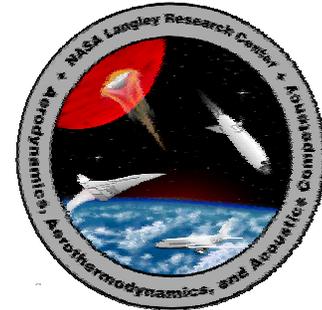


TFAWS AUGUST 2003 VULCAN CFD CODE OVERVIEW / DEMO

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**Hypersonic Airbreathing
Propulsion Branch**





VULCAN DEVELOPMENT HISTORY

- Evolved from the LARCK code development project (1993-1996).
 - LARCK developed as a cell-centered, finite volume, multi-block multi-grid, code to solve the full Navier-Stokes equations for turbulent non-equilibrium chemically reacting flows to replace SPARK.
 - Assumed PDF turbulent chemistry models developed and added.
- VULCAN was created from LARCK as part of a RAM/SCRAMJET CFD code development project conducted under contract to the Air Force Research Lab, Propulsion Directorate, at Wright Patterson Air Force Base (1996-1997).
 - Multi-region domain decomposition paradigm added.
 - Space Marching scheme added.
 - Wall matching (wall functions) added.
- VULCAN code and algorithm development continued by Hypersonic Airbreathing propulsion branch (1997-2003).
 - Space marching with multi-grid and sub-stepping developed.
 - Turbulent model options expanded (Wilcox, EARS, etc.).
 - Graphical User interfaces developed.
 - Parallel processing version (MPI) developed.
 - Non-C(0) block-to-block interface capability added.
 - LES scheme added by AFRL WPAFB.
 - New chemical kinetic and turbulent chemistry models added.



GOVERNING EQUATIONS AND SOLUTION METHODS

- Solve the equations governing 2-D, axisymmetric or 3-D calorically perfect or thermally perfect non-equilibrium chemically reacting flows.
 - Structured grid, cell centered, finite volume, density based method.
 - Inviscid fluxes computed to 2nd order accuracy using vanLeer's MUSCL scheme with either of:
 - flux difference split scheme of Phil Roe, or the
 - low dissipation flux split scheme of Jack Edwards
 - Viscous fluxes computed to 2nd order accuracy using either a
 - thin layer gradient construction (ignores cross derivatives)
 - full gradient construction (includes cross derivatives)
- Solve the full spatially elliptic Euler or full Navier-Stokes equations by integrating the conservative form of the unsteady equations in real or pseudo-time.
- Solve the spatially hyperbolic Euler or parabolized Navier-Stokes equations by integrating the conservative form of the unsteady equations in pseudo-time.



DOMAIN DECOMPOSITION METHODOLOGY

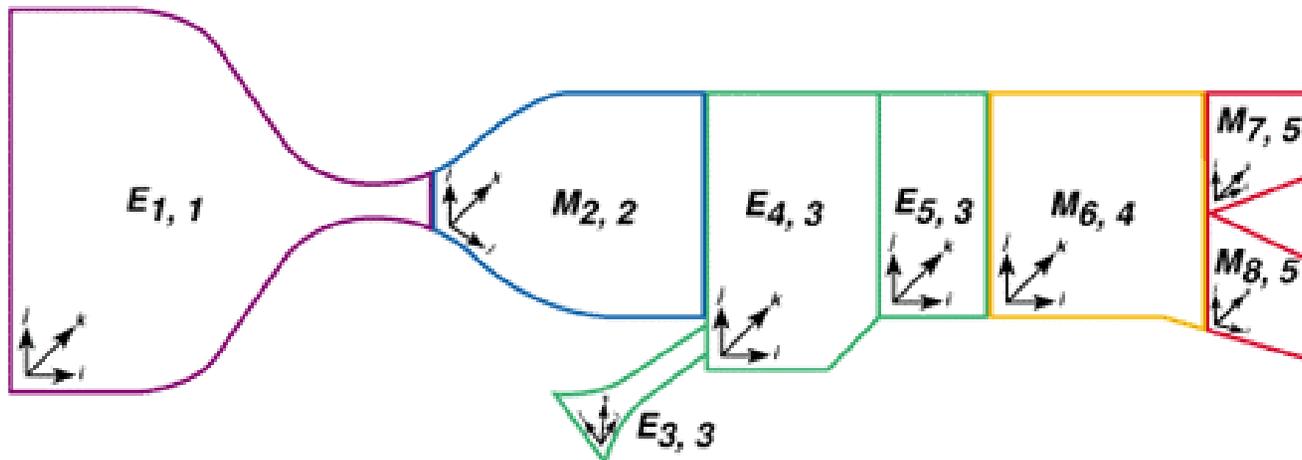
- Four level hierarchy of domain decomposition.
 - Structured grid cell : a six sided finite volume.
 - Structured grid block : an $I_{max} \times J_{max} \times K_{max}$ group of cells.
 - Structured grid region : a group of blocks solved together.
 - Structured grid computational domain : Sum of all cells, blocks and regions.
- The no. of governing equations is consistent across all cells in the computational domain.
- The no. and order of the chemical species is consistent across all cells in the computational domain.
- The thermodynamic and transport models are consistent across all cells in the computational domain.
- Turbulence models can be turned on or off at the block level.
- Chemical reaction models can be turned on or off at the block level.



DOMAIN DECOMPOSITION METHODOLOGY

Computational domain decomposition rules

- 1- **Block:** A logical i, j, k group of grid nodes or cells
- 2- **Region:** A group of blocks solved simultaneously using a common algorithm;
 - a) **Spatially elliptic:** $E_{B, R}$; Solve block B in region R using an elliptic algorithm
 - b) **Spatially marched:** $M_{B, R}$; Solve block B in region R using a space marching algorithm



- 3- Regions are solved in ascending order
- 4- Marching blocks that connect across block i -faces **MUST** be in different regions
- 5- Marching blocks can be marched in the i -direction **ONLY!**



THERMODYNAMIC AND TRANSPORT MODELS

- Thermodynamic properties are modeled either as
 - Single component calorically perfect gas (constant C_p)
 - Arbitrary mixture of thermally perfect gases where
 - Curve fits of C_p , enthalpy, and Gibbs free energy are obtained from a species curve fit data base provides with VULCAN
 - Curve fits are provided for selected species using either
 - Single interval 7th order curve fit (300-6000 Kelvin range)
 - Two interval 7th order curve fit (300-6000 Kelvin range)
 - Three interval 9th order curve fit (200-20,000 Kelvin range)
- Transport properties (molecular viscosity, thermal conductivity) using
 - Sutherland's law for the molecular viscosity and constant Prandtl no. for the thermal conductivity of a single component calorically perfect gas.
 - Sutherland's law for species molecular viscosity with Wilke's law for the mixture molecular viscosity.
 - Sutherland's law for species molecular conductivity with Wassileja's for the mixture molecular conductivity.



CHEMICAL KINETIC MODELS

- Species production/destruction computed using law of mass action.
 - Reaction model data base provided where reactions are specified in equation form.
 - A 3 step - 6 specie ethylene mechanism would look like
 - ‘ $\text{C}_2\text{H}_4 + \text{O}_2 \rightleftharpoons 2\text{CO} + 2\text{H}_2$ ’
 - ‘ $2\text{CO} + \text{O}_2 \rightleftharpoons 2\text{CO}_2$ ’
 - ‘ $2\text{H}_2 + \text{O}_2 \rightleftharpoons 2\text{H}_2\text{O}$ ’
 - Reaction equations can be specified as bi-directional
 - ‘ $\text{C}_2\text{H}_4 + \text{O}_2 \rightleftharpoons 2\text{CO} + 2\text{H}_2$ ’
 - and/or specified as uni-directional.
 - ‘ $\text{C}_2\text{H}_4 + 2\text{O}_2 \Rightarrow 2\text{CO} + 2\text{H}_2\text{O}$ ’
- Forward chemical reaction coefficients are modeled using Arrhenius model.

$$k_f = A T^B e^{(-T_a/T)}$$

- Backward chemical reaction coefficients modeled using either an
 - Arrhenius model or an
 - equilibrium model $k_b = k_f / k_e$
 - Third body efficiencies are modeled / specified for each individual third body reaction.
- Global reaction rate models using an arbitrary reaction order method. **(NEW)**



MEAN FLOW TURBULENCE MODELS

Momentum and energy turbulence effects are modeled using two-equation turbulence models which solve for :

- Turbulent kinetic energy
- Dissipation related variable
 - dissipation rate of turbulent kinetic energy (epsilon) or
 - specific dissipation rate of turbulent kinetic energy (omega)
- The Reynolds stresses present in the mean flow equations and the production terms of the two-equation models are consistently modeled using either a
 - Boussinesq model or a
 - Explicit algebraic stress model (Gatski-Speziale).
- A new two-equation turbulent scalar diffusion model for thermal diffusion is currently under development through a NGLT grant. **(NEW)**



MEAN FLOW TWO-EQUATION TURBULENCE MODELS

- k-epsilon based models
 - Low Reynolds no. wall integration model of Abid.
 - Explicit algebraic Reynolds stress model of Gatski and Speziale.
- k-omega based models
 - Wilcox's 1998 family of models
 - High Reynolds no. wall integrable model
 - High Reynolds no. with wall matching functions
 - Low Reynolds no. wall integrable model
 - Explicit algebraic Reynolds stress wall integrable model
 - Explicit algebraic Reynolds stress with wall matching functions
 - Menter's family of models
 - Baseline high Reynolds no. wall integrable model
 - Baseline high Reynolds no. model with wall matching functions
 - Shear stress transport (SST) high Reynolds no. wall integrable model
 - Shear stress transport (SST) high Reynolds no. with wall matching functions



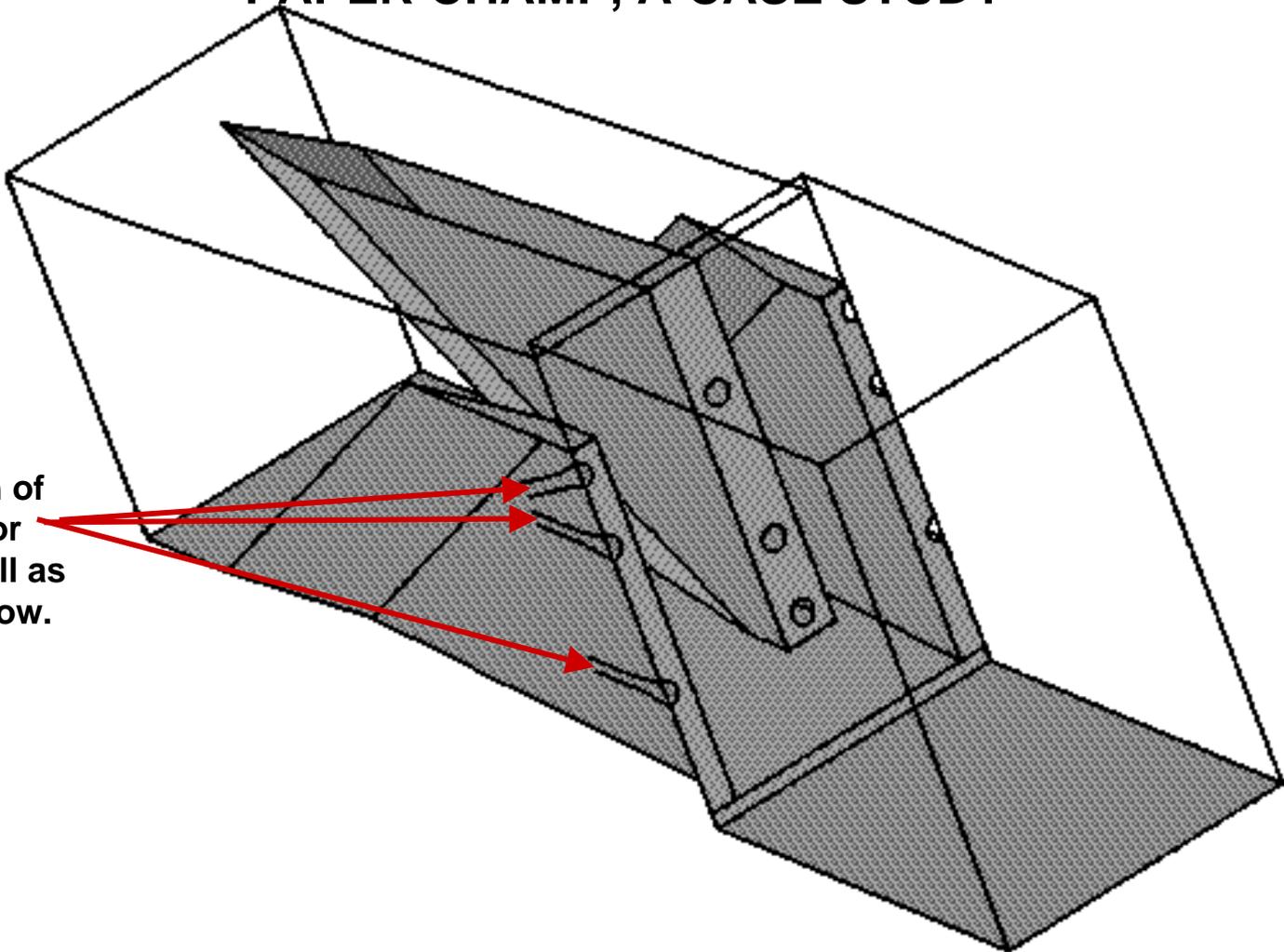
WILCOX WALL MATCHING FUNCTIONS

- Wall matching functions are:
 - Corrected for the streamwise pressure gradient effects.
 - Corrected for compressibility effects (vanDriest II).
 - Blended with the high Reynolds no. solve-to-wall method for $y^+ < 10$.
 - Solved iteratively using Newton's method.
- Wall matching functions are solved to provide:
 - The wall shear stress magnitude.
 - The wall heat flux magnitude.
 - Solution to the k and ω equations at the first cell center off the wall.
- Wall matching functions can be:
 - Used on the coarse and/or fine grids.
 - Used on any subset on a boundary face.
 - Mixed with with solve-to-wall boundary conditions.



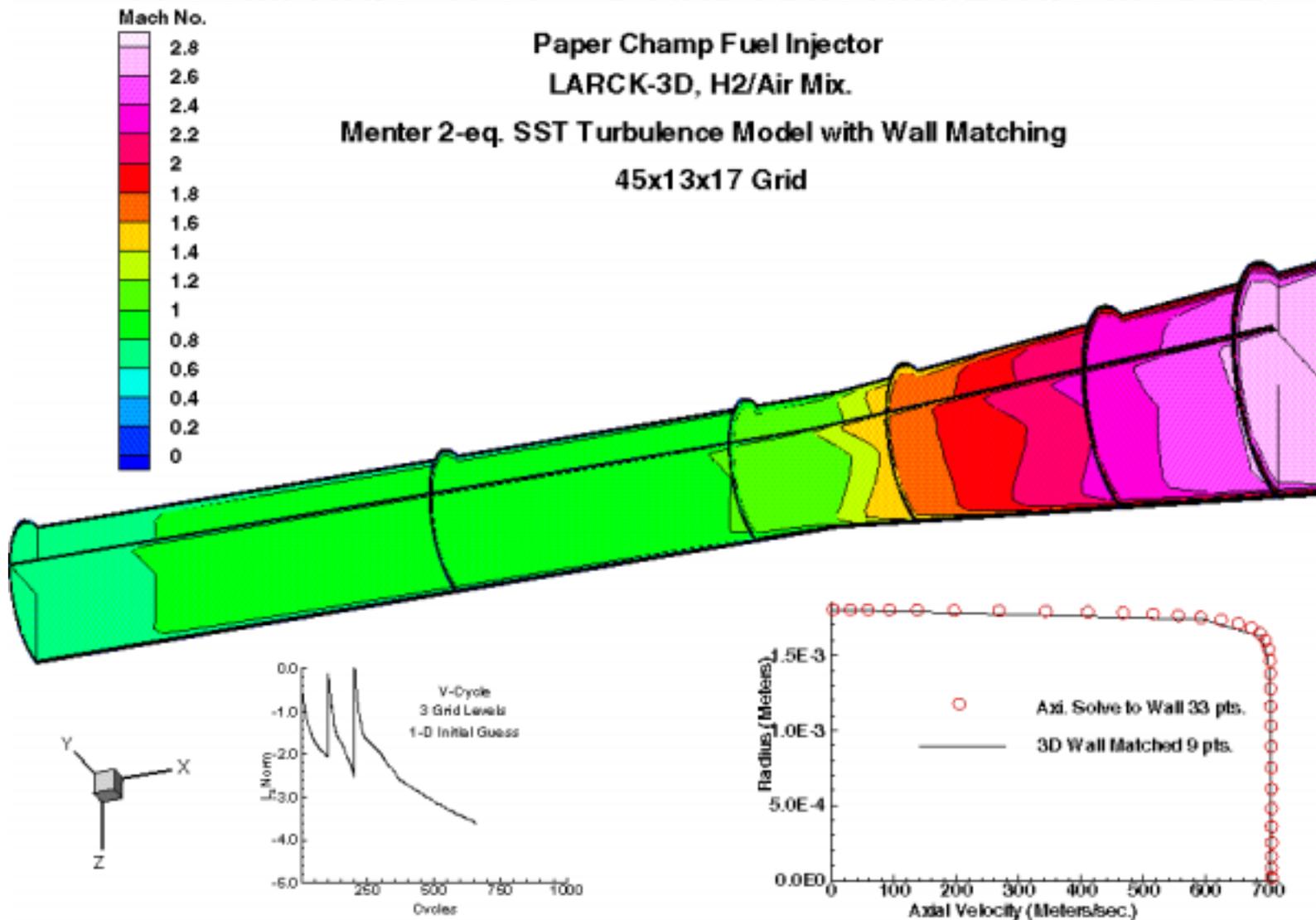
FIDELITY OF WALL MATCHING FUNCTIONS: PAPER CHAMP, A CASE STUDY

Objective:
Simulation of
fuel injector
flow as well as
passage flow.



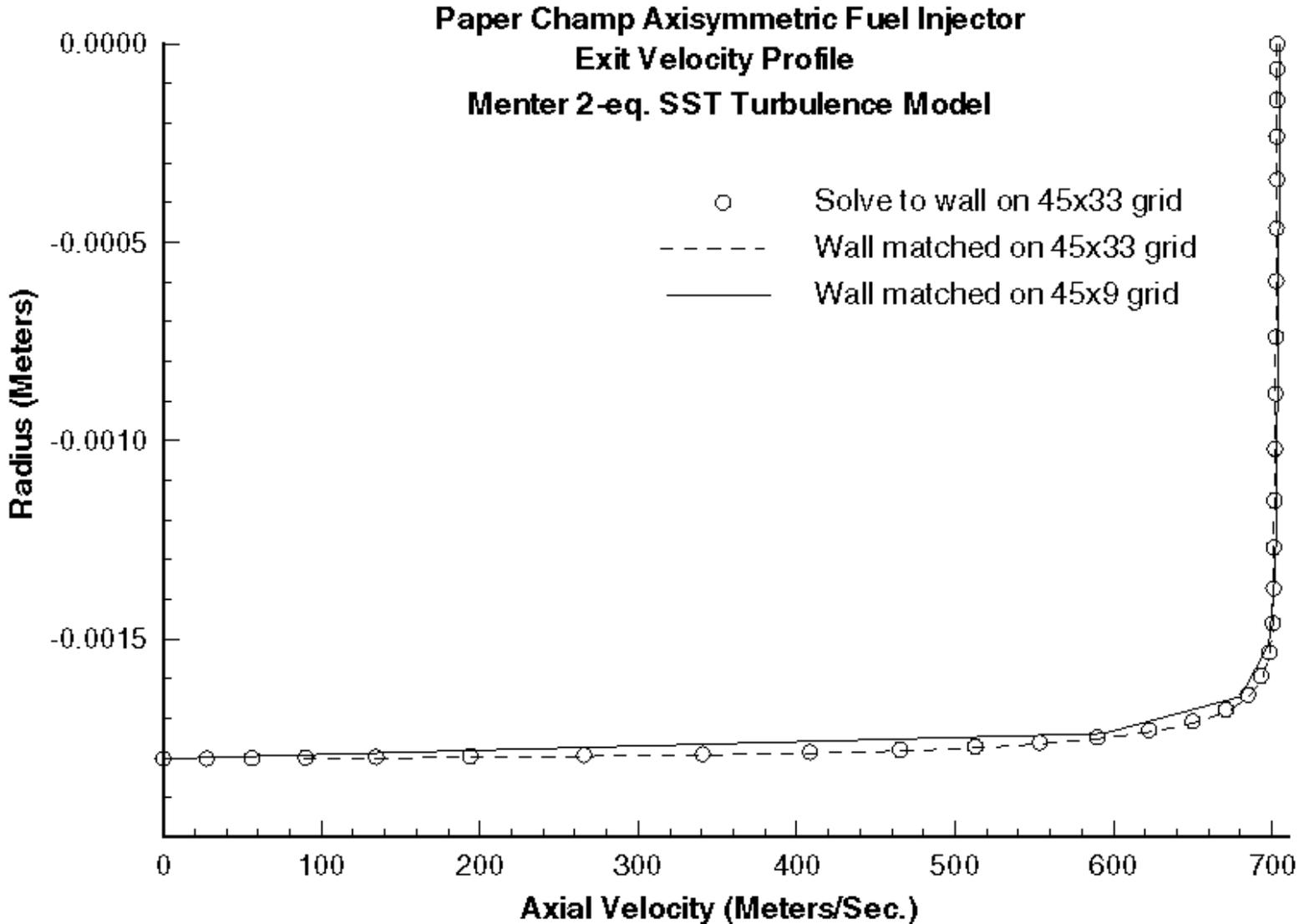


PAPER CHAMP FUEL INJECTOR SIMULATION STUDY : A COMPARISON OF 3-D AND AXISYMMETRIC MODELS



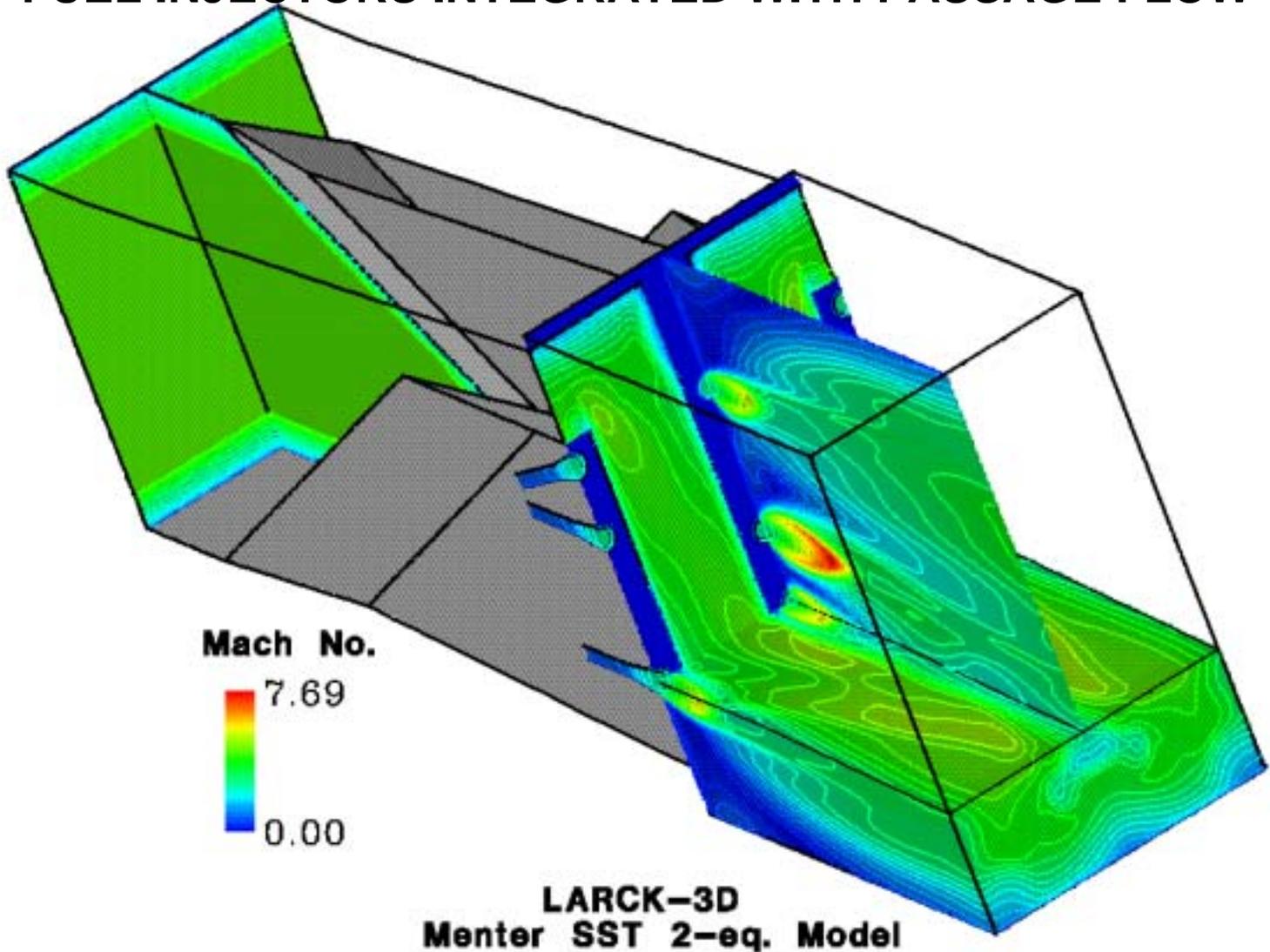


PAPER CHAMP FUEL INJECTOR SIMULATION STUDY : A COMPARISON OF WALL TREATMENT AND GRID RESOLUTION





PAPER CHAMP FUEL INJECTOR SIMULATION STUDY : FUEL INJECTORS INTEGRATED WITH PASSAGE FLOW





CHEMISTRY TURBULENCE MODELS

Turbulence interactions with the chemical kinetics are modeled using either mixed is burned or variance+PDF models :

- Mixed is burned model based on the eddy dissipation concept of Magnussen et. al. **(NEW)**
- Chemistry turbulence models (turbulent species production/destruction) are currently modeled as de-correlated.
 - Energy variance + a scalar assumed Beta Probability Density Function (PDF) for the effect of temperature fluctuations on the reaction rate coefficients (k_f and k_b)
 - Sum of species variance + multivariate assumed Beta PDF for the effect of the species fluctuations on the species production/destruction.
- A new two equation turbulent scalar diffusion model for species diffusion is currently under development through a NGLT grant. **(NEW)**



TIME/SPACE INTEGRATION ALGORITHMS

- Spatially and temporally explicit schemes:
 - Second order time accurate Runge-Kutta scheme (global time step).
 - Steady state Runge-Kutta scheme (local time step) with or without residual smoothing.
- Spatially and temporally implicit schemes:
 - Steady state diagonalized approximate factorization (local time step DAF).
 - Steady state block approximate factorization (local time step BAF).
 - Steady state diagonally dominant alternating direction implicit (local time step DDADI).
 - Second order time accurate implicit dual time-stepping scheme using 2nd order backward temporal differences. **(NEW)**
 - Second order time accurate implicit dual time-stepping scheme using Crank-Nicolson method. **(NEW)**



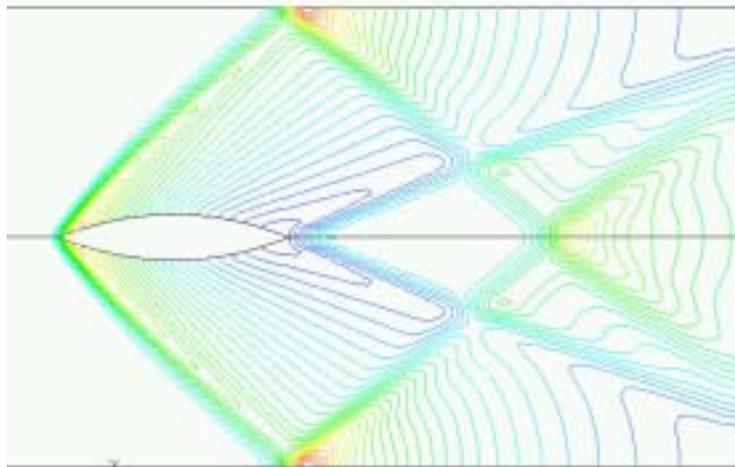
CONVERGENCE ACCELERATION

- Convergence acceleration can be accomplished using either:
 - Full coarsened coarse-to-fine grid sequencing:
 - Solve on a coarsened grid with a robust scheme (e.g. a 1st order scheme).
 - Interpolate from the coarsened grid to the next finer grid level and then solve.
 - Repeat until fine grid is reached and then switch to a higher order scheme.
 - Full coarsened V or W-cycle full approximate storage multi-grid (FAS).
 - Full coarsened full multi-grid (FMG : A combination of coarse-to-fine grid sequencing and V or W FAS)
- Coarse-to-fine sequencing works well for wide variety of flows.
- Multi-grid a good approach for elliptic flows only when computational grid is very fine.
- Coarse-to-fine sequencing and multi-grid have been found to work very well with space marching scheme.

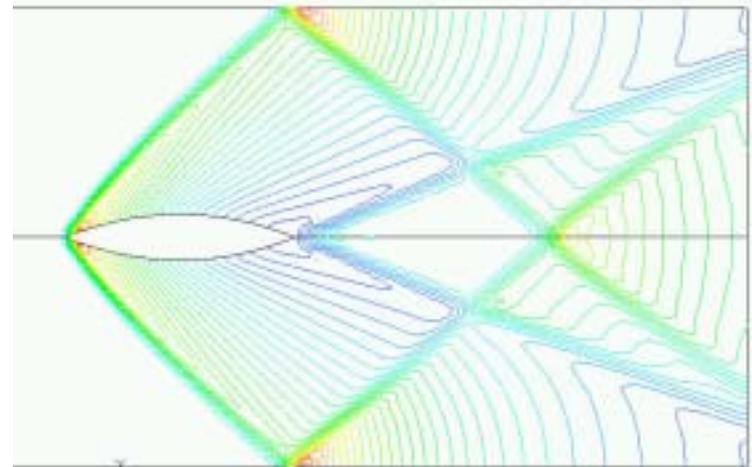


SUB-STEPPING FOR SPACE MARCHING

- Allows the user to linearly refine the grid in the marching direction without regenerating the grid.
- Can be used to help remove numerical oscillations in the space marching direction by either:
 - Reducing the size of the gradient used in the second order fully upwind flux construction.
 - Allow the user to switch to a 1st order fully upwind streamwise flux construction.



No Sub-stepping



Sub-stepping factor of 3



PHYSICAL AND INTRA-BLOCK CONDITIONS

- There are seventeen different types of boundary conditions implemented which:
 - Can be specified on any boundary or subset of a boundary.
 - Can be treated explicitly or implicitly (depending on time/space integration scheme used).
- There are two types of intra-block (block-to-block) boundary conditions:
 - CUTS : $C(0)$ (point wise continuous) block-to-block connectivity that:
 - Can be specified on any boundary or subset of a boundary.
 - Are fully second order accurate when grid is smooth.
 - Are fully conservation preserving when flux telescopes.
 - PATCHES : Non- $C(0)$ (point wise discontinuous) block-to-block connectivity that:
 - Can be specified on any boundary or subset of a boundary.
 - Are fully second order accurate when grid is smooth.
 - Are weakly conservative.

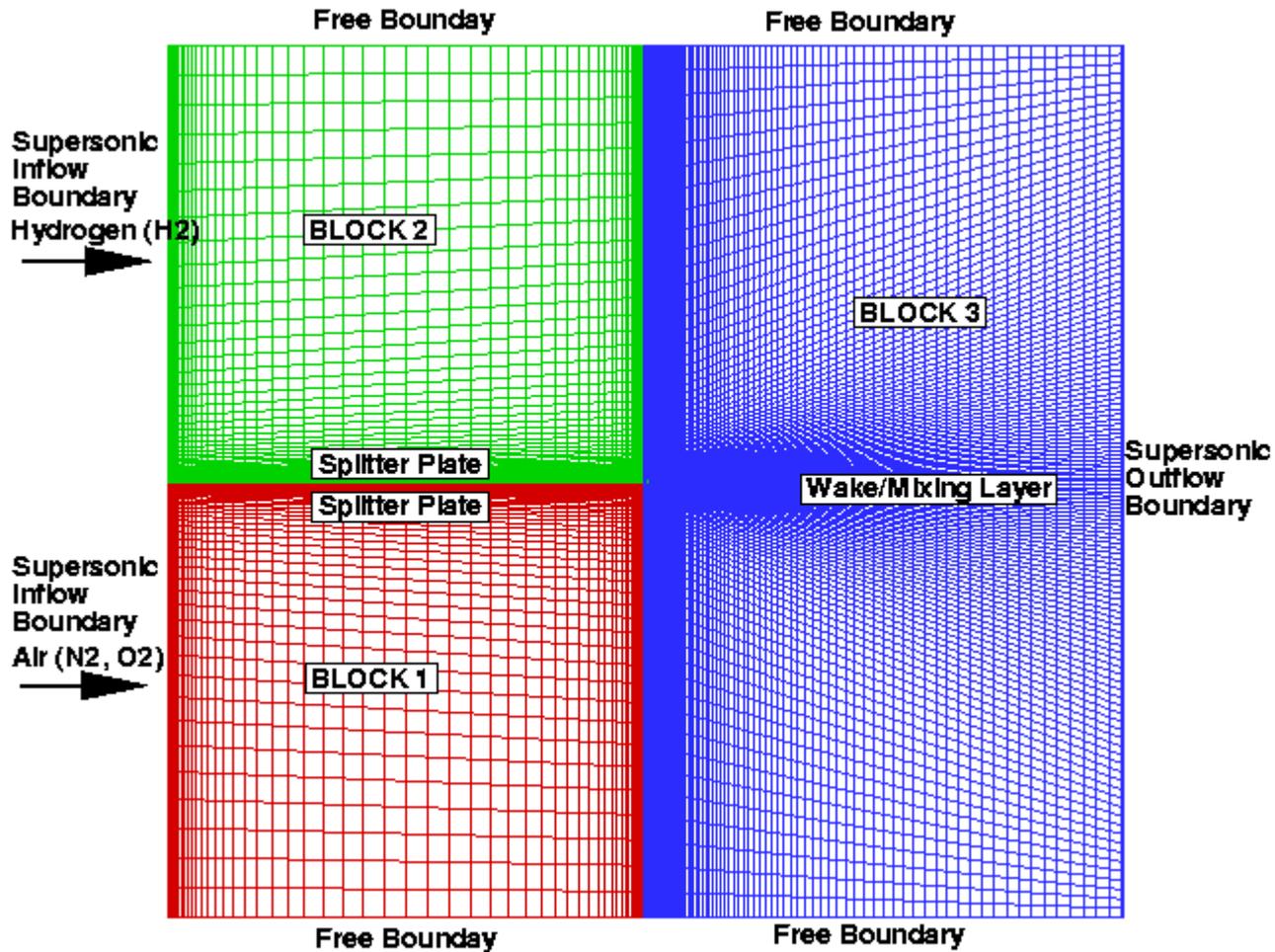


FLOW INITIALIZATION

- Experience has shown that as applications become more complex the initial guess plays an increasingly important role.
- There are seven different types of flow initialization methods implemented to provide flexibility in specifying the initial guess.
 - 1) The reference conditions are always used to set a default initialization of all cells in all blocks and regions.
 - 2) Initialization by propagation of physical boundary condition ghost cell data.
 - 3) Initialization by propagation of 'INITIAL' boundary condition ghost cell data (these b.c. are ignored during solution process).
 - 4) Initialization by a 'BLEND'ed propagation of any boundary condition ghost cell data.
 - 5) Initialization by propagation of CUT ghost cell data.
 - 6) Initialization by propagation of PATCH ghost cell data.
 - 7) C-D nozzle one-dimensional initialization.

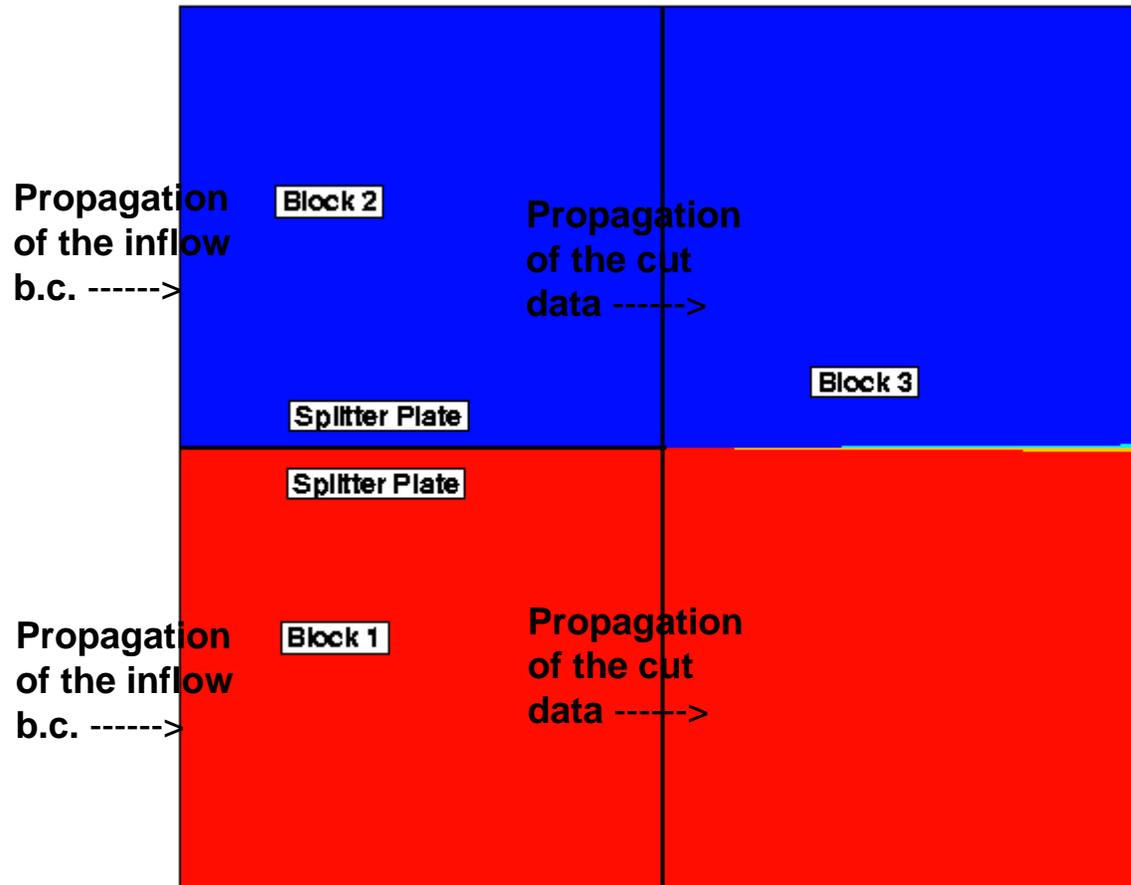


FLOW INITIALIZATION EXAMPLE (PROPAGATE)





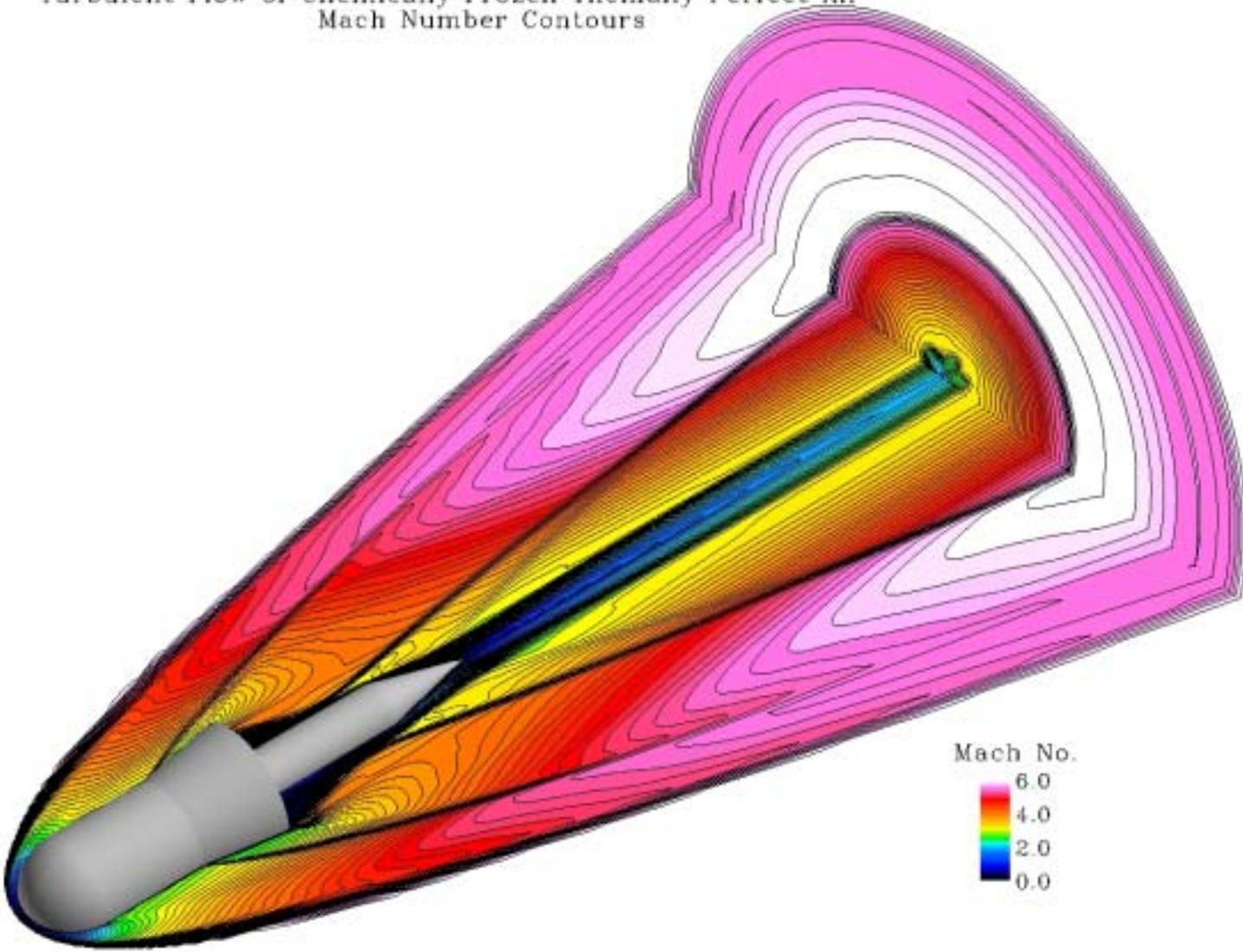
FLOW INITIALIZATION EXAMPLE (PROPAGATE)





FLOW INITIALIZATION EXAMPLE (BLENDing)

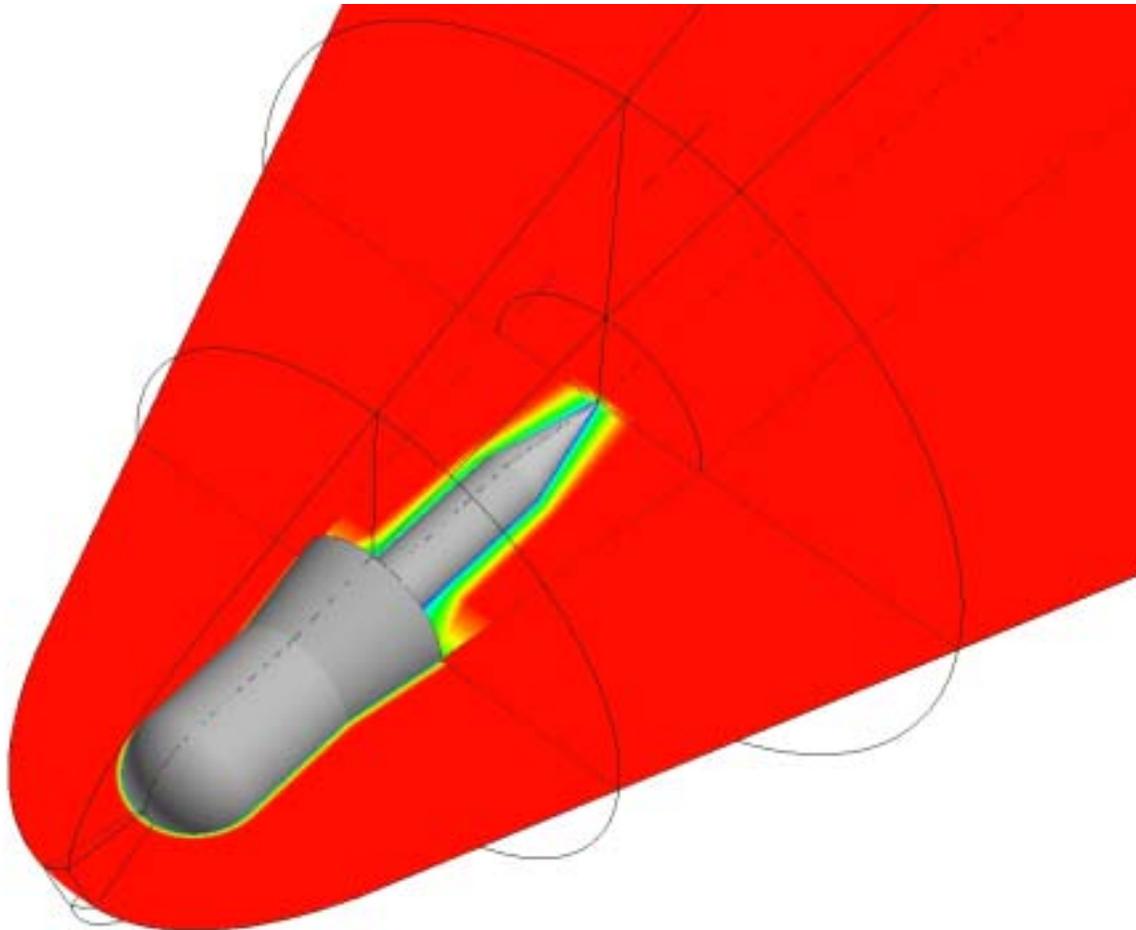
Hypersonic Projectile at Mach 6
Turbulent Flow of Chemically Frozen Thermally Perfect Air
Mach Number Contours





FLOW INITIALIZATION EXAMPLE (BLENDing)

Mach 6 Projectile





LAMINAR AND IGNITION SUB-BLOCKS

- Laminar sub-block are a group of cells within a block for which the turbulent source terms are turned off.
- This is done in such a manner that the code:
 - Passively advects the inflow turbulence b.c.'s. and resets the turbulence eq. wall b.c.'s in the sub-block.
 - Provides a way to control where flow becomes turbulent.
- Ignition sub-blocks are a group of cells within a block where a minimum user specified static temperature is enforced.
- This is done in such a manner that the code:
 - Adds energy to the flow in the sub-block.
 - Provides a way to “spark the flow” or force ignition when and where needed.



CODE INTERFACES AND POST-PROCESSING

- The VULCAN input file generation graphical user interface can read and extract two kinds of information from the Gridgen generic flow solver file.
 - Physical b.c.'s.
 - Intra-block C(0) connectivity data.
- The VULCAN post-processor writes I-blanked plot3d grid, and either Q or function files and a Fieldview name file.
- The VULCAN post-processor can be made to write out the conserved variables contained in the cells adjacent to a physical b.c. into a “profile file”.
 - Profile files can be read by VULCAN and treated as b.c.'s
 - Profile files can be used to provide data to external codes
- The VULCAN post-processor automatically integrates the forces, moments and heat loads of all “walls” and flow-thru b.c.'s in the computational domain and summarizes them by :
 - Each individual b.c. type (wall or flow-thru)
 - The sum of the each b.c. type in each block.
 - The sum of all b.c. types in the computational domain.
- The VULCAN post-processor automatically writes a file containing the y_+ of the 1st cell center off-the wall, the wall PdA components, shear force components, heat flux and cell face area of all wall b.c.'s to a file.



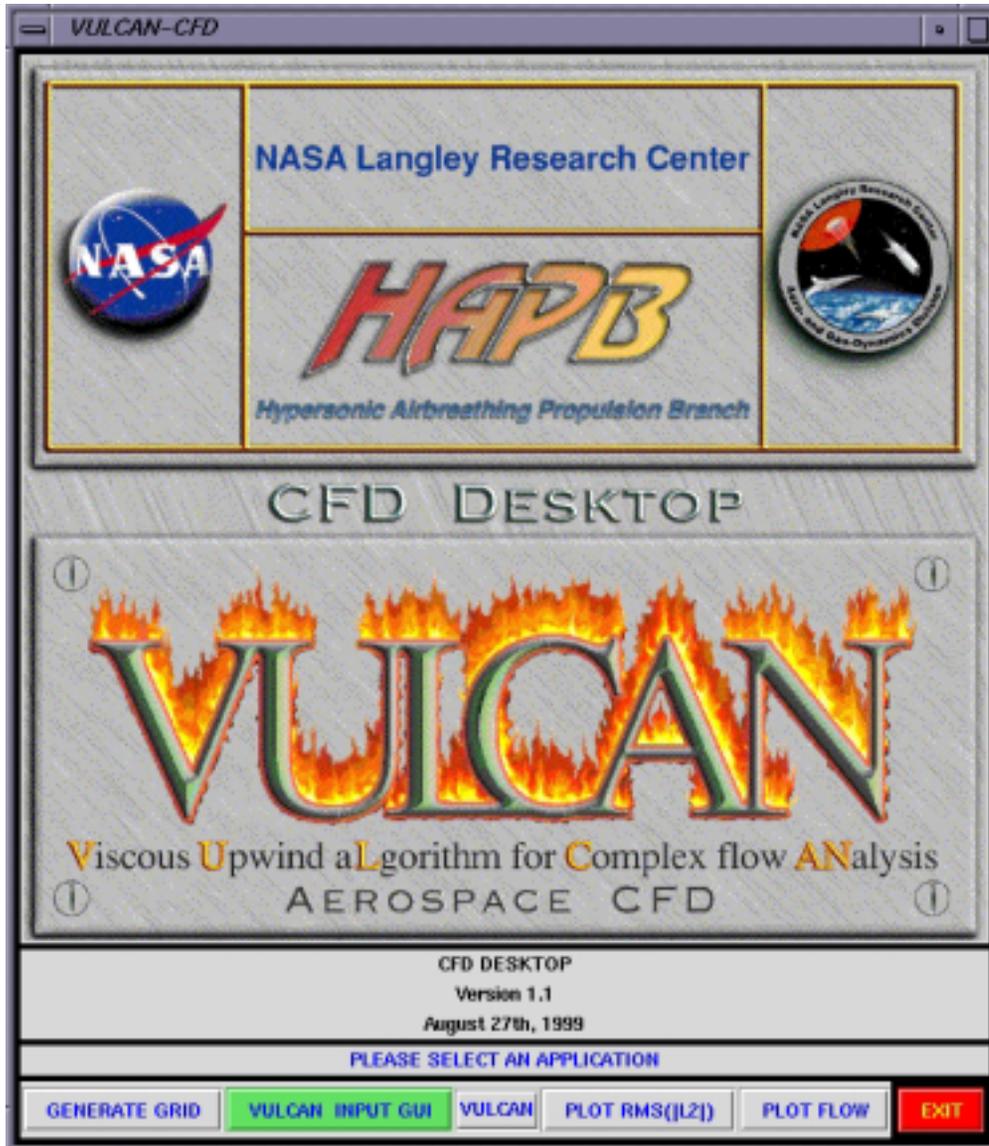
CODE GRAPHICAL USER INTERFACE (GUI)

Two **tcl/tk** based GUIs are supplied with VULCAN

- **VULCAN-CFD** : A desktop GUI to provide an API that connects the CFD process tools together,
 - Grid generation tool (Gridgen, ICEM, Tecplot, ...)
 - VULCAN input file GUI
 - VULCAN
 - Residual history plotting tool (Tecplot, ...)
 - Graphical Post-processor tool (FIELDVIEW, Tecplot, ICEM, ...)
- **VULCANIG** : An input file GUI/wizard to provide a quick way to create VULCAN input files with error checking and interfaces to Industrial grid generation codes for the importation of block connectivity and b.c. information.
 - Gridgen generic flow solver file importation.
 - ICEM VULCAN input file importation.



VULCAN-CFD



VULCANIG

