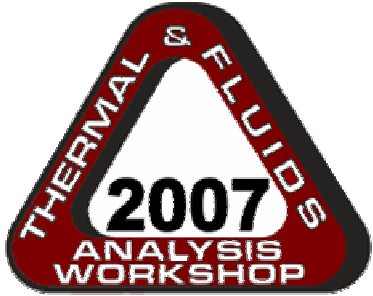




**Thermal Cooling Design of an Electronic System
using Coupled Conduction, Three Dimensional
Convection (CFD), and Radiation Heat Transfer
Finite Element Analysis with PID-Control System**

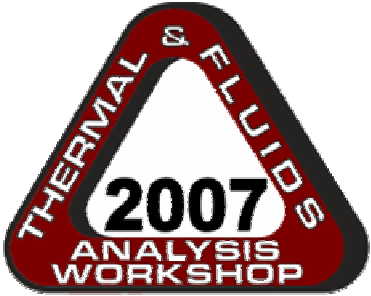
**Venkatacha Parameswaran
Boeing**

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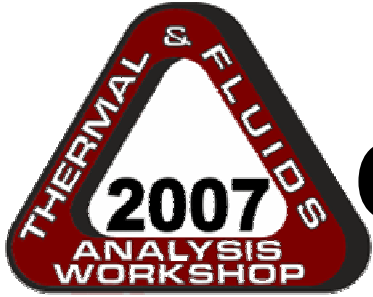
Overview

- **Purpose**
- **Background**
- **The 3 axis system**
- **FE Modeling**
- **The Control System**
- **Results**
- **Conclusion**



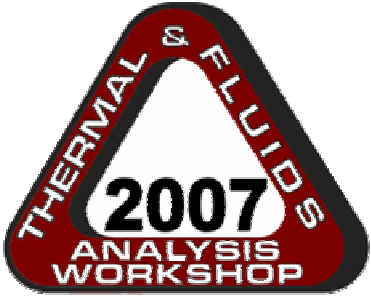
Abstract

- **This paper attempts to explain the concurrent thermal design of an electronic component assembly, involving coupled conduction convection, and radiation analysis together with Proportional, Integral, and Derivative control**
- **I-DEAS/TMG/ESC software is used to demonstrate the technique**



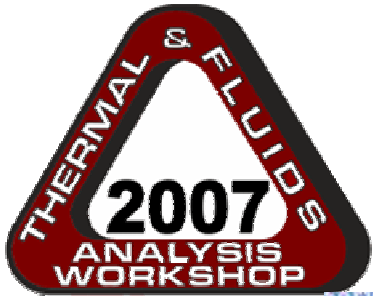
Concurrent Engineering

- **In concurrent engineering, various engineering disciplines work together in unison to come up with an optimum design**
- **This eliminates redesigns and waste.**
- **Generally designs are created and owned by mechanical design organization based on compromises among various engineering disciplines**

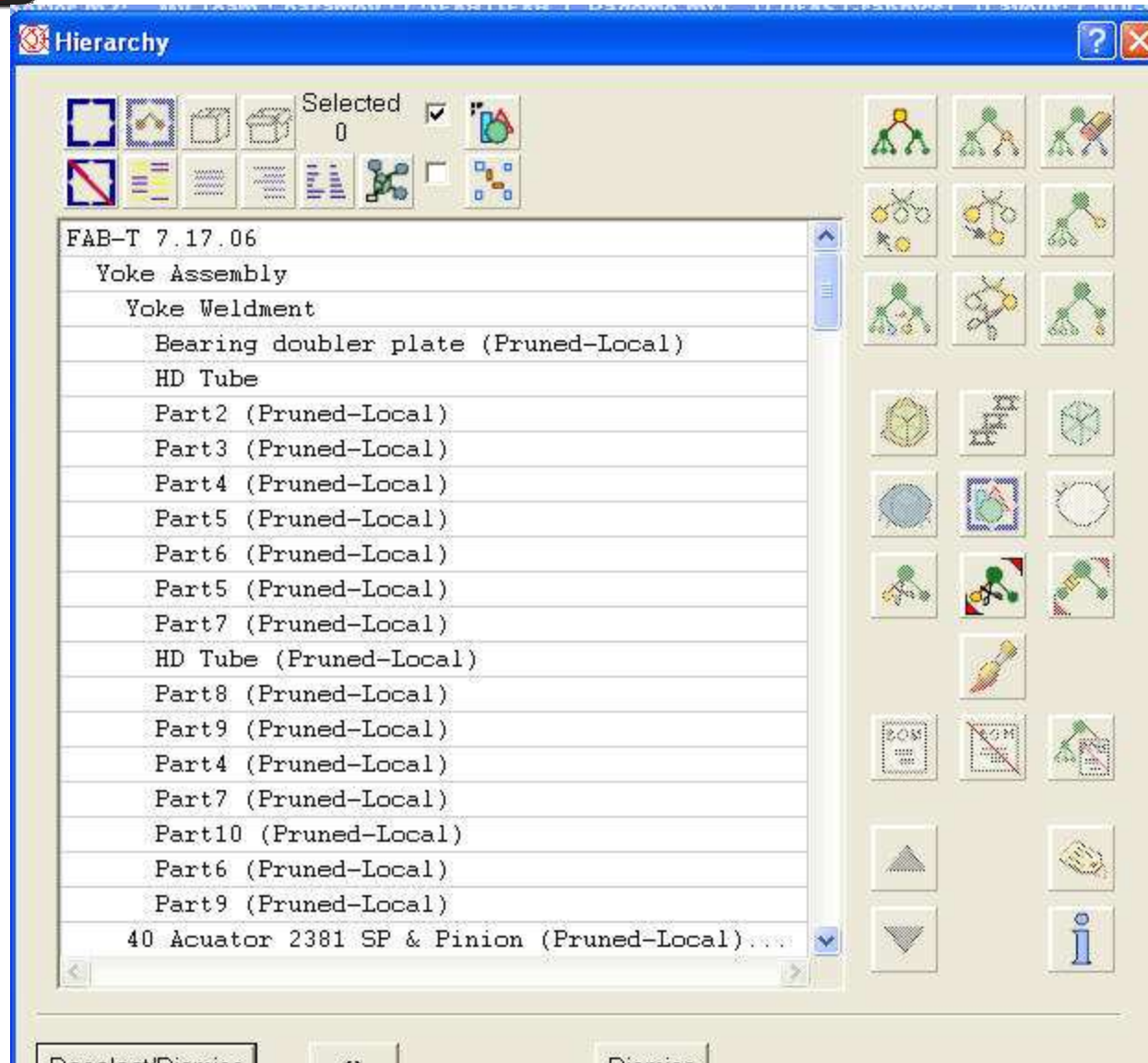


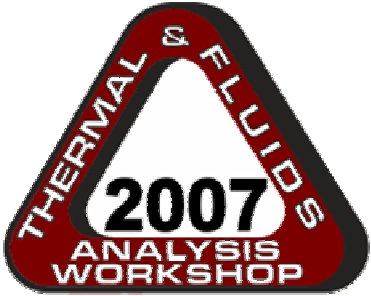
Implementation

- **Designs are assemblies, sub-assemblies, or LRUs, and parts created in a CAD design tool**
- **This is then imported into the analysis tool suite**
- **Only parts, sub-assemblies that are deemed to be important for thermal analysis are selected**
- **Such parts can be selected by the use of prune features in IDEAS from the assembly hierarchy**
- **This involves the use of assembly tree structure**



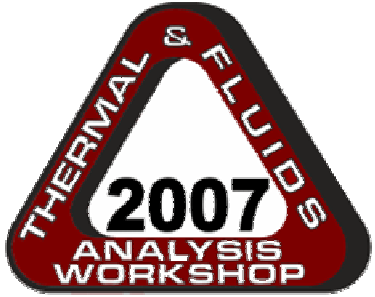
Parts Selection



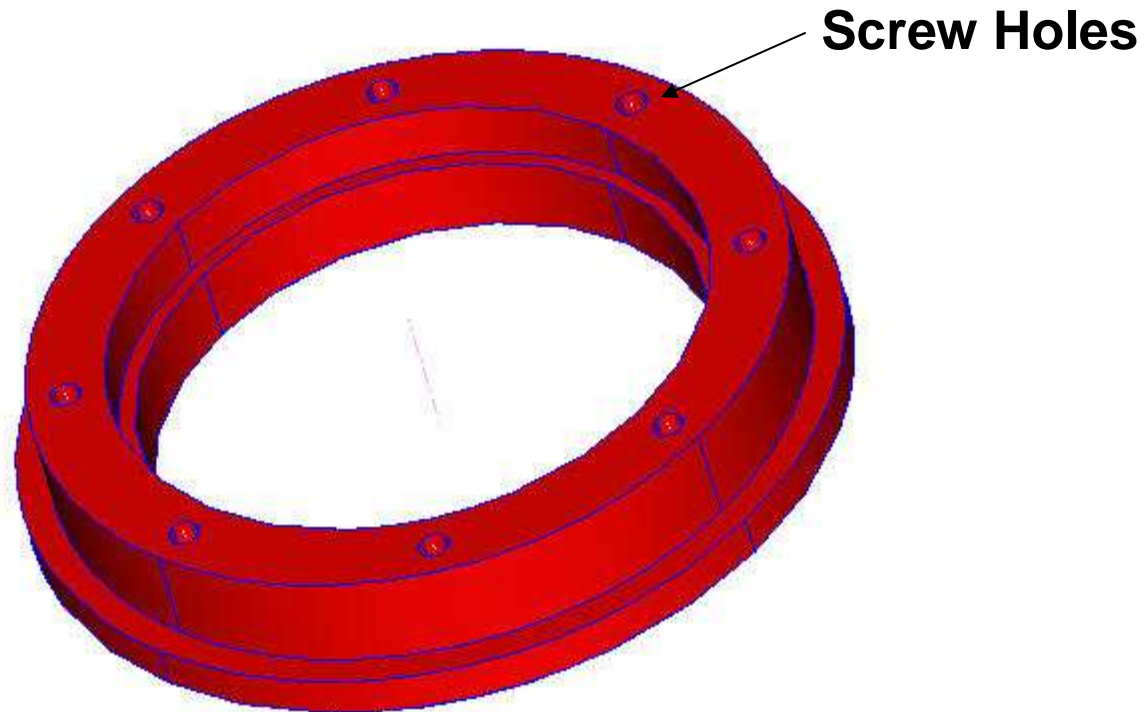


Idealized part

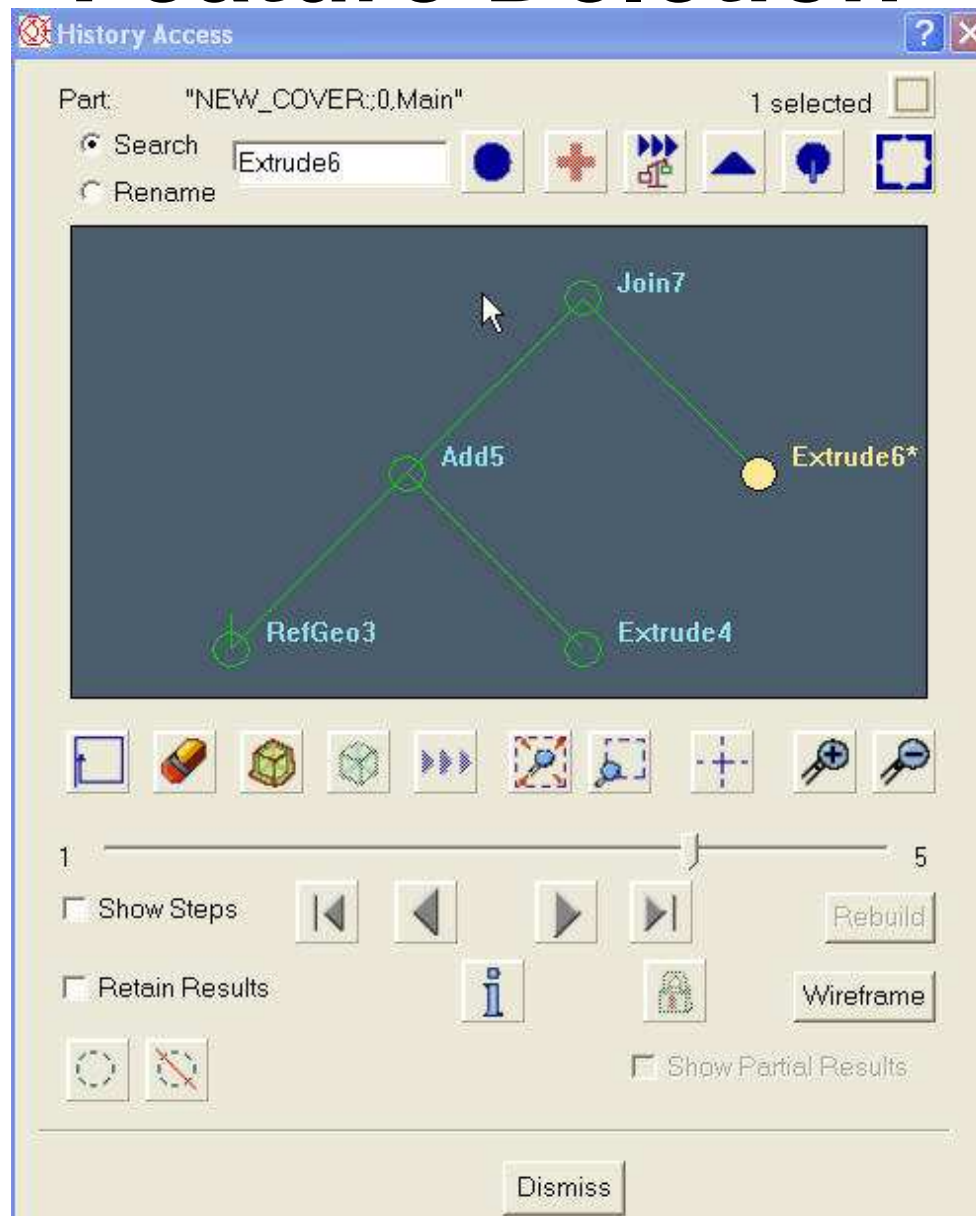
- **After parts are selected unwanted features are removed**
- **Chamfers, holes, fillets and minor details are removed**

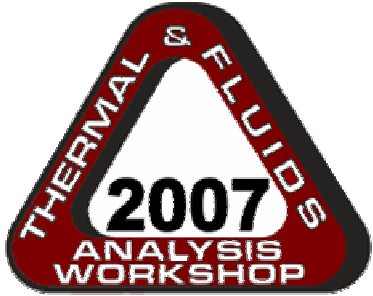


Part Features



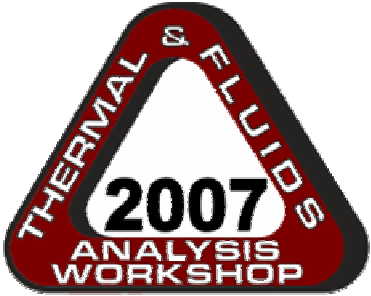
Feature Deletion





Meshing and Analysis

- **The parts are then meshed, checked and all the FEMs are combined**
- **Analysis is run, results examined**
- **If it does not meet requirements, modifications made and re-run and recommendations provided**



Solution

- **Most thermal involves conduction, convection, and radiation.**
- **In many problems use of most commonly used empirical correlations for convection are inadequate**
- **Flow field may be complex and can not be approximated by one dimensional flow field**
- **Thus use of empirical correlations may yield incorrect results**



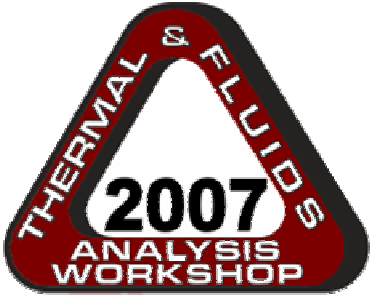
Governing Equations

- **3-D Transport equations:**
 - **Energy** $\frac{\partial(\rho h)}{\partial t} + \frac{\partial(\rho U_j h)}{\partial x_j} = \frac{\partial(k/C_p \partial(T)/\partial x_j - \underline{\rho u_j h'})}{\partial x_j} + S_h$
 - **Momentum** $\frac{\partial(\rho h)}{\partial t} + \frac{\partial(\rho U_j h)}{\partial x_j} = \frac{\partial(\mu \{ \partial U_i / \partial x_j + \partial U_j / \partial x_i \} - \underline{\rho u_i u_j})}{\partial x_j} + S_{U_j}$
 - **Mass conservation** $\frac{\partial \rho}{\partial t} + \frac{\partial \rho U_j}{\partial x_j} = S$
 - **Turbulence k-e Model with wall function**
 - **The above are integrated over a finite control volume and difference equations are obtained at various volume centers.**
 - **Requires boundary conditions of surface temperature or flux, which is unknown to be obtained from conduction solution**



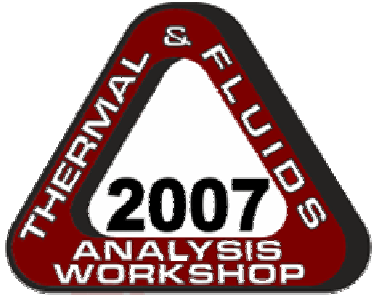
Governing Equations

- **Sij includes the buoyancy terms, Coriolis forces, and centripetal forces**
- **Buoyancy: $-g\beta(T-T_r)g$**
- **Coriolis: $-\rho(2\omega \times V + \omega \times (\omega \times R))$**
 - **V is the velocity vector and ω is the angular velocity vector**



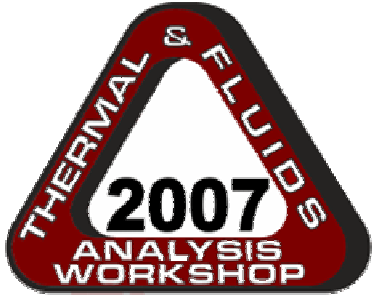
Governing Equations

- **Conduction Equation:**
 - $\partial(\rho C_p T)/\partial t = q + (\partial/\partial x(k\partial T/\partial x) + \partial/\partial y(k\partial T/\partial y) + \partial/\partial z(k\partial T/\partial z))$
- **Boundary Condition: Radiation, Convection**
 - Radiation in terms of a view-factor, emissivity, and enclosure temperature
 - Convection in terms of a heat transfer coefficient, and fluid temperature, which is unknown and has to be obtained from solution of transport equations



Boundary Conditions

- For an infinitesimal control volume around the solid/liquid interface the energy flux should balance
- $Q = kdT/dn$ (solid) = KdT/dn (Liquid)
- The above formulation couples the conduction convection transport and generally written as $h(T_w - T_f)$, where T_w is the surface temperature and T_f the fluid temperature



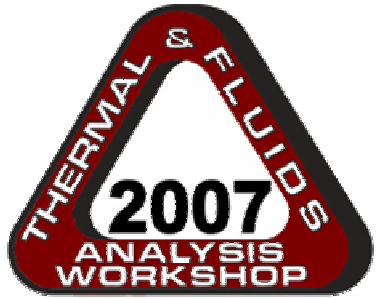
Example

- **The following examples demonstrates the principle**
- **It does not represent any real component, used for illustration only**

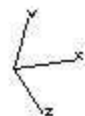
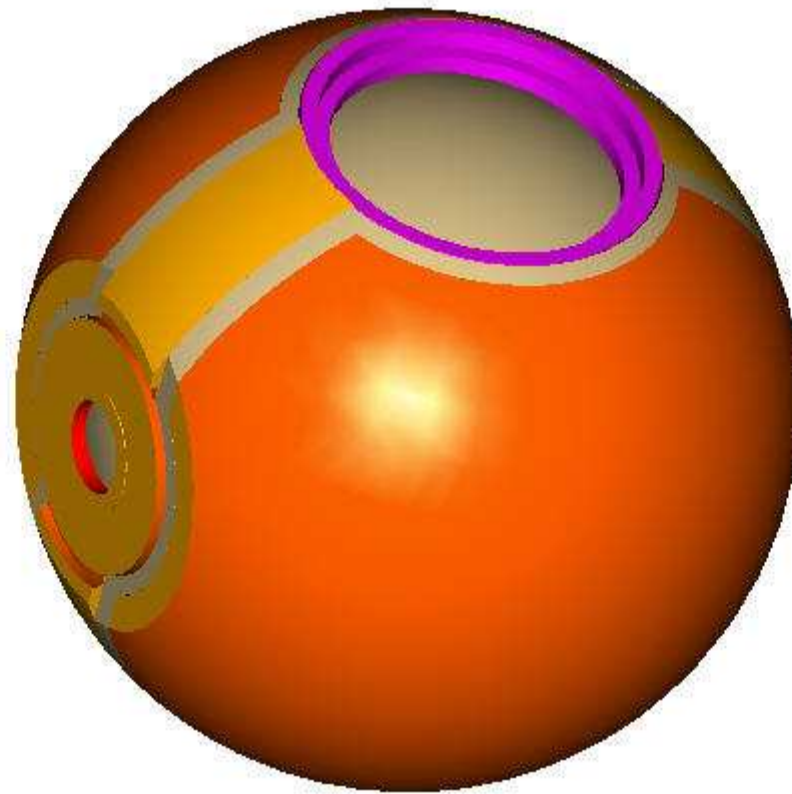


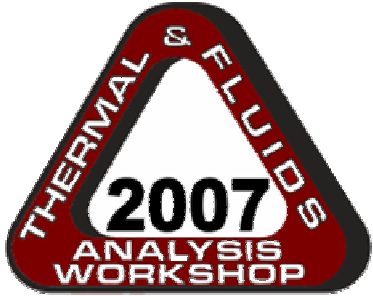
Background

- **The system consists of parts inside a sphere called instrument mount which rotates about another sphere called inner sphere**
- **This rotates about another sphere called outer sphere which in turn rotates about another sphere called case. The case does not rotate but fixed.**
- **The innermost sphere is kept fixed in an inertial frame of reference**
- **The parts dissipate heat and cooled by water on the case**
- **It is desired to keep the part temperature at a desired level**



Sphere





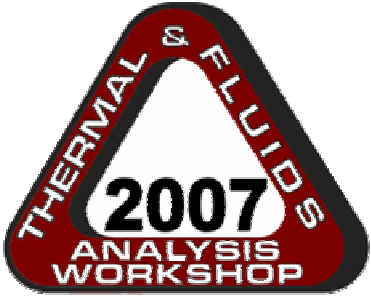
The 3-Axis System

- **The air gap between the sphere conducts heat**
- **The case is cooled by water**
- **A control system maintains the temperature of the casing to a desired set point**



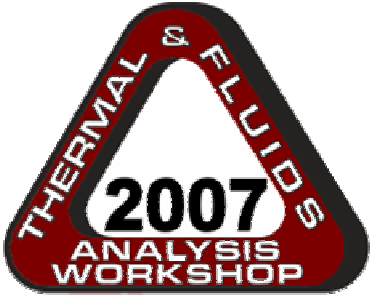
Thermal Model

- **The goal of the thermal model is to be able to predict the thermal profile of the system which will help in studying the effect of various parameters on the performance**
- **Finite element thermal model and validated**



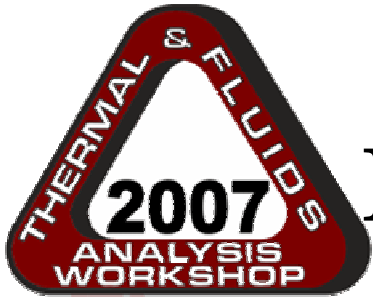
Thermal Model

- **Both solid and surface elements were modeled.**
- **Heat conduction and radiation across gaps were modeled with articulation.**
- **Cooling thermal control system was modeled by user subroutines**
- **Rotation was also included in the model**

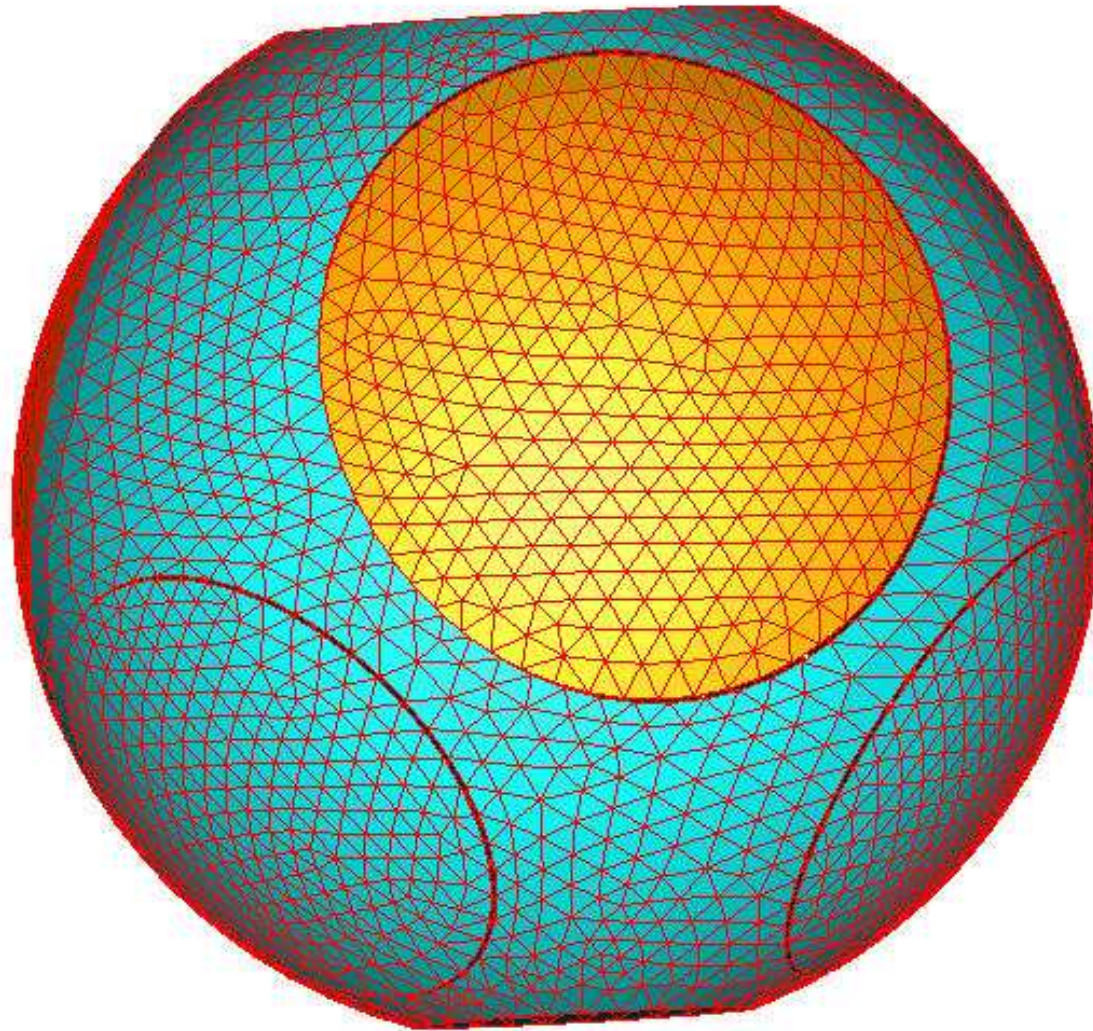


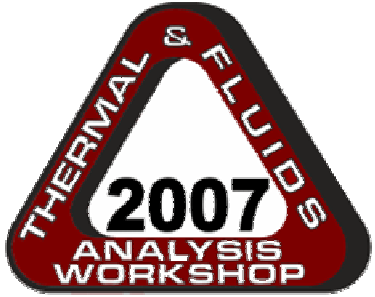
Thermal Model

- **Natural convection in the central air pocket was modeled in a rotating frame of reference using the CFD equations in ESC**

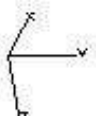
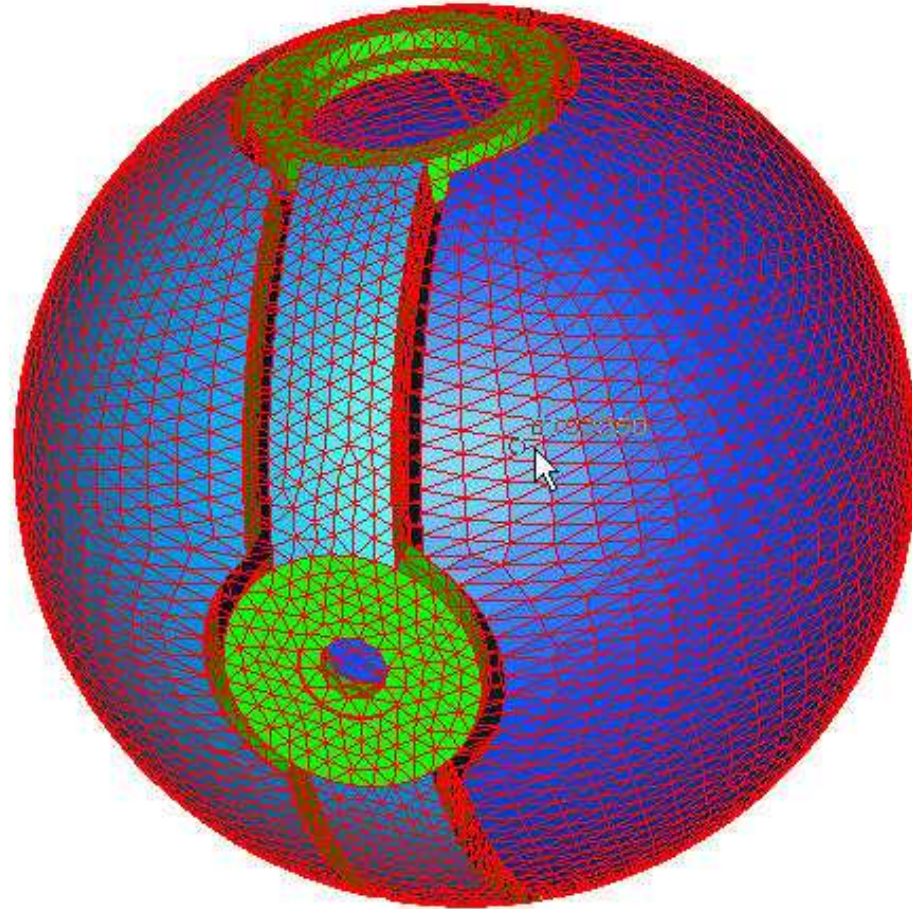


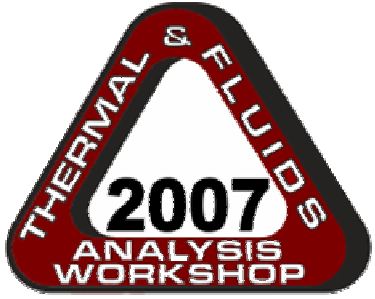
FE Model of the Assembly



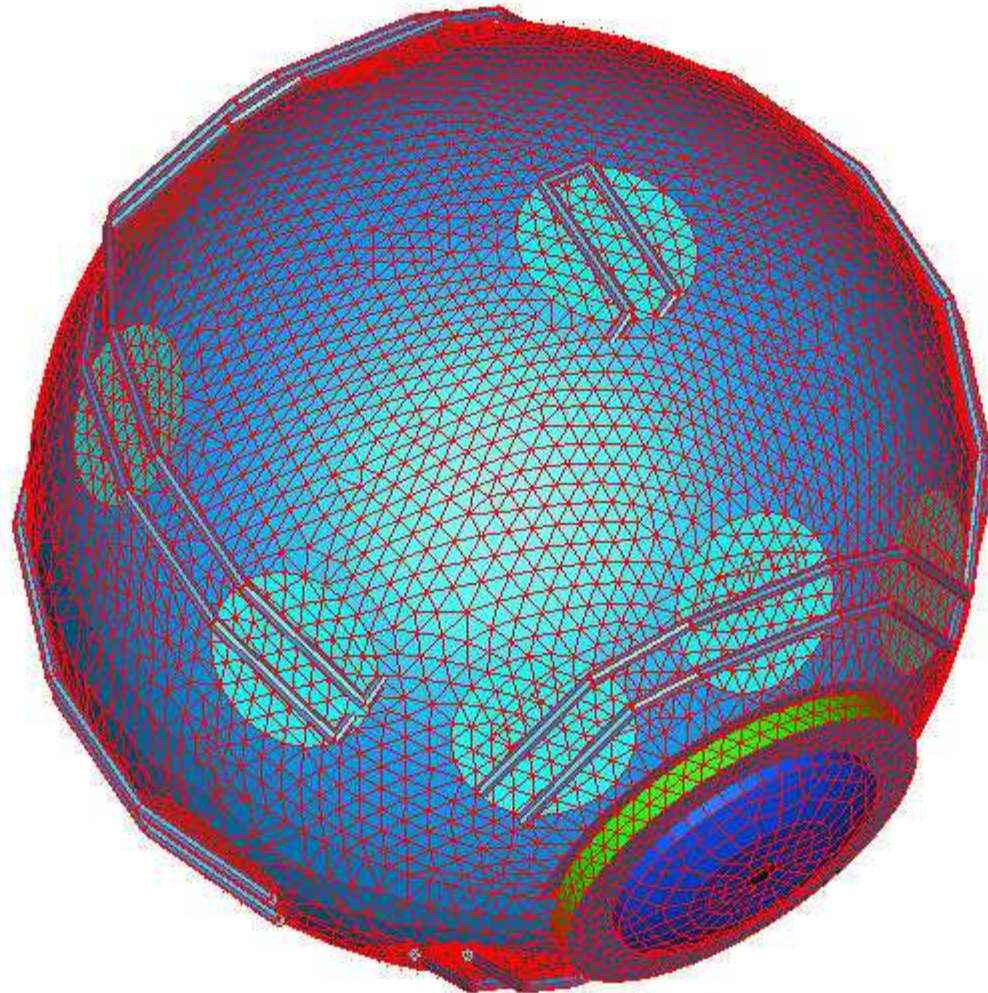


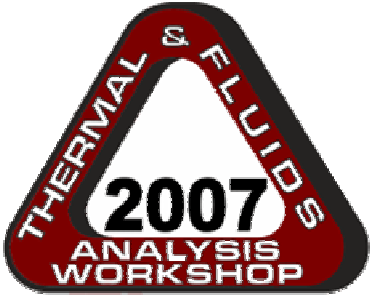
FE Model of Sphere





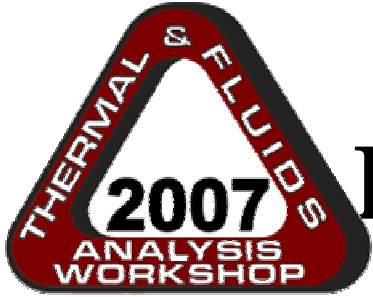
FE Model of the Tubes





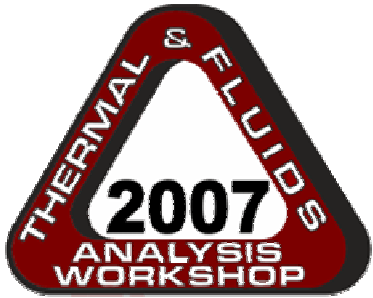
Thermal Model

- **Contact resistances at various bolted joints were modeled**
- **Conduction through bearings in torquers and encoders were modeled from the MIT report “Analytical and Experimental Investigation on the thermal Resistance of Angular Contact Bearings” by MM Yovanovich, 1967**
- **Conduction across air gaps (rotating) was modeled as articulation**

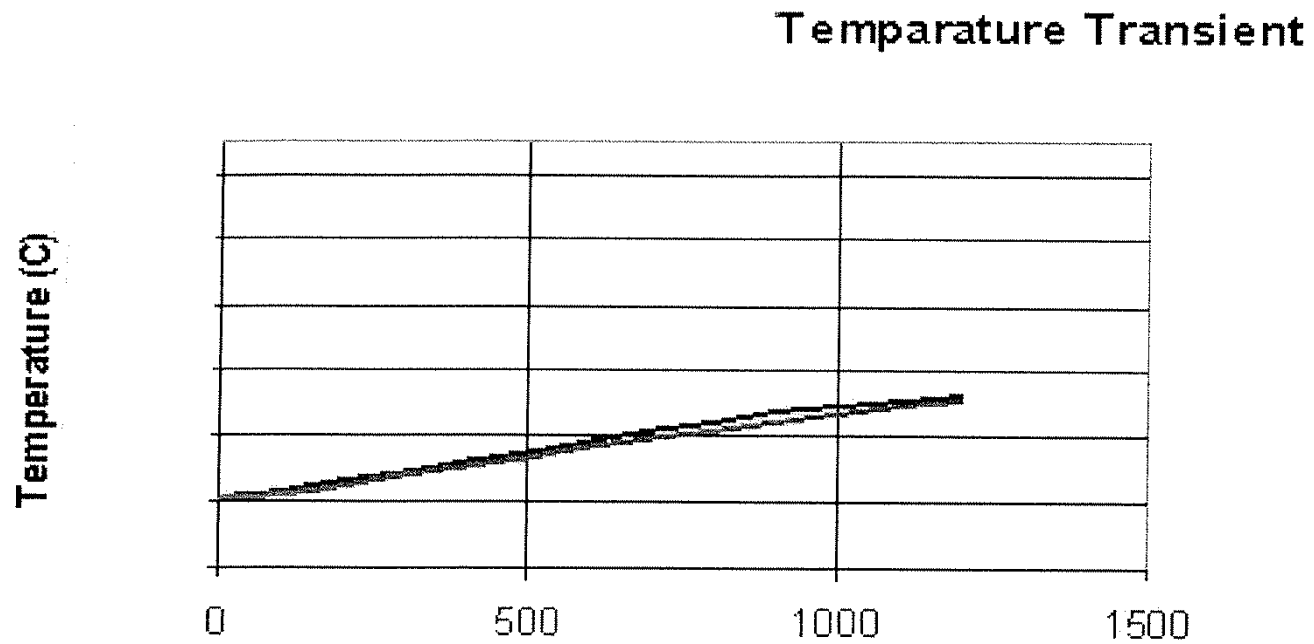


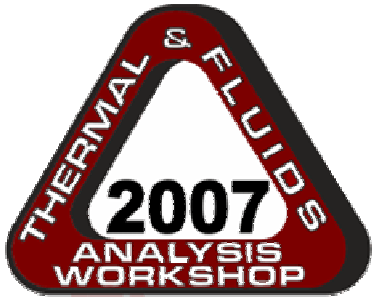
Feed-Back Control System

- $T_{cerr} = (T_{case} - T_{cset})$
- **Case Current: $I_{case} = K_{pc} T_{cerr}$**
- $T_{oserr} = (T_{os} - T_{osset})$.
- **Outer Sphere Current: $I_{os} = I_{os} + K_{iog} T_{oserr} dt$.**

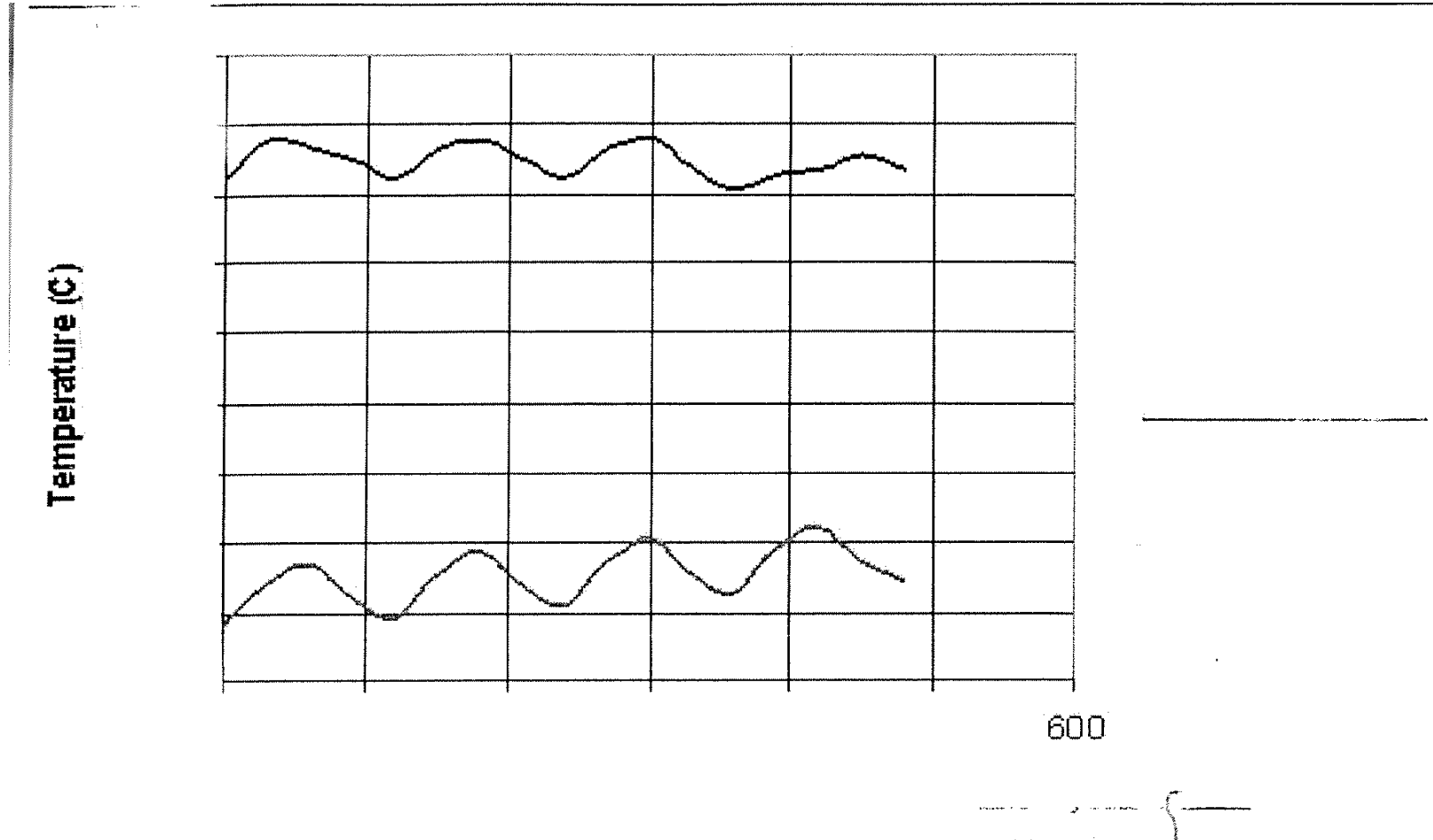


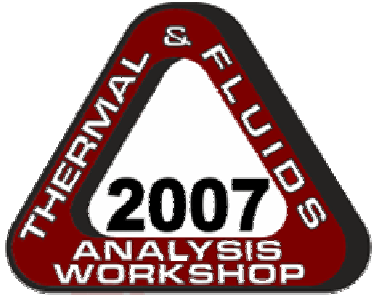
Results





Results





Conclusions

- **Concurrent engineering concepts enabled design analysis of the system**