



Multiphysics-based Damage Modeling and Crack propagation using Meshless Peridynamics Approach

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- ◆ Prof. Max Gunzburger (Florida State University)



- ◆ Background
 - ◆ Challenges with damage, crack propagation
 - ◆ Peridynamics based meshless modeling approach

- ◆ ACT's Development of Peridynamics based meshless tools for damage and crack propagation
 - Multi-physics based modeling of corrosion damage in metals
 - Crack propagation in composites
 - Other examples

- ◆ Summary



Outline



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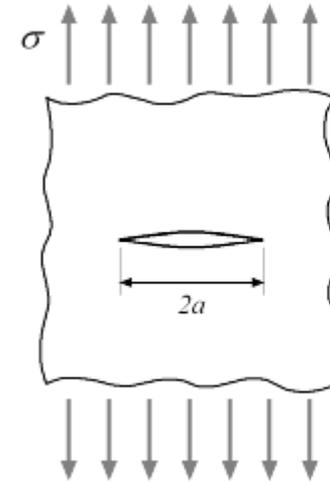
- ◆ Summary

- ◆ Conventional Failure Analysis (strength of materials approach)
 - Most straight forward design consideration to avoid structural failure is to keep the stresses, strains, or strains in a material within the *material strength* limits and use a *factory of safety*.

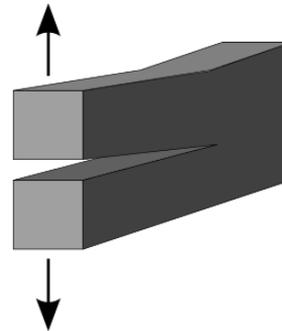
Maximum Stress ↔ Strength of Material

Applied Stress ↔ Failure Criterion

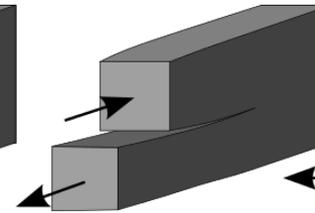
- ◆ Fracture Mechanics approaches define three basic modes of crack tip deformation
- ◆ Common analysis includes finding the stress intensity factor, K .
 - For example, a plate with crack (shown on right)
 - Relations strain energy release rate f



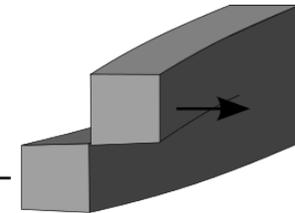
$$K_I = \sigma \sqrt{\pi a}$$



Mode I:
Opening



Mode II:
In-plane shear



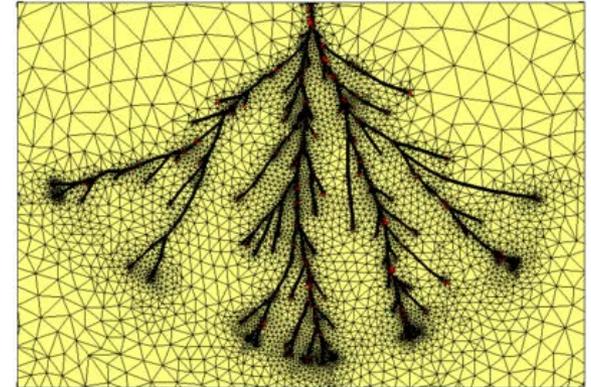
Mode III:
Out-of-plane shear

- ◆ Several relations between strain energy release rate and stress intensity factors (for different conditions, geometry) have been developed
 - **Griffith's (energy) criterion, Irwin's formula, CTOD, J-integral**

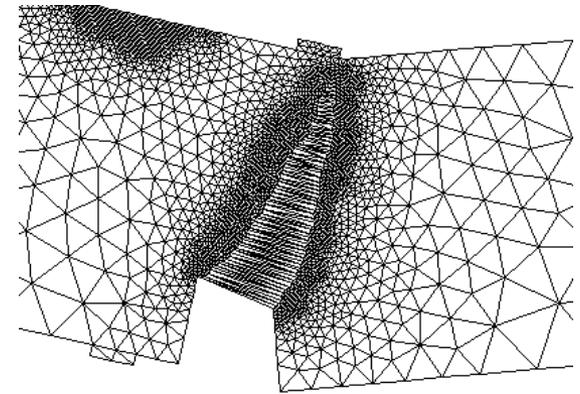
- ◆ Despite development in finite element methods, fracture mechanics and several advancements in theory of applying fracture mechanics approaches for failure prediction, challenges exist on how can the crack be modeled
- ◆ Things to consider:
 - Crack propagation path
 - Branching of cracks (splitting)
 - Load redistribution due to crack

The challenge ...

- ◆ Crack in conventional mechanics is a singularity which needs explicit tracking (i.e., its location need to be specified for the mechanics problem of σ evolution).
- ◆ FEM lends itself well for solving the continuum mechanics equation, but needs:
 - prescription of crack path and
 - re-meshing of the domain for every crack propagating step

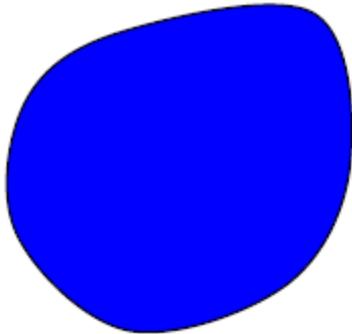


Crack propagation and branching

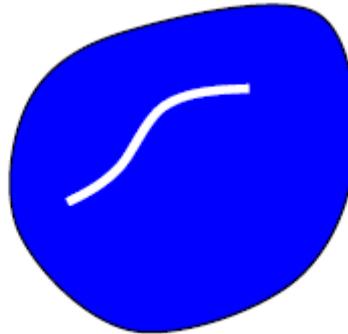


FE mesh near a crack tip

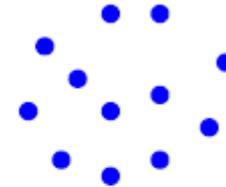
- ◆ To unify the mechanics of continuous and discontinuous media within a single set of equations.



Continuous body



Continuous body
with a defect

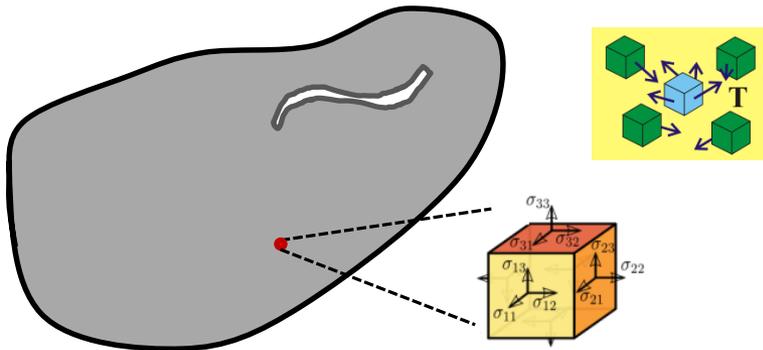


Discrete particles

- ◆ Why do this?
 - Provide a unified mathematical description of the material without the issues of discontinuity (crack)
 - Model complex fracture patterns
 - Avoid coupling of dissimilar mathematical systems
- ◆ To accomplish this, the *Peridynamics* approach was proposed as a reformulation of elasticity theory, by Stewart Silling (Sandia) in 2000.

- ◆ Peridynamics (PD) is a nonlocal reformulation of classical elasticity theory that permits modeling materials with discontinuities such as cracks.

peri “near” and *dynamic* “force” (Greek) → *peridynamics*

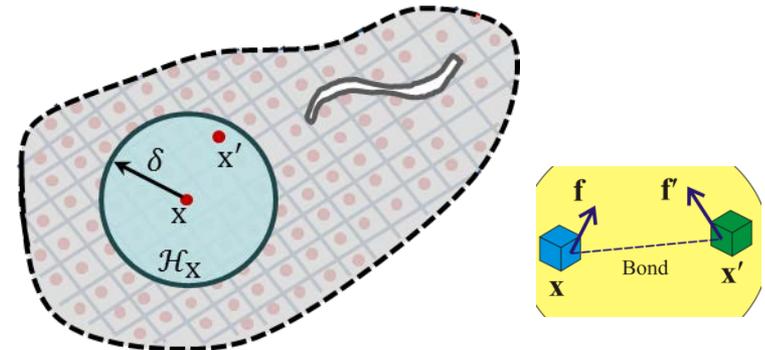


Classical continuum solid with crack

Classical/Cauchy equation of motion

$$\rho \ddot{u}(\mathbf{x}, t) = \nabla \cdot \sigma(\mathbf{x}, t) + b(\mathbf{x}, t)$$

- Assumes differentiable displacement field
- Continuous distribution of mass
- Local interactions through contact forces
- Crack (discontinuity) treated as a pathology



Peridynamic solid with crack

Peridynamic equation of motion

$$\rho \ddot{u}(\mathbf{x}, t) = \int_{\mathcal{H}_{\mathbf{x}}} f(u' - u, x' - x) dV + b(\mathbf{x}, t)$$

- Allows discontinuous fields (singularities)
- Material points interaction through bond forces, a force function, f which defines constitutive model
- Non-local integral allows for interaction over a distance

- ◆ Reformulation of classical elasticity theory, proposed by Stewart Silling, 2000.
- ◆ The internal forces within a body is treated as a network of interactions between material points
- ◆ The **governing equation** given by local conservation of linear momentum as,

$$\rho(\mathbf{x})\ddot{\mathbf{u}}(\mathbf{x}, t) = \int_{\mathcal{H}_{\mathbf{x}}} \mathbf{f}(\mathbf{u}(\mathbf{x}', t) - \mathbf{u}(\mathbf{x}, t), \mathbf{x}' - \mathbf{x})dV_{\mathbf{x}'} + \mathbf{b}(\mathbf{x}, t)$$

\mathbf{x} is material point (reference configuration)

$\mathbf{u}(\mathbf{x}, t)$ is displacement of material point \mathbf{x}

\mathbf{f} is nonlocal force density (vector function),
force exerted by material point \mathbf{x}' on point \mathbf{x}

$\mathbf{b}(\mathbf{x}, t)$ is external body force density

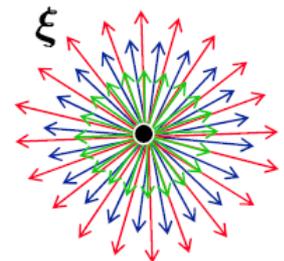
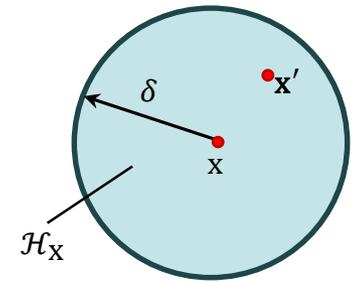
$\rho(\mathbf{x})$ is mass density

$\mathcal{H}_{\mathbf{x}}$ is neighborhood (family) of \mathbf{x} over which interactions occur

$\xi = \mathbf{x}' - \mathbf{x}$ represents a bond in reference configuration

$\eta = \mathbf{u}(\mathbf{x}', t) - \mathbf{u}(\mathbf{x}, t)$ relative displacement

$\mathbf{f}(\eta, \xi)$ describes material behavior by mapping deformation given by η for bond ξ



◆ Bond based PD model

- Simple version of Peridynamics model

$$\rho(\mathbf{x})\ddot{\mathbf{u}}(\mathbf{x}, t) = \int_{\mathcal{H}_{\mathbf{x}}} \mathbf{f}(\mathbf{u}(\mathbf{x}', t) - \mathbf{u}(\mathbf{x}, t), \mathbf{x}' - \mathbf{x}) dV_{\mathbf{x}'} + \mathbf{b}(\mathbf{x}, t)$$

- $\mathbf{f}(\boldsymbol{\eta}, \boldsymbol{\xi})$ is a pairwise force function, value is a force vector (force/volume²)
 - $(\boldsymbol{\xi} + \boldsymbol{\eta}) \times \mathbf{f}(\boldsymbol{\eta}, \boldsymbol{\xi}) = 0$ and $\mathbf{f}(-\boldsymbol{\eta}, -\boldsymbol{\xi}) = -\mathbf{f}(\boldsymbol{\eta}, \boldsymbol{\xi})$
- where, $\boldsymbol{\xi} + \boldsymbol{\eta}$ is current relative position vector between particles

Example, Prototype micro-elastic brittle (PMB)

- Force density described as ,

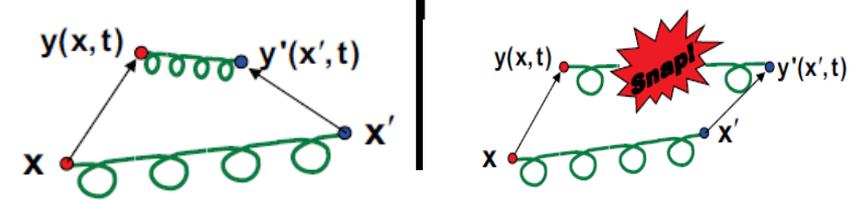
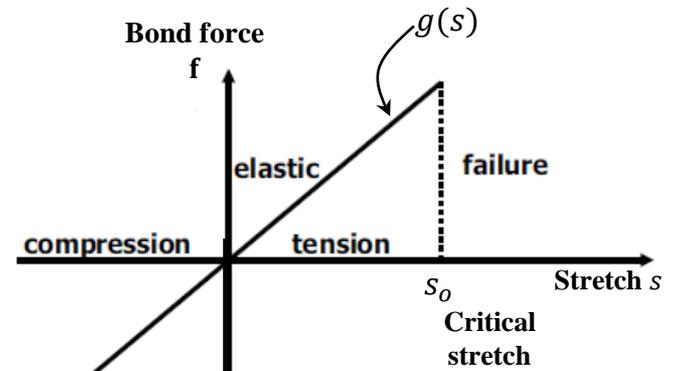
$$\mathbf{f}(\boldsymbol{\eta}, \boldsymbol{\xi}) = \mathbf{g}(\boldsymbol{\eta}, \boldsymbol{\xi}) \frac{\boldsymbol{\eta} + \boldsymbol{\xi}}{|\boldsymbol{\eta} + \boldsymbol{\xi}|},$$

where, $\mathbf{g}(\boldsymbol{\eta}, \boldsymbol{\xi}) = \begin{cases} c s(t, \boldsymbol{\eta}, \boldsymbol{\xi}) \boldsymbol{\mu}(t, \boldsymbol{\eta}, \boldsymbol{\xi}) & , |\boldsymbol{\xi}| \leq \delta, \\ 0 & , |\boldsymbol{\xi}| > \delta. \end{cases}$

c = stiffness of material

$s = \frac{|\boldsymbol{\eta} + \boldsymbol{\xi}| - |\boldsymbol{\xi}|}{|\boldsymbol{\xi}|}$ is bond strain

$$\boldsymbol{\mu}(t, \boldsymbol{\eta}, \boldsymbol{\xi}) = \begin{cases} 1 & \text{unbroken bonds} \\ 0 & \text{broken bonds} \end{cases} .$$



PMB material model

Peridynamic Material Models : State based

◆ State based PD model

- Generalized PD model, admits materials with any Poisson ratio.
(PMB materials have Poisson ratio of ¼ only)
- Each bond force depends on collective deformation of all bonds within the horizon, i.e., Forces within each bond are not independent

$$\rho(\mathbf{x})\ddot{\mathbf{u}}(\mathbf{x}, t) = \int_{\mathcal{H}_{\mathbf{x}}} \{ \underline{\mathbf{T}}[\mathbf{x}, t] \langle \mathbf{x}' - \mathbf{x} \rangle - \underline{\mathbf{T}}[\mathbf{x}', t] \langle \mathbf{x}' - \mathbf{x} \rangle \} dV_{\mathbf{x}'} + \mathbf{b}(\mathbf{x}, t)$$

$\underline{\mathbf{T}}$ is a force state vector material point in reference configuration

$\underline{\mathbf{T}}[\mathbf{x}, t] \langle \cdot \rangle$ is a mapping of $\mathbf{x}' - \mathbf{x}$ to a force vector field

$\mathbf{x}' - \mathbf{x}$ is the bond between displacement point \mathbf{x} and \mathbf{x}'

- PD state are continuum equivalent of multibody potentials (like EAM) of classical particle mechanics

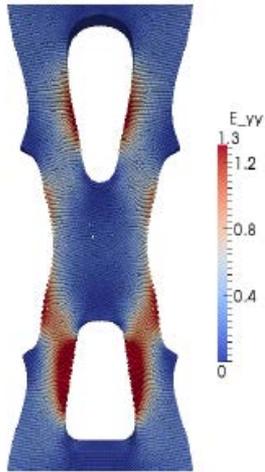
◆ Linear Peridynamic solid

$$\rho(\mathbf{x})\ddot{\mathbf{u}}(\mathbf{x}, t) = \int_{\mathcal{H}_{\mathbf{x}}} \mathbb{C}(\mathbf{x}' - \mathbf{x})(\eta' - \eta) dV_{\mathbf{x}'} + \mathbf{b}(\mathbf{x}, t)$$

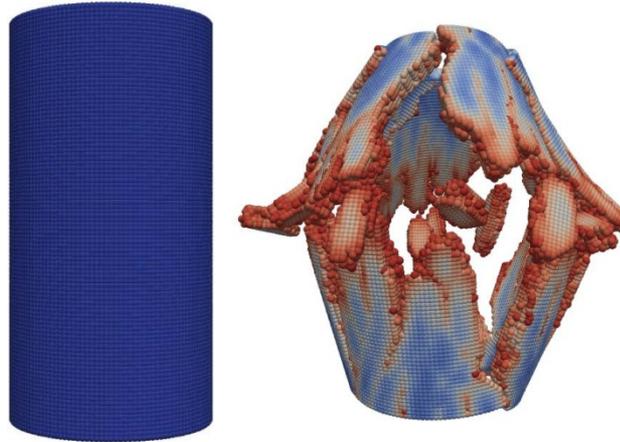
- $\mathbb{C}(\mathbf{x}' - \mathbf{x})$ is micromodulus function

What can Peridynamics model?

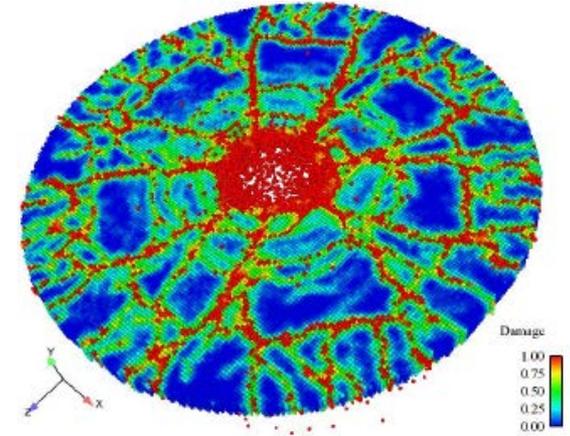
- ◆ Crack propagation and fracture failure



Necking under uniaxial tension [Littlewood et al.]



Cylinder before and after fragmentation simulated using PERIDIGM [Parks et al.]



Fracture patterns in a disc after impact with a hard ball, simulated using PD LAMMPS [Seleson et al.]

- ◆ Failure of composite laminate
- ◆ Fatigue failure
- ◆ Transient heat conduction
- ◆ Electromigration
- ◆ Corrosion, Corrosion Fatigue modeling ← ACT's work

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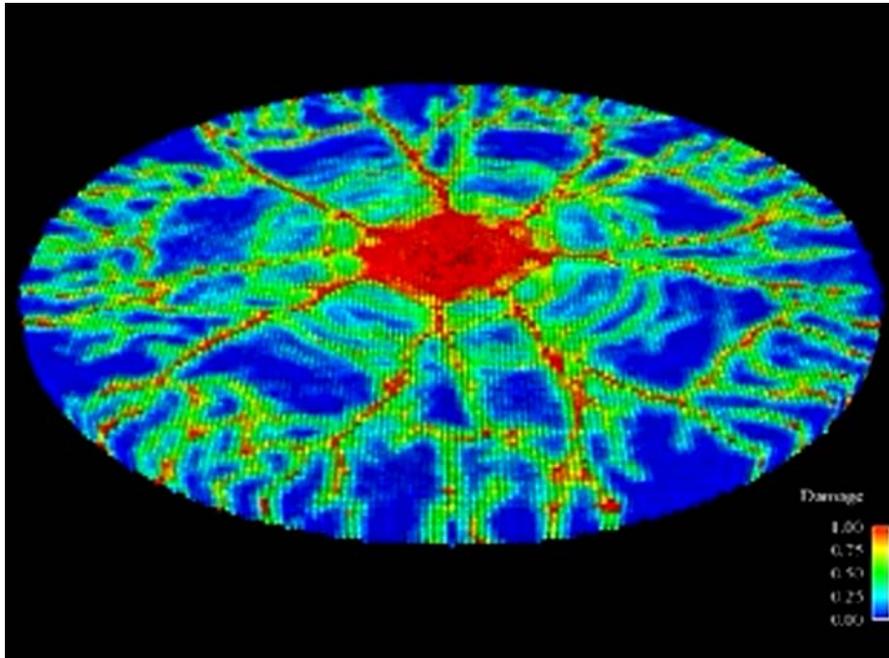
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- ◆ Some Slides removed for proprietary content

- ◆ Evolution of fracture patterns in a disc after impact with a hard ball (ball not shown for clarity)



disc.mp4

- ◆ Video credit : Pablo Seleson, University of Texas (work done during PhD with Prof. Gunzburger, Florida State Univ.)

- ◆ The peridynamics approach automatically enables simulation of cracks propagation and failure, without the need for complicated crack path algorithms like that of XFEM or cohesive element method.
- ◆ We developed a peridynamics framework for multiple applications:
 - Modeling corrosion damage phenomena mechanistically, taking into account material weakening due to pitting.
 - Modeling crack propagation in composites, taking into account the degradation of composites
 - Brittle fracture
- ◆ Corrosion test cases: illustrate capture of pit nucleation, growth and coalescence phenomena, both with and without manifestation of stress.
- ◆ Composite crack propagation cases: illustrates the failure propagation in composites under tensile loads.
- ☞ Peridynamics based damage modeling tools provide a framework for physics-based prediction, prognostics and maintenance in different applications.



Thank you



- ◆ Our modeling services include:
 - Modeling of crack propagation and damage using meshless (peridynamics methods)
 - Damage propagation and failure in composites
 - Corrosion damage and fatigue modeling
 - Modeling multiphysics of semiconductors and battery materials Combustion modeling
 - Modeling hypersonic phenomena
 - Computational chemistry and chemical kinetics

- ◆ We provide/develop custom modeling capabilities for all the above applications.

- ◆ Contact us:

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