with the Fondu-Fyre refractory material
- Shuttle era design required frequent and costly repairs:
 - Average cost of repair, per launch, is roughly **\$500K*** (for MFD only)
 - **2-3 weeks** of repair time
- MFD re-design for the new launch complex:
 - Compatibility with Space Launch System (SLS) and **commercial** launch vehicles

- Guide MFD re-design with CFD
 - Fast simulation turn-around time
 - Support fast-paced design iterations
 - Reasonably accurate, time-dependent predictions of
 - Pressure loading
 - Heat flux
- Traditional CFD analysis of wall heat flux
 - Isothermal wall assumption
 - Vast over-prediction (with hot plume impinging on cold wall)
 - Adiabatic wall + post analysis with empirical correlations
 - Dubious predictions for complicated flows
 - Lack of time-dependent response of the surface temperature
 - Thus, CFD thermal analysis of MFD was not used



- LAVA CFD code introduced **conjugate** simulations:
 - Tightly coupled fluid flow & surface material heat transfer
 - Predictive capability for MFD thermal environment
- Developed by the authors at NASA ARC
- High performance oriented
- Handles Cartesian, arbitrary polyhedral unstructured & curvilinear meshes
 - Hybrid meshes are possible via an overset coupling
 - Adaptive mesh refinement for Cartesian meshes
- 2nd order spatial and temporal accuracy
- SST, SA and SA-DES turbulence models

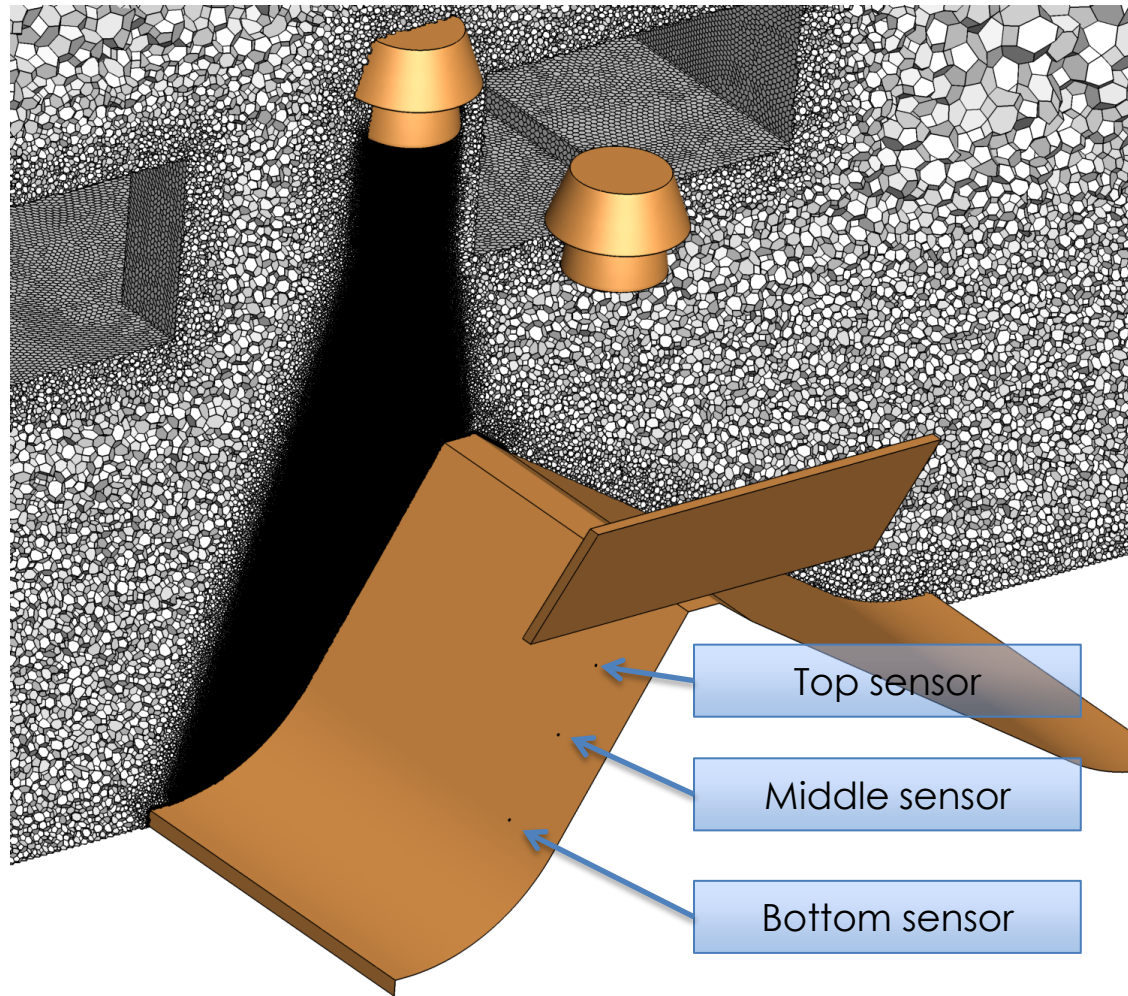
- Fluid domain:
 - Arbitrary polyhedral unstructured mesh
 - Polygonal prism boundary layer mesh
 - 3D Navier-Stokes equations
- Solid domain:
 - 1D, unsteady heat conduction equation
 - Along rays for each fluid mesh face on the surface
 - Solid back assumed insulated
- Coupling:
 - Two-way information exchange at each iteration





- MFD pressure and heat flux measured during launches
 - STS-133-134-135
 - 3 locations instrumented with COTS sensors which feature
 - Kulite – High speed pressure
 - Medtherm – Heat flux
 - Nanmac – Heat flux
 - Sensors were embedded in stainless steel encasing





21 million polyhedral unstructured elements

Orbiter, external tank were omitted

Only nozzles of SRB's included

Time step of 3.5×10^{-5} seconds

20 sub-iterations each time step

Prismatic boundary layer mesh ($y^+ < 1$)



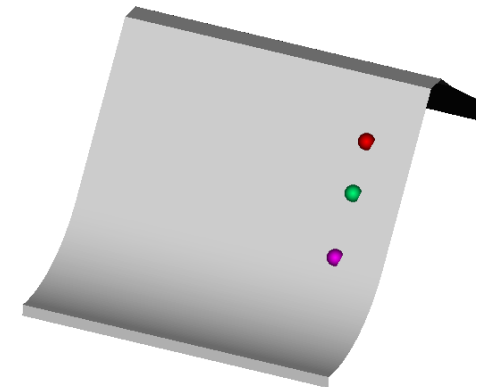
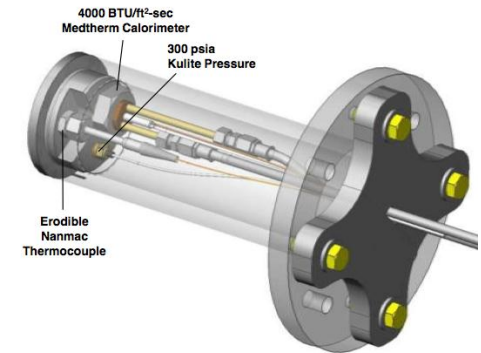
- SA-DES turbulence model
- Unsteady SRB plenum data was used from STS-1
 - Likely inconsistencies with STS-135 (current case)
- Non-reacting, single species plume exhaust gas
 - Not expected to affect impingement heating
- Water sound suppression system is neglected
 - Not expected to affect impingement heating
 - Affects wave propagation speed
- These assumptions all contribute to **temporal error**
- Solid particles from SRB's omitted
- MFD surface irregularities neglected
- No MFD refractory material recession and surface reactions
- Solid heat transfer is modeled as 1-dimensional

- MFD surface material (Fondu Fyre) properties:

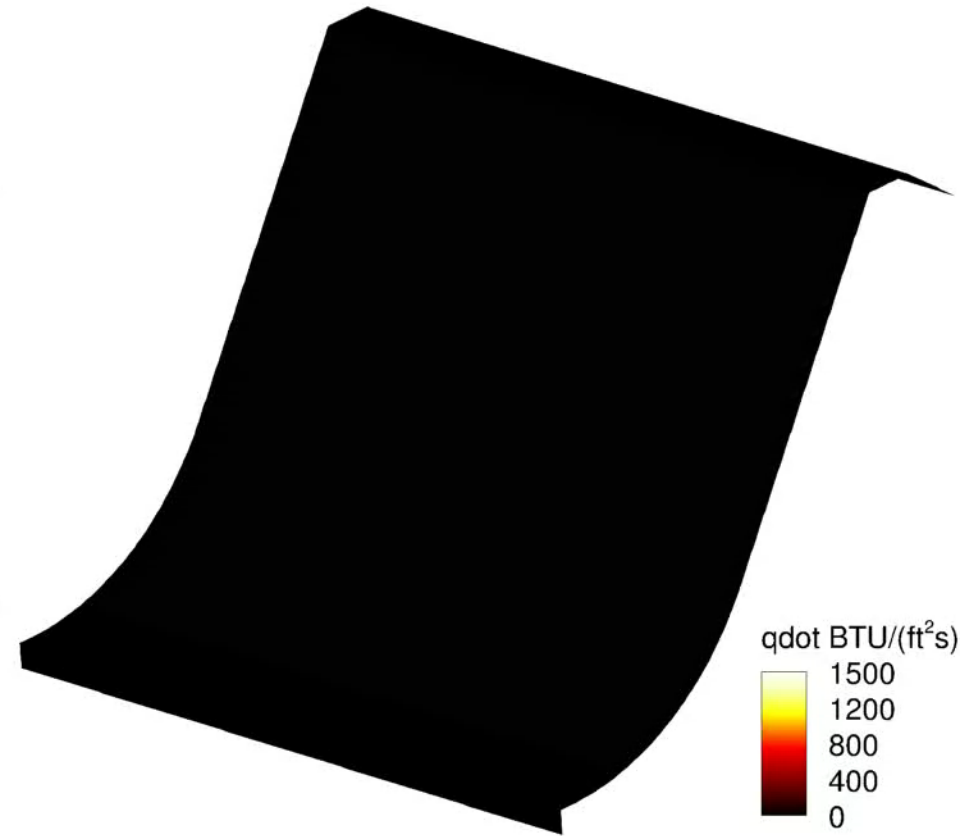
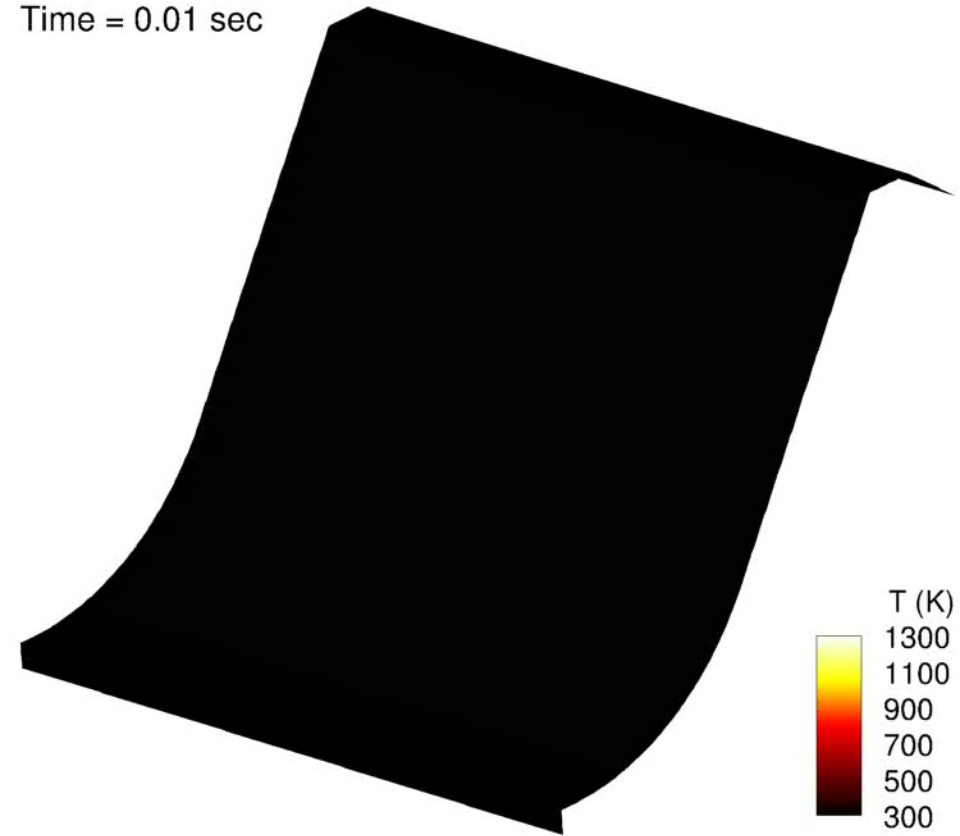
Thickness	6 in
Density	2000 kg/m ³
Specific Heat	Temperature dependent*
Melting Temperature	1373 K
Thermal Conductivity	1 W/(m.K)

- Sensors are embedded in stainless steel structures
- Encasing is modeled as 3.5" diameter discs
- Sensor encasing material (stainless steel) properties:

Thickness	1 in
Density	8030 kg/m ³
Specific Heat	500 J/(kg.K)
Melting Temperature	1700 K
Thermal Conductivity	21.4 W/(m.K)

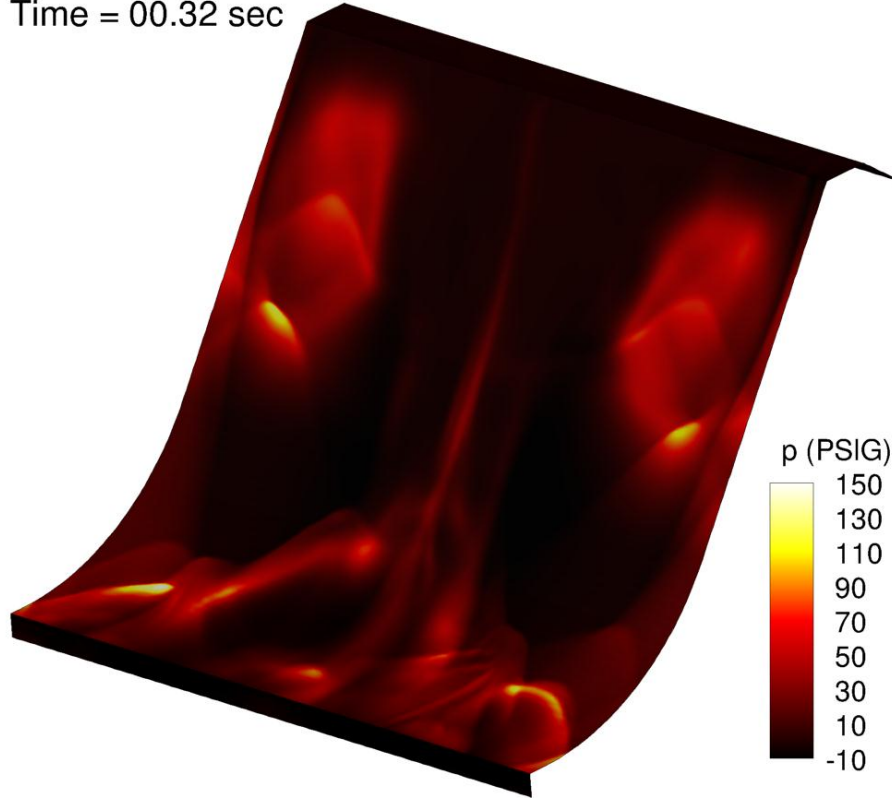


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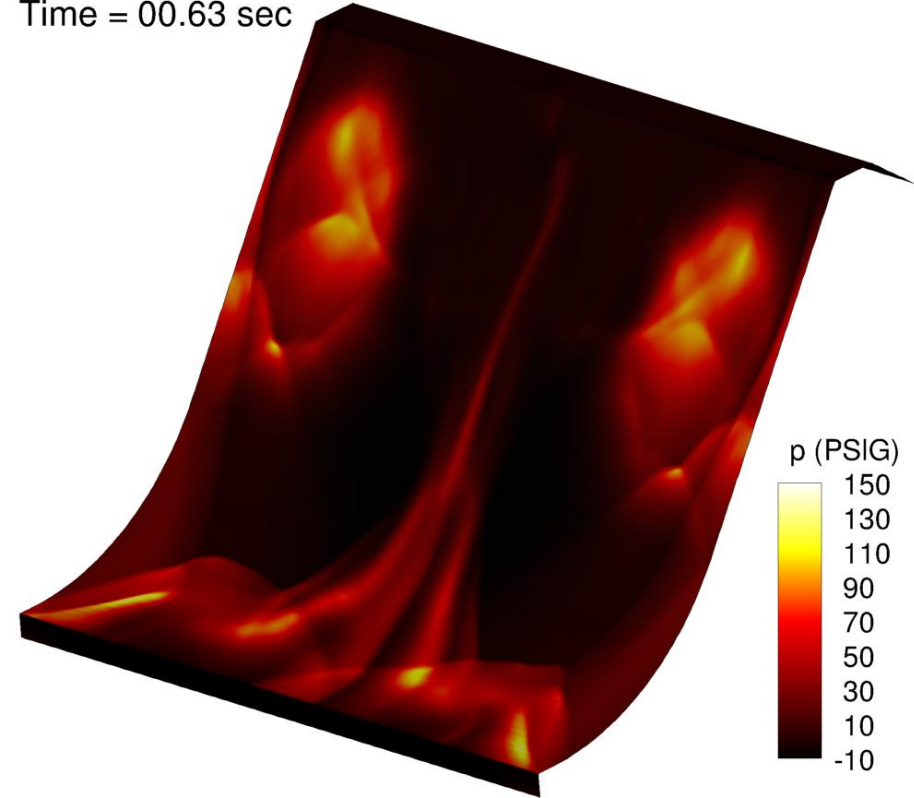


- Instantaneous pressure distribution over MFD
 - High pressure regions at the primary and secondary impingement locations
 - Near quasi-steady conditions reached around 0.6 sec

Time = 00.32 sec

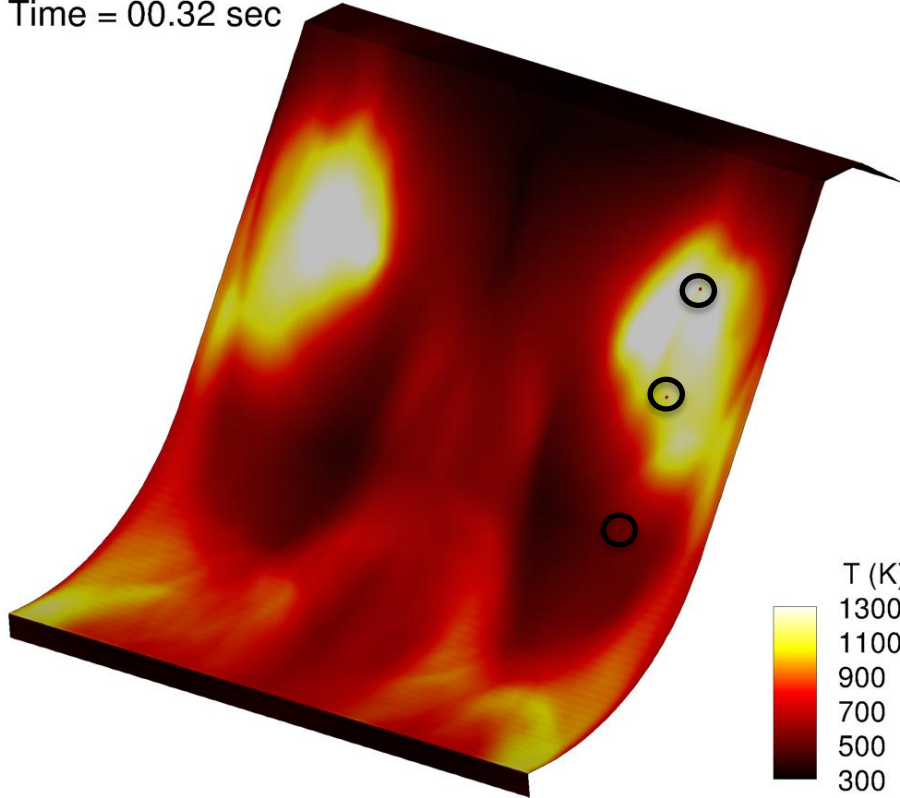


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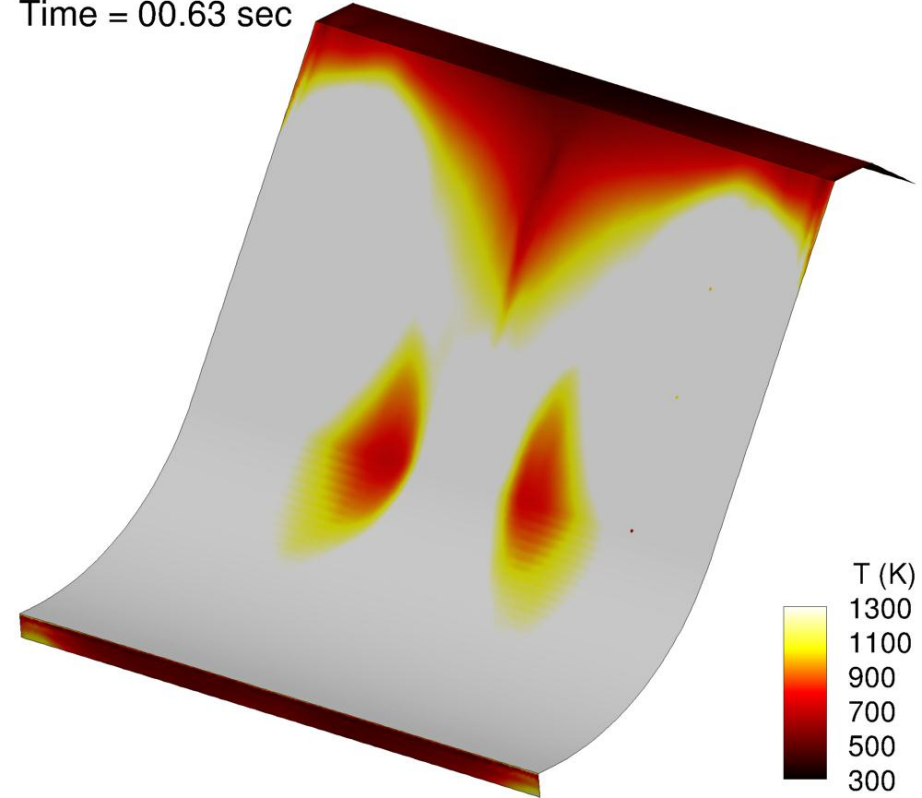


- Instantaneous temperature distribution over MFD
 - Temperature builds-up over time
 - Relatively cooler sensor locations (stainless steel) identified
 - Lack of water cooling results in wide spread melting

Time = 00.32 sec

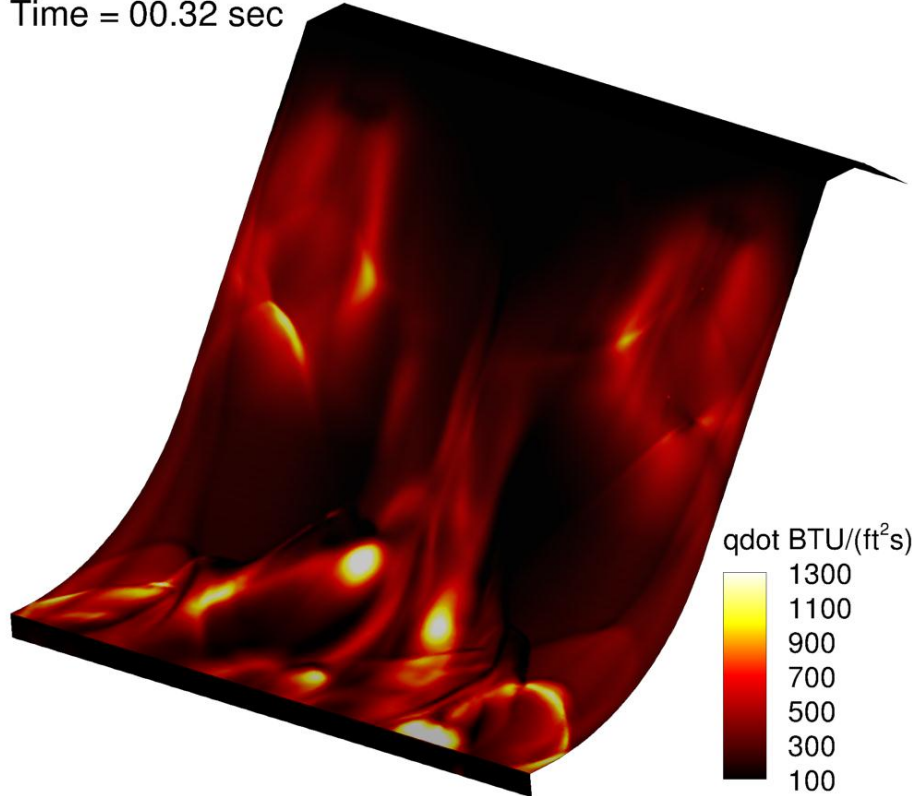


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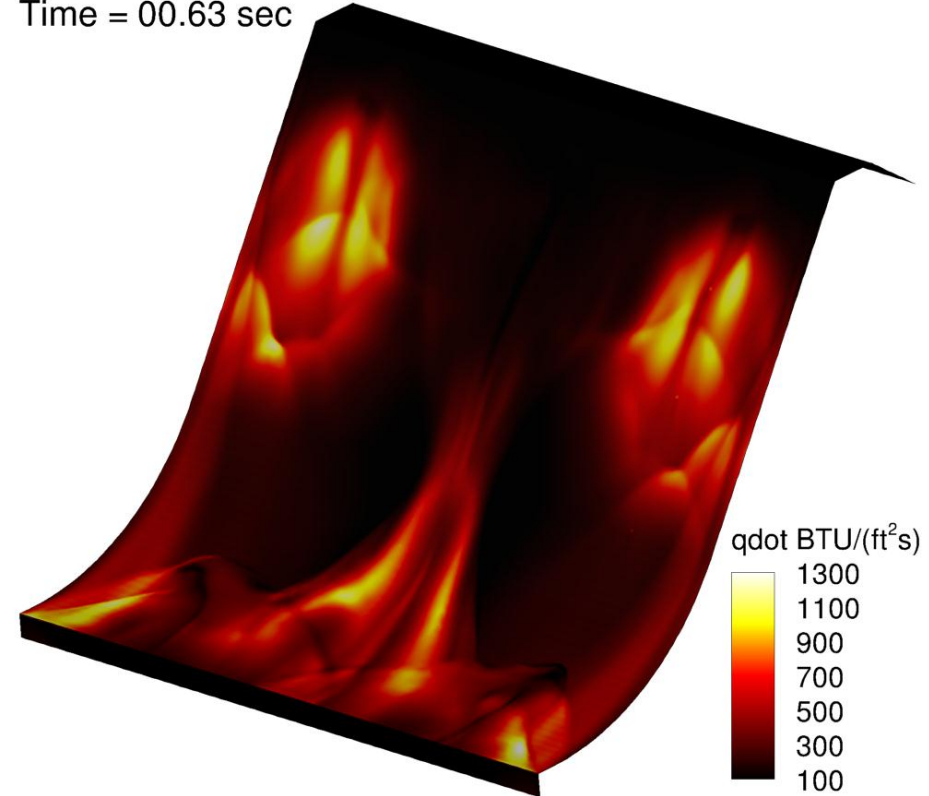


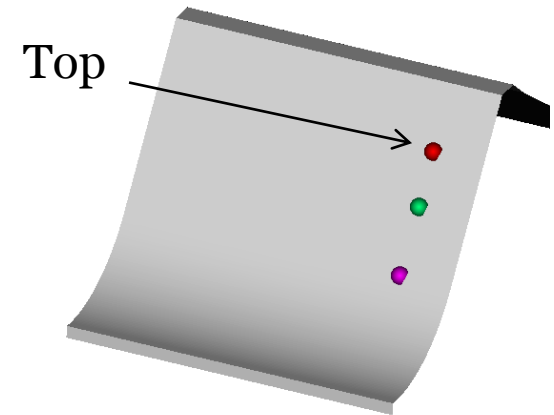
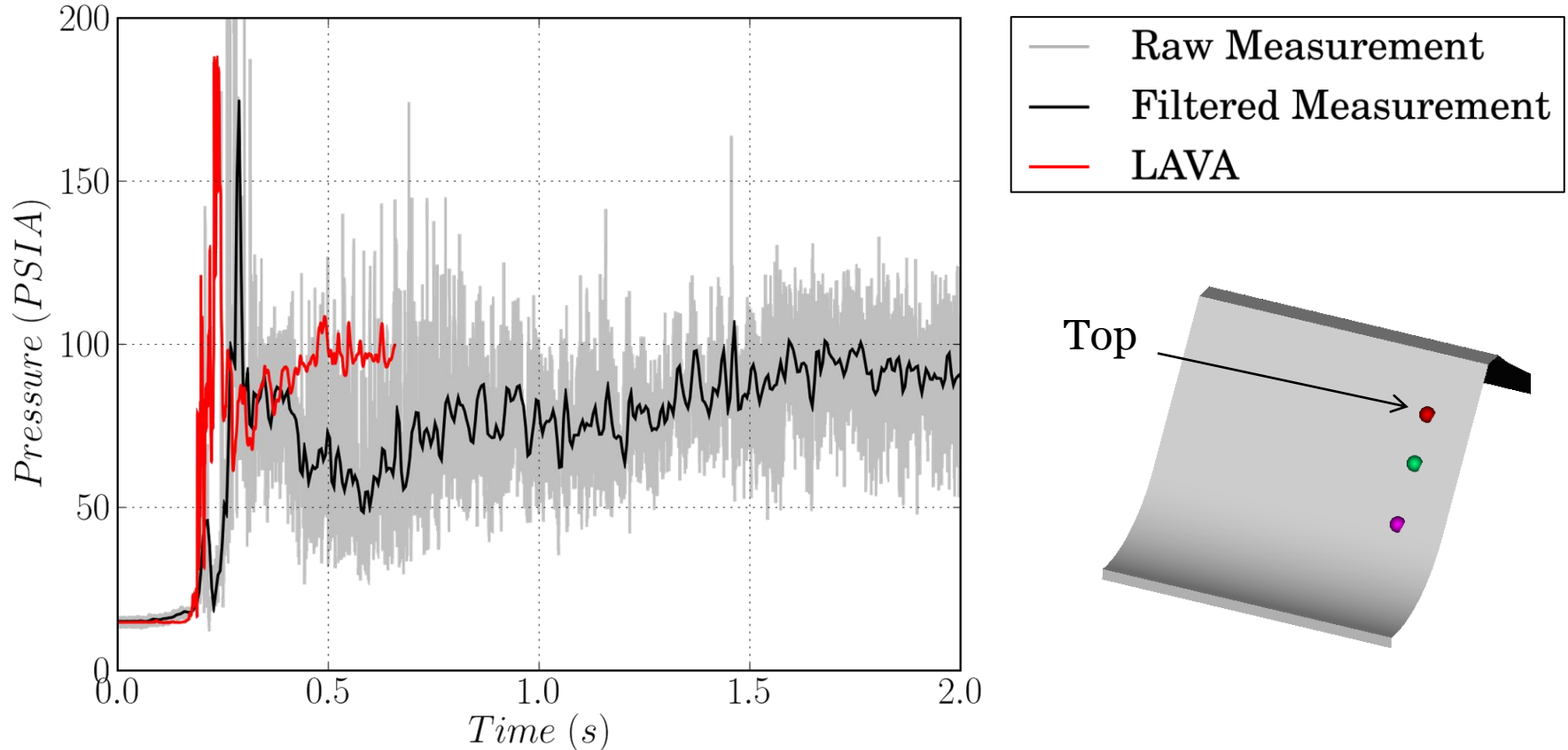
- Instantaneous heat flux distribution over MFD
 - High heat flux regions at the primary and secondary impingement locations
 - Similar pattern as the pressure distribution

Time = 00.32 sec

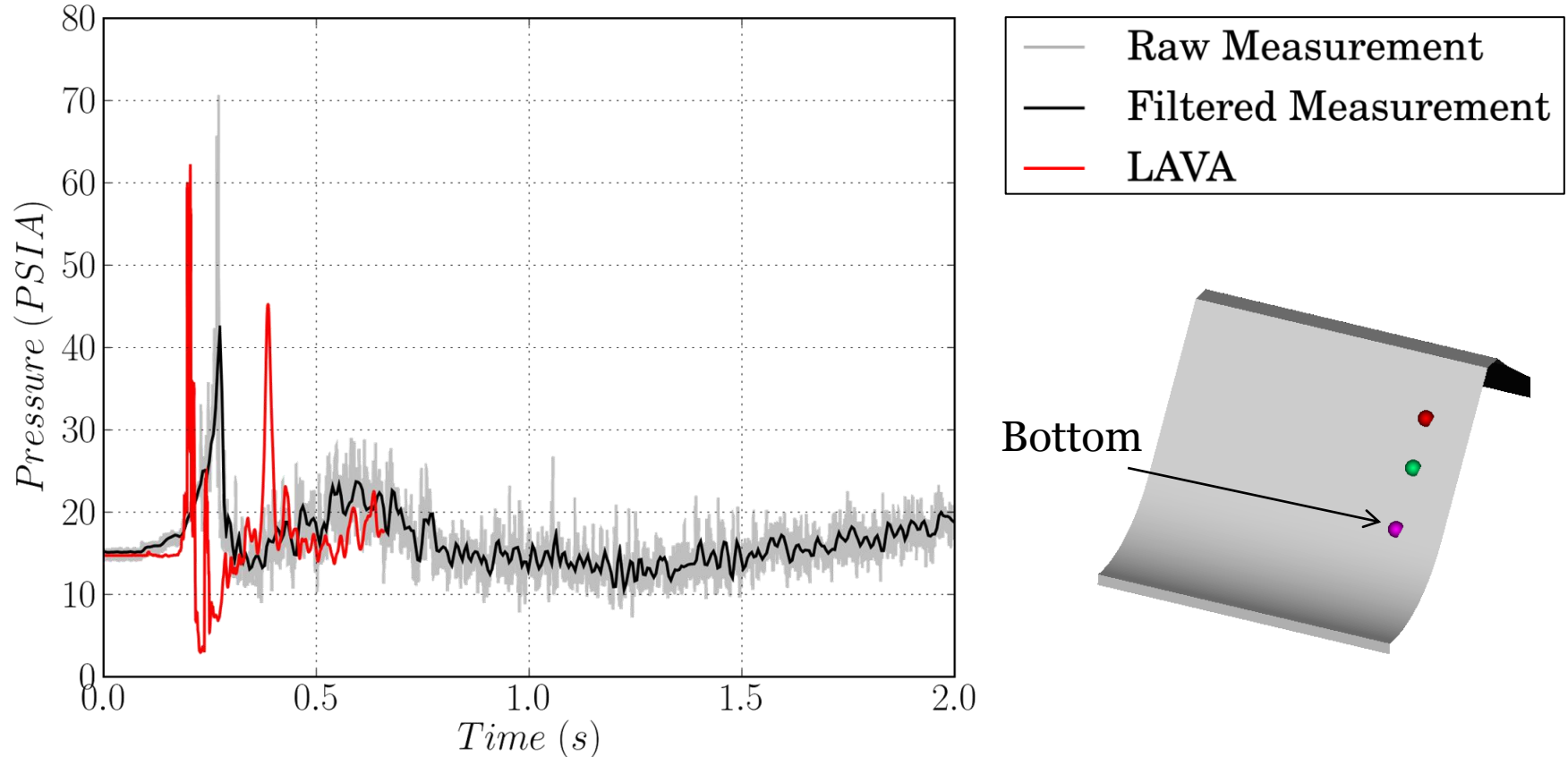


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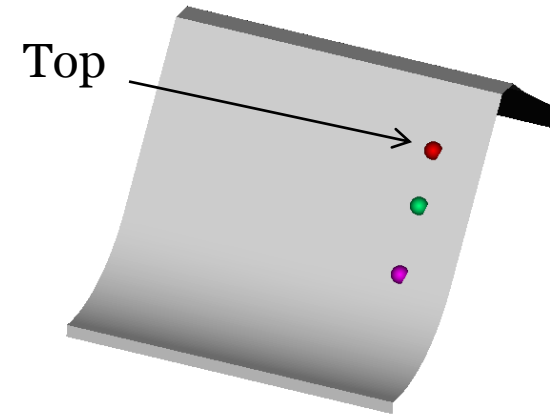
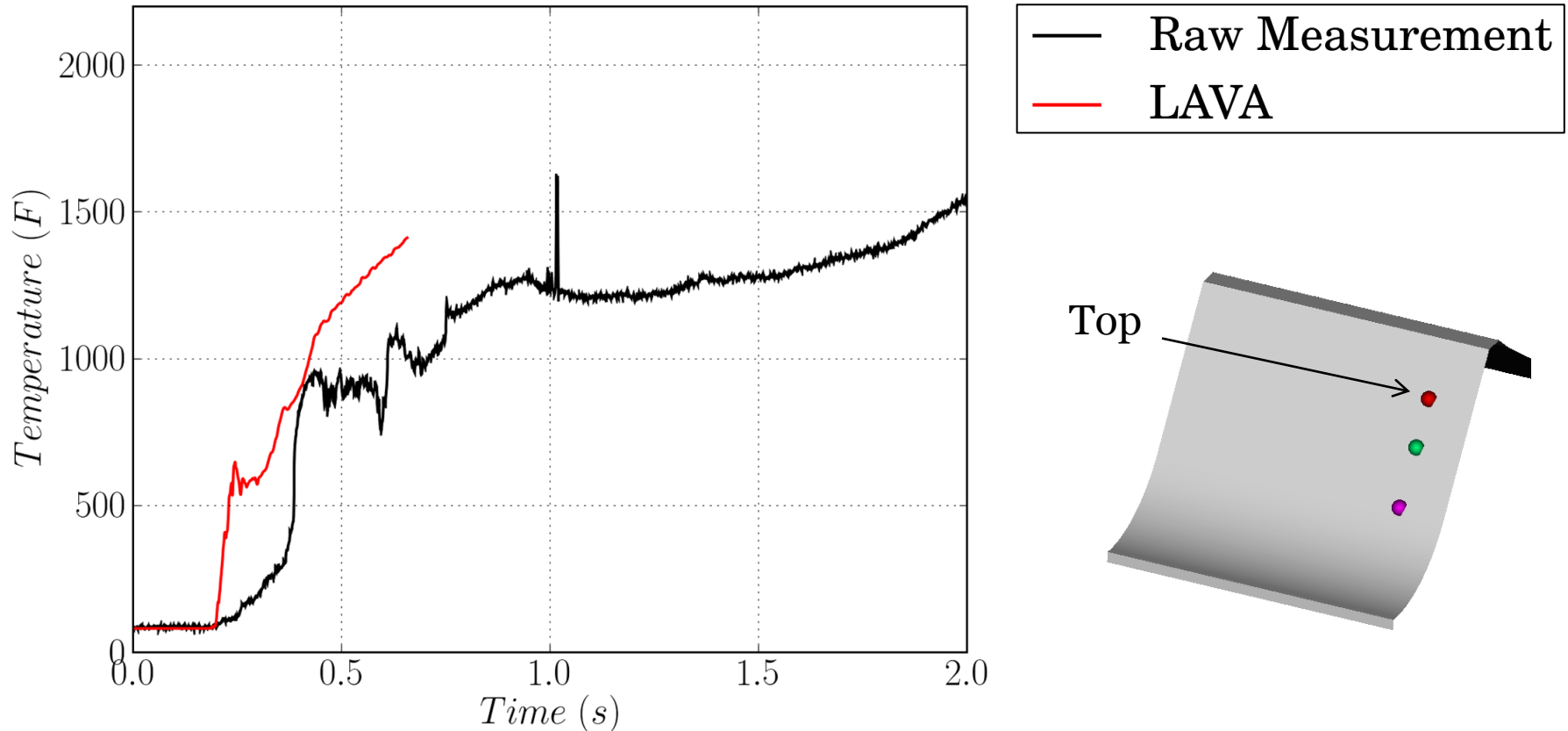




- Peak Ignition Over Pressure (IOP) well predicted
- CFD simulation seems to precede measurement by ~0.05 sec.
 - Difference maybe attributed to assumptions emphasized earlier
 - Particularly, the omission of water sound suppression system

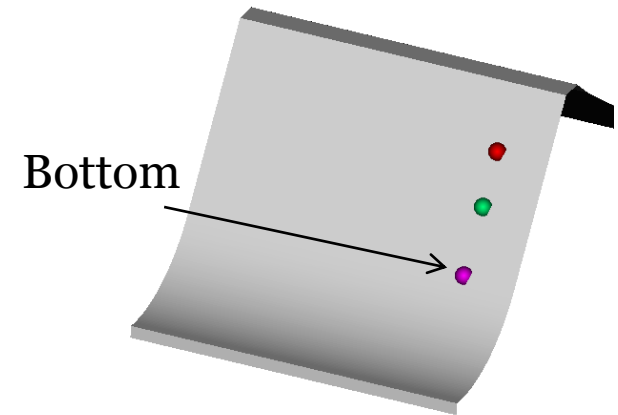
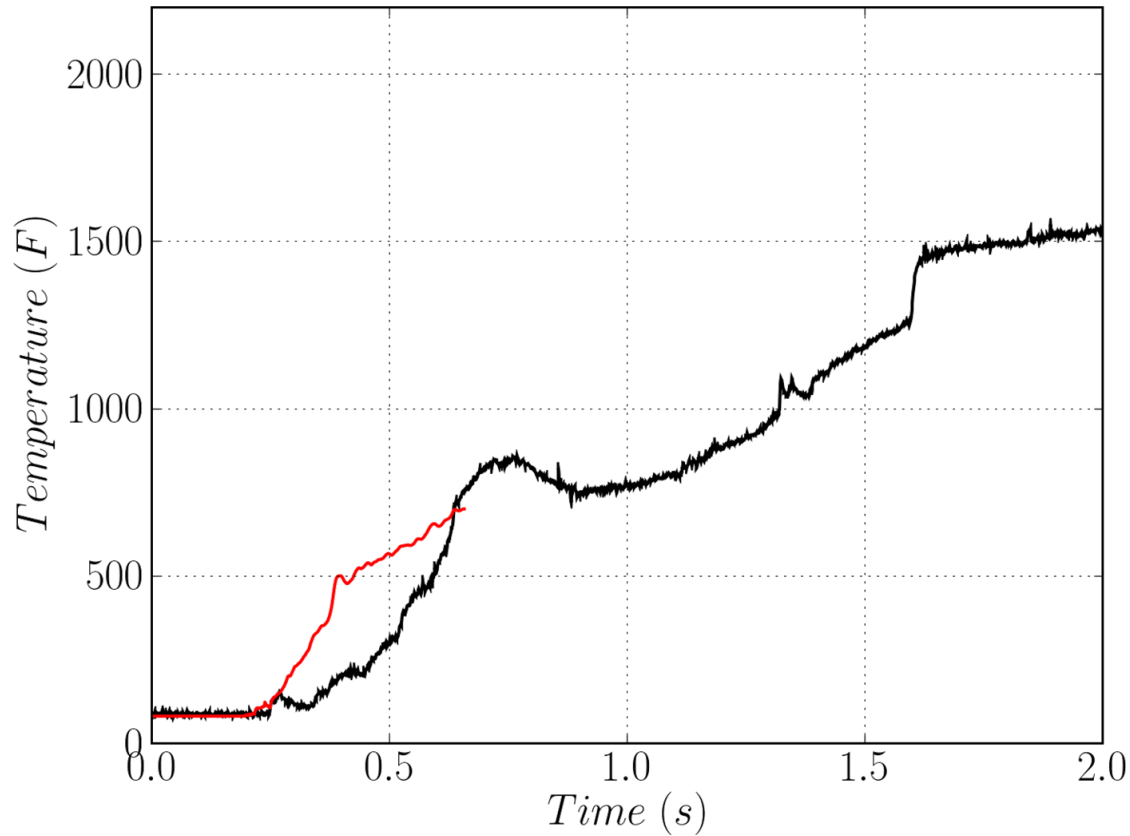


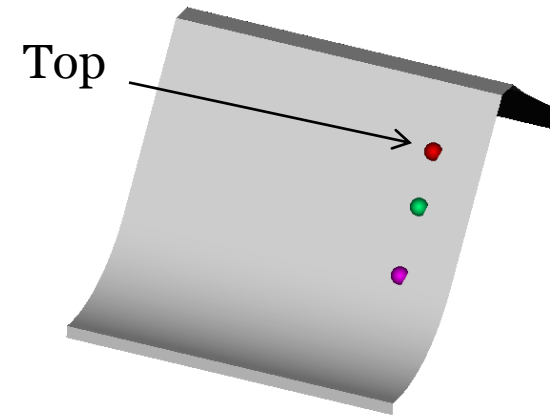
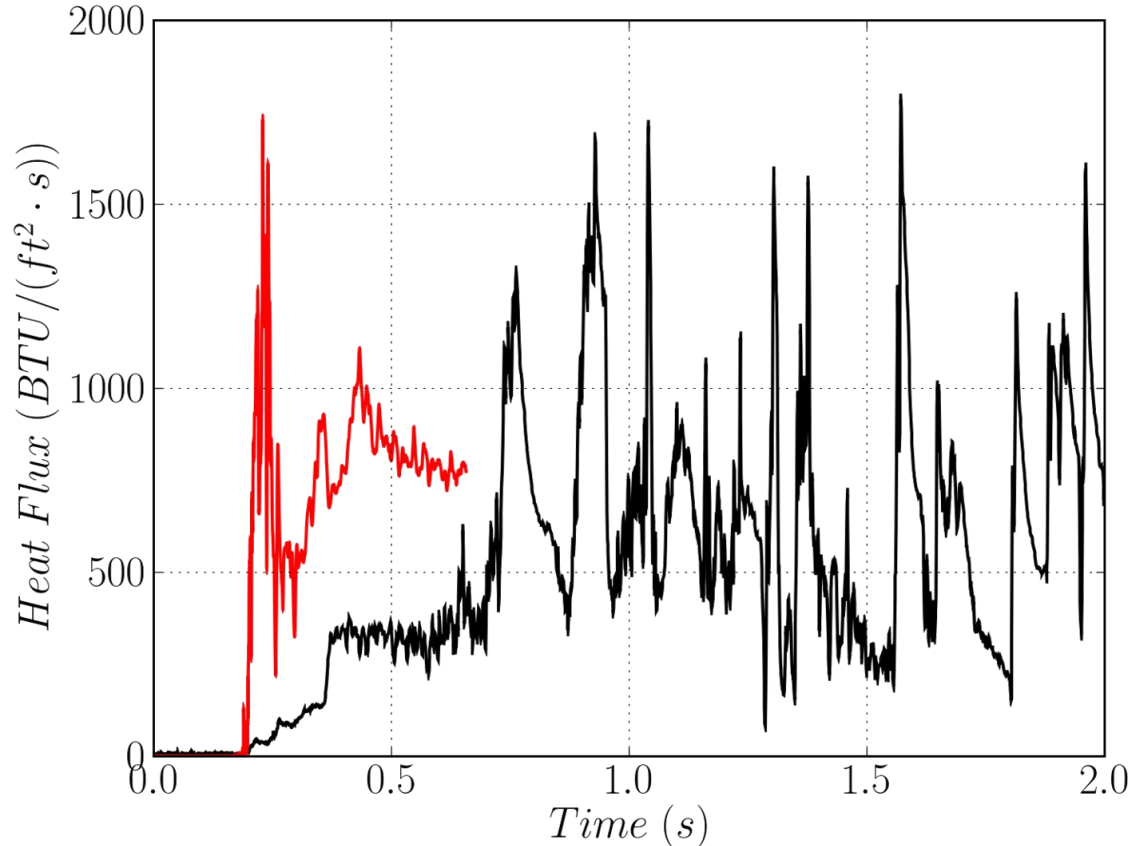
- Similar time shift as in the top sensor
- CFD shows a dip, followed by a secondary peak (~0.4 sec)
 - Not observed in measurements
 - Reason is to be investigated (possibly also due to water system suppressing the IOP)



- Same time shift issue appears for temperature and heat flux
- Overall, well matched temperature climb profiles

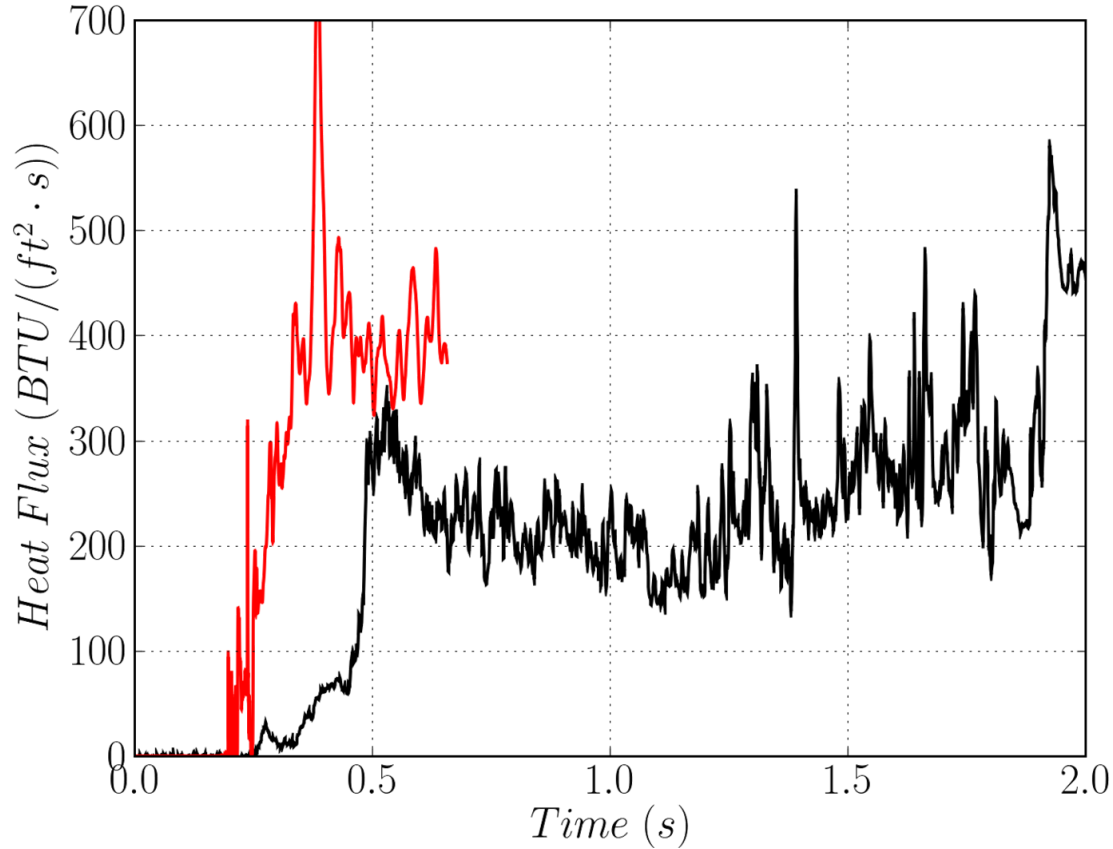
STS-135 :: BOTTOM TEMPERATURE SENSOR



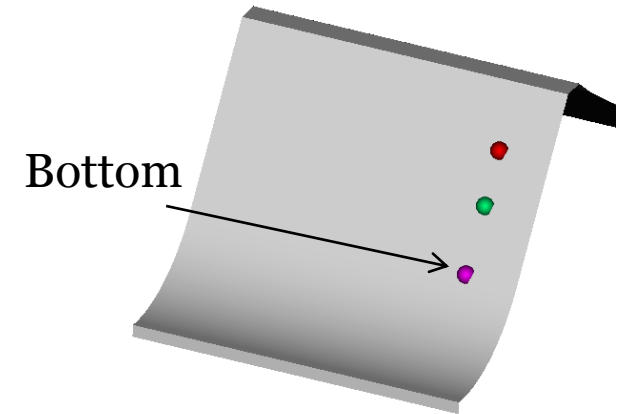


- The initial heat flux peak (~ 0.3 sec) not observed in measurements
- Spikes in measurements were attributed to particle impingement
- CFD prediction is conservative within reasonable margin
 - Heat flux is difficult to measure and simulate
 - Large uncertainties in both

STS-135 :: BOTTOM HEAT FLUX SENSOR



— Raw Measurement
— LAVA



- A first-principles based analysis of MFD heating
 - Conjugate fluid flow/ solid heat transfer CFD simulation
- Many simplifying assumptions were made
 - Physical and geometrical complexities/unknowns
- Reasonable agreement with the measurements
 - Temporal discrepancy is observed, possibly due to water exclusion
 - IOP wave amplitude is accurately captured
 - Temperature predictions are very consistent
 - Heat flux predictions are conservative within reasonable margin
 - Keeping in mind the large measurement uncertainty in heat flux
- Present method is:
 - Computationally affordable
 - Can be practically used to guide design process
- Would benefit from further validation in simpler cases
 - Investigation of sensitivity to modeling simplifications