TFAWS Active Thermal Paper Session



CFD Analysis of Thermal Control System in NX Thermal & Flow

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Background



- Thermal Control System (TCS) provides thermal control, mainly cooling, to several Advanced Plant Habitat (APH) subsystems. One of these systems is the Environmental Control System (ECS), which provides temperature and humidity control inside the growth chamber to optimize plant growth.
- TCS consists of three cold plates that use Thermoelectric Coolers (TECs) to heat or cool a water loop as needed to meet ECS temperature requirements.



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Environmental Control System

Environmental Control System (ECS)



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Problem Statement



- Pressure drop and heat transfer analysis was performed to optimize the TCS design.
- Computational analysis was performed in Siemens NX Thermal/Flow.
 - Method 1: Uses NX Thermal only. Includes 3D mesh thermal solver and 1D duct network solver for fluid flow in pipes or tubes. This may include wall thickness (if desired).
 - Method 2: Uses NX Thermal/Flow, which includes 3D mesh thermal solver and 3D computational fluid dynamics (CFD) flow solver.
 - Both methods were used and the results will be compared in this presentation.

Method 1: 1D duct flow network analysis

- Models fluid region as onedimensional fluid duct.
 - Pressure
 - Velocity
 - Mass flow rate
 - Temperature
- 1D mesh
 - Fluid only
 - Fluid and tube wall
- Heat transfer (Thermal coupling)
 - Conduction, convection, radiation
 - Free, forced and user defined convection





Method 1: 1D duct flow network analysis

- Does not use NX Flow
 - Only NX Thermal is used
- Duct boundary conditions
 - Fan/pump
 - Opening
 - Pressure
 - Flow properties
 - Duct to 3D flow connection
 - Connects 1D duct to 3D CFD model





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Method 2: 3D CFD Analysis





3D mesh

- Structured hexahedral
 - Quad 2D face and sweep (manual)
- Unstructured tetrahedral
 - Either automatic or manual meshing
- Turbulent model
 - K-Omega
 - K-Epsilon
 - Mixing Length
 - LES
- Both NX Flow and Thermal
- Serial & Parallel processing

Method 2: 3D CFD Analysis



- Fully coupled pressure velocity scheme (parallel solver)
- All results converged for a steady state solution



Method 1: Duct Mesh Sizing



- Fluid and 3D thermal model for wall were tested
 - Tube used 0.075 inches element size
- 1D duct mesh (fluid)
 - 0.125 inches element size
- 1D duct mesh (tube wall)
 - 0.125 inches element size
- 3D tetrahedral cold plate mesh
 - 0.125 inches element size (0.395 inch recommended)
- Mesh sensitivity was tested at half and double of the element size and found that changing mesh size had no effect on the solution



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1D duct with wall

1D duct with 3D wall



Method 2: CFD Mesh Sizing

- Fluid mesh (3D tetrahedral)
 - 0.33 inch element size
 - wall functions were used so viscous sublayer did not need to be resolved
- Tube wall mesh (3D tetrahedral)
 - 0.075 inch element size (0.164 inch recommended)
- Cold plate mesh (3D tetrahedral)
 - 0.125 inches element size (0.395 inch recommended)
- Mesh sensitivity was tested by varying the mesh size and no effects to the solution was noticed

Method 2: CFD Mesh

- Inner layer
 - 1. Viscous sublayer
 - 2. Buffer layer
 - 3. Log-law region
- Goal was to keep mesh large enough so y+>30
 - Actual ranged 7.8 to 13.5





Method 2: CFD Mesh





Case Summary



- Used constant mass flow rate at
 - 50, 60, 70, 80, 90 and 100 lbm/hr
- IATCS fluid from ISS
 - Water was used in model
 - Initial temperature of water was 73.4 $^{\circ}\,\text{F}$
- TCUI TECs
 - 18 Watts of heating per TEC
- HCU TECs
 - 4.9 Watts of heating per TEC
- TCUF TECs
 - 6.1 Watts of cooling per TEC

Cold Plate Surface Temperature Results

Method 1

70

60

50

60

70

Mass Flow Rate (lbm/hr)

80

90

100

Method 2







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Method 1







Fluid Pressure Drop Results





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Method 1

Method 2

Conclusions



- Models produced similar fluid temperatures, but differed in pressure drop and surface temperature results.
- Testing sensitivity in Method 1 to convection coupling or Method 2 to turbulence model did not produce drastic changes
 - Grid size sensitivity also did not affect the solution
- Preliminary data from the integrated testing at Orbitec showed the CFD method was closer in actual pressure drop to prototype.
 - While CFD pressure drop analysis was closer to system pressure drop seen during testing, it was still 50% lower.
 - Analysis will need to be updated based on system changes during testing.
 - Currently no thermal data is available to correlate model to test data



Questions?

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