



## The Design and Aero Thermodynamic Analysis of An Inversely Derived Scramjet Configuration

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**TFAWS**  
JSC • 2018

Presented By  
**Dehua Feng**

Thermal & Fluids Analysis Workshop  
TFAWS 2018  
August 20-24, 2018  
NASA Johnson Space Center  
Houston, TX



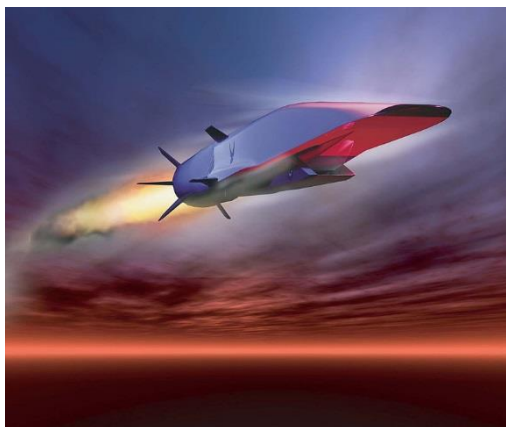
# Outline



- Introduction
- Morphing Scramjet Model-Two Phase Approach
  - Phase I: Forebody
    - 2D oblique shock theory
    - 2D - 3D transfer
    - Validation
    - Summary of forebody
  - Phase II: Aft-Body
    - Modified Quasi 1-D tool development
    - Validation of the Quasi 1-D tool
    - Configuration test
    - Configuration results
    - Proof of concept

## Taking Humans to Space

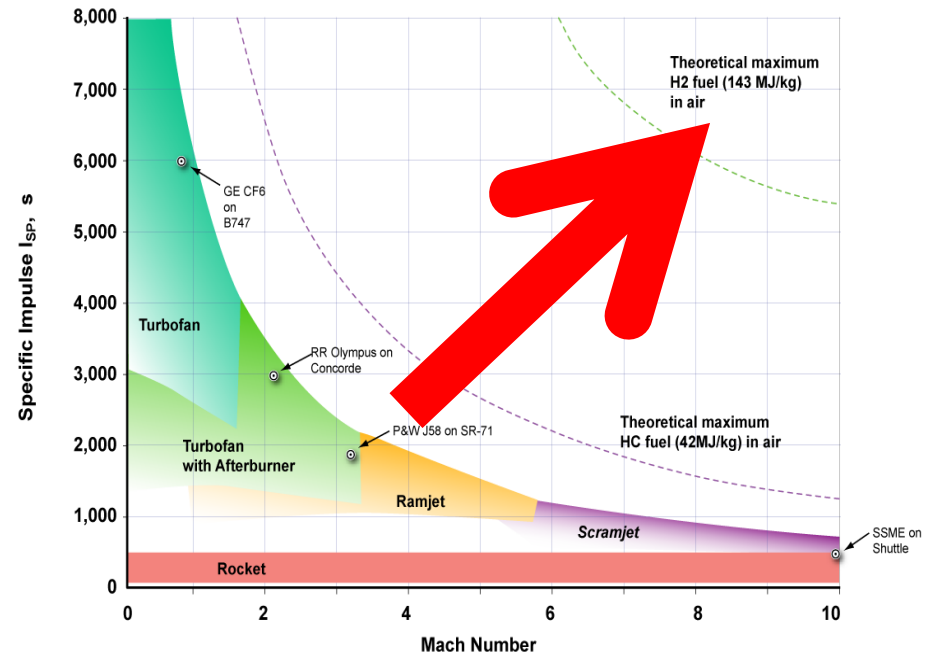
- US, China, India, Europe are creating & designing concepts
- In US, Several exists, at US Research Agencies & Academia
- Our Concept at NCAT!



NASA - <http://antwrp.gsfc.nasa.gov/apod/ap040329.html>

## NCAT Focus: Optimized Scramjet Engine

### Propulsion Performance



By Kashkhan - CC BY-SA 3.0,  
<https://upload.wikimedia.org/wikipedia/commons/4/4f/Specific-impulse-kk-20090105.png>

- Higher specific impulse than rocket engines
- Does not need to carry its own oxidizer
- Potential for high reusability and practicality over rockets

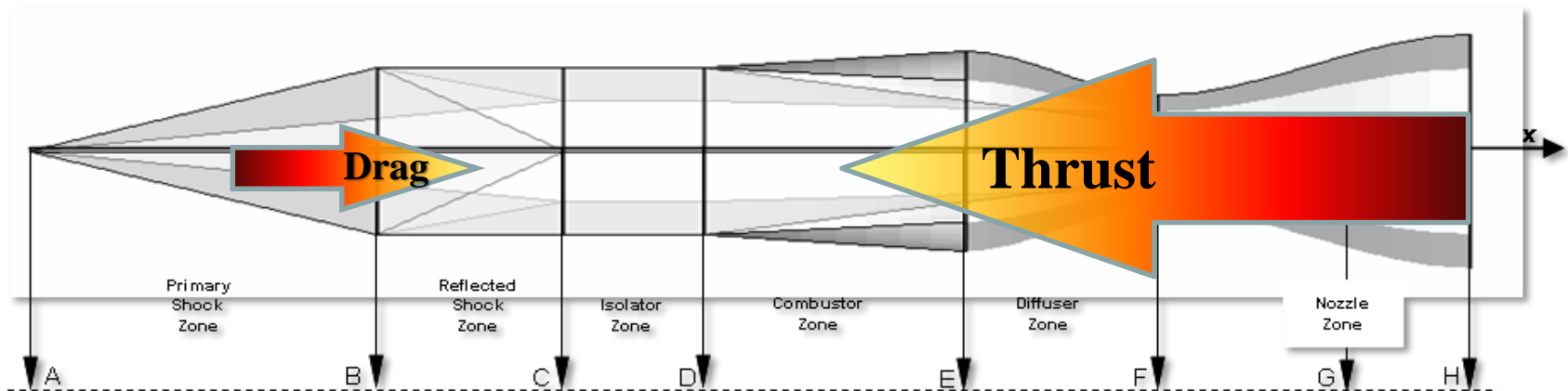
## My Research Approach

### 1. Create A 3D-Shape generator that incorporates

- i. Aerodynamically Coupled Forebody: Inlet-Isolator (Mach 3-8)
- ii. Oblique, Quasi-1D and Pseudo-Shock/Shock Train Relationships

### 2. Create An Internal 3D-Shape generator that incorporates

- i. Simplified Injector, mixing and combustor models
- ii. Quasi-1D (Mach 3 – 8) Aerodynamics/Combustor/Nozzle

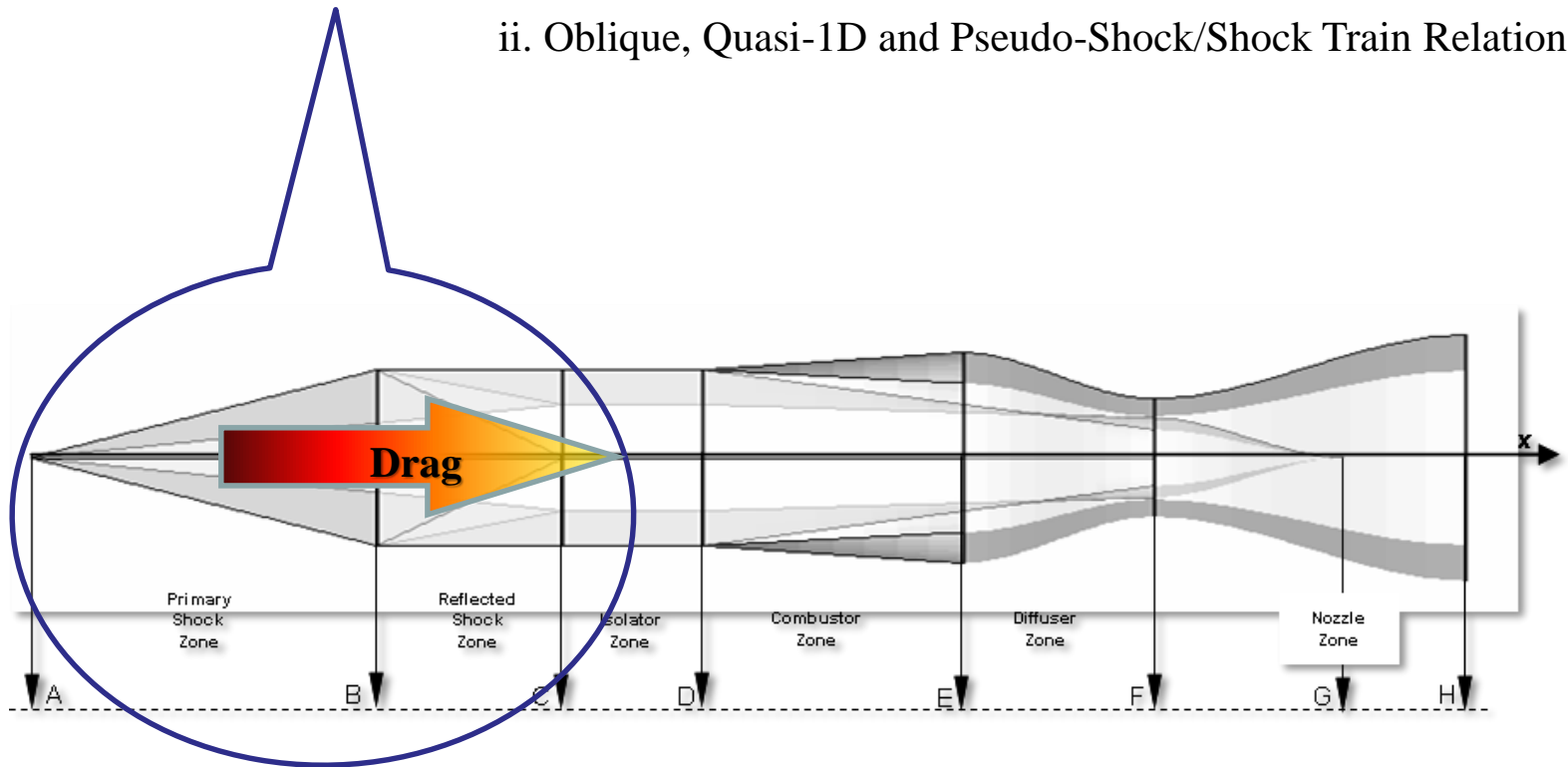


✓ **Optimized for Maximum ‘Thrust to Drag’ Ratio**

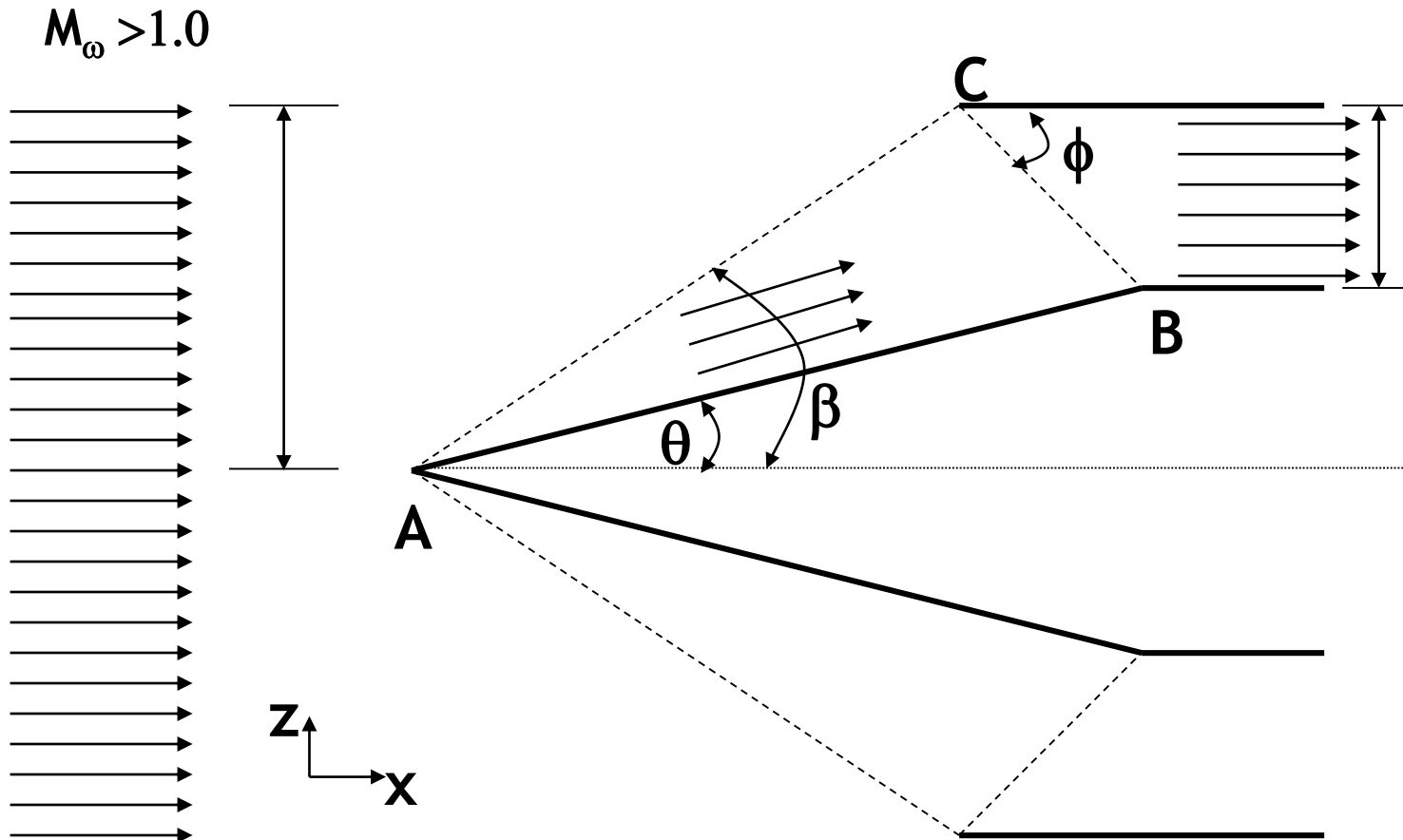
## The Conceptual Design Process

### 1. Create A 3D-Shape generator that incorporates

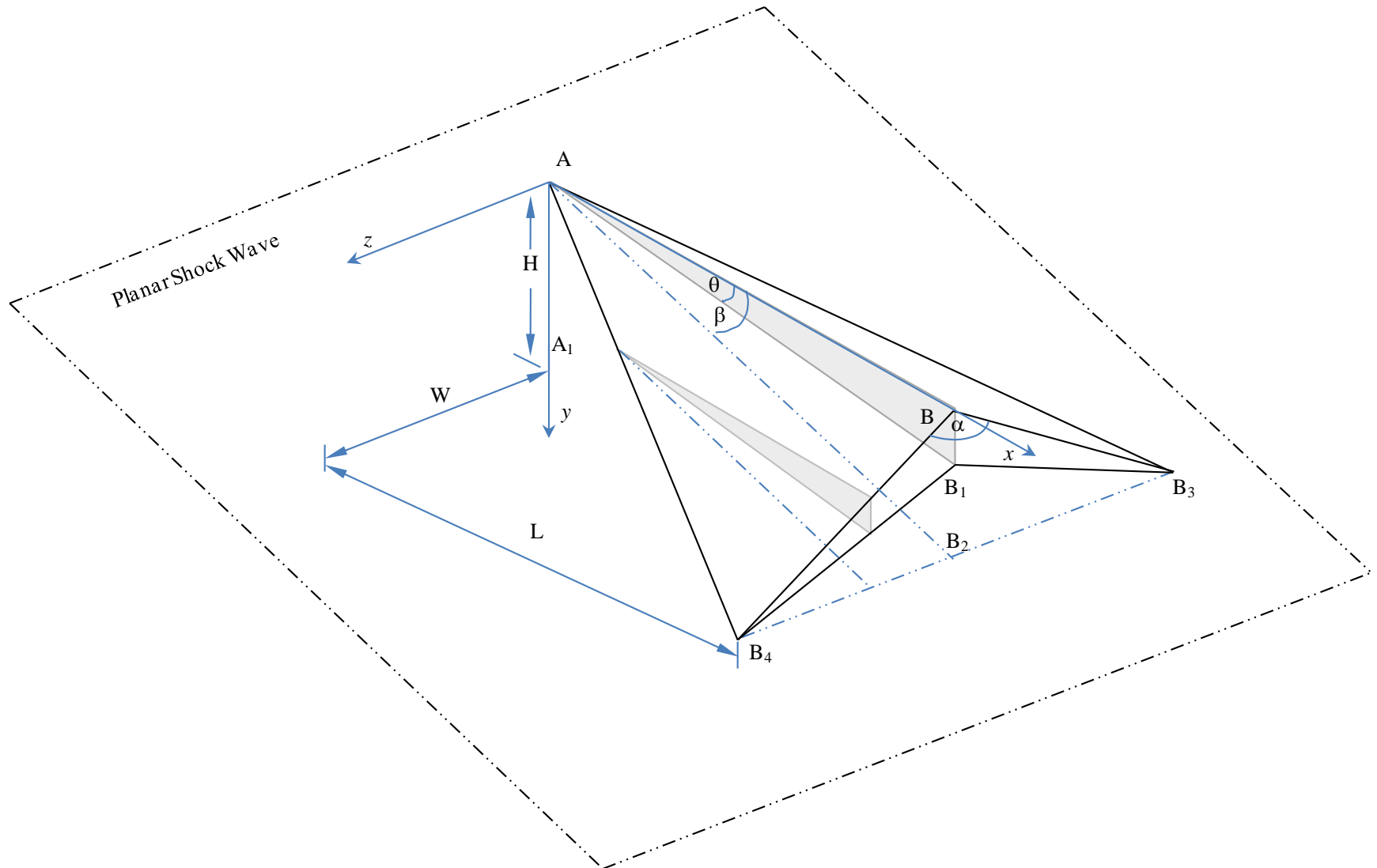
- i. Aerodynamically Coupled Forebody-Inlet-Isolator (M 3-8)
- ii. Oblique, Quasi-1D and Pseudo-Shock/Shock Train Relationships



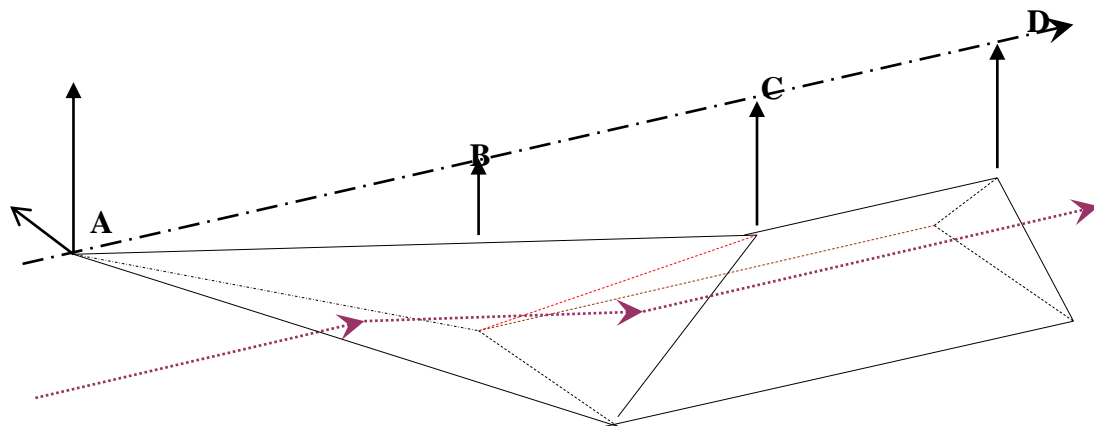
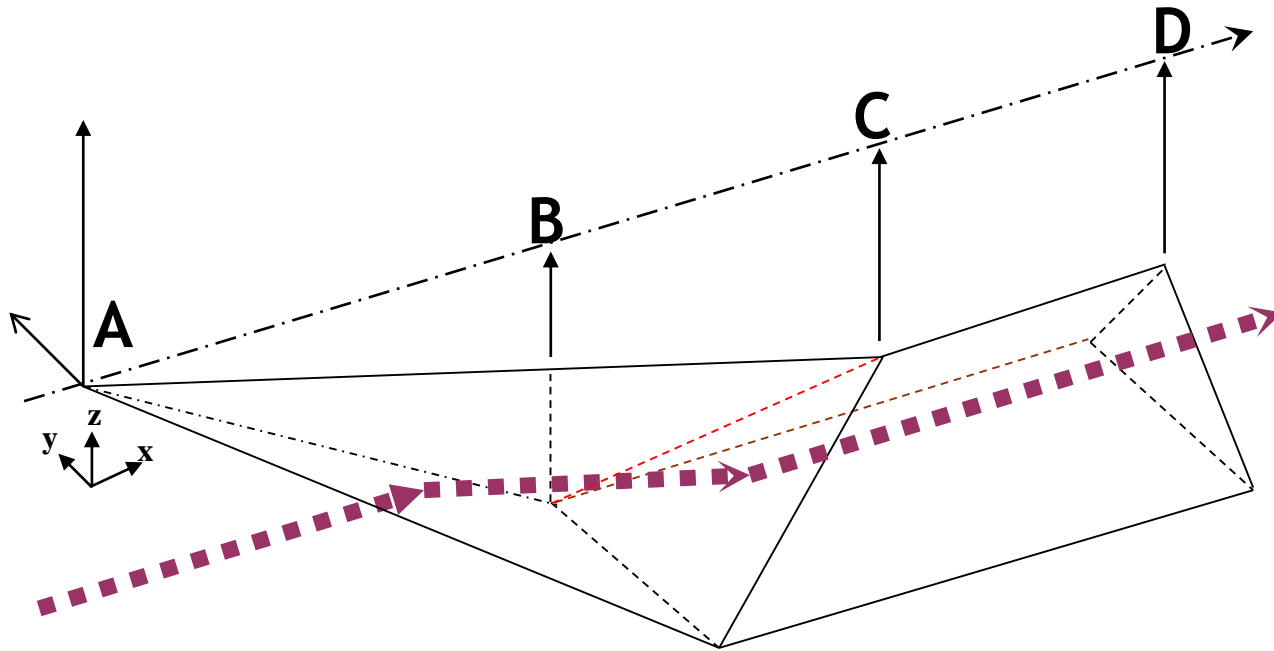
## NCAT Inverse Design Method for the Forebody



# Caret Waverider Design Concept

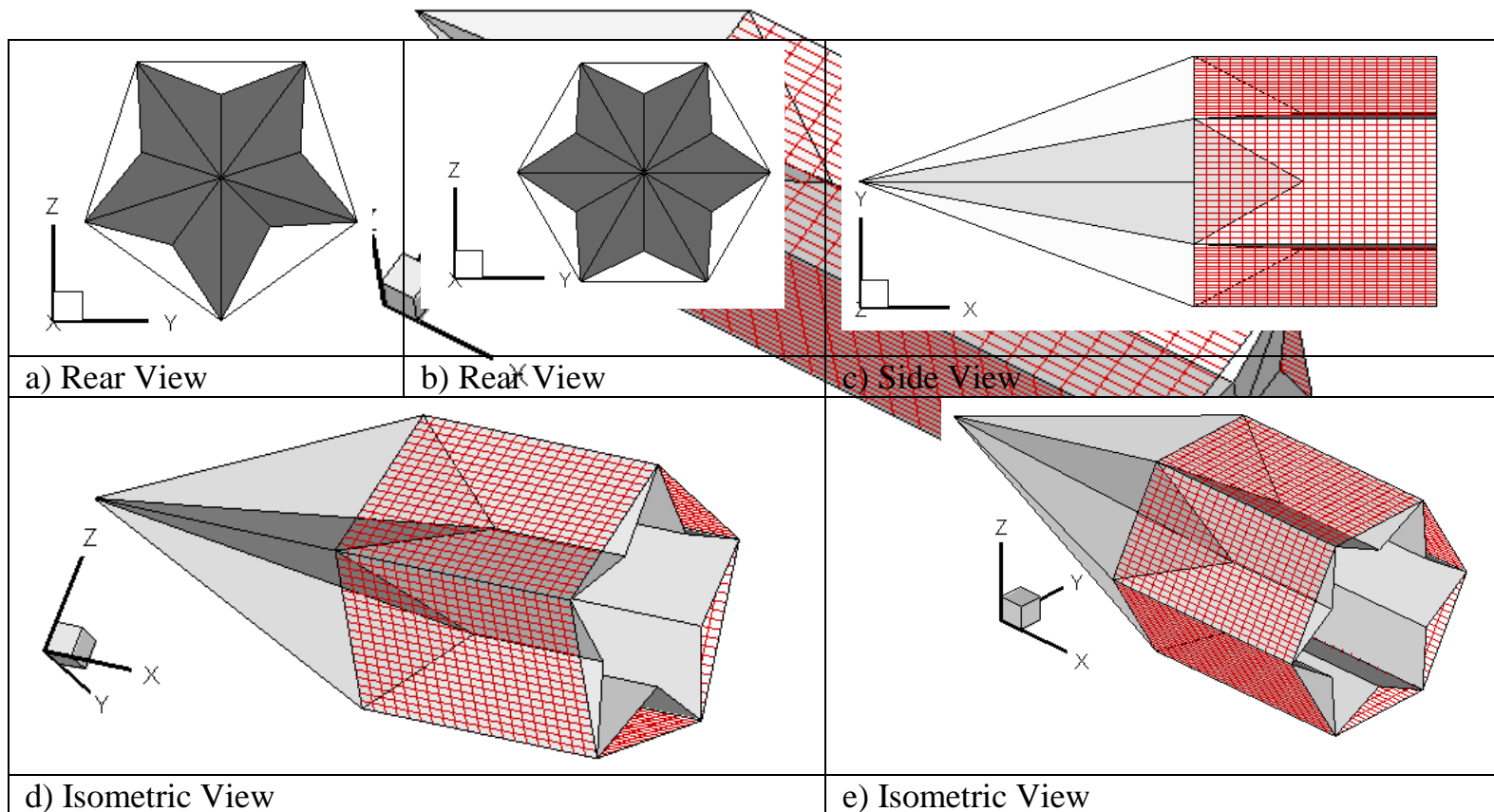


# 3-D Steam Tube Flow Path





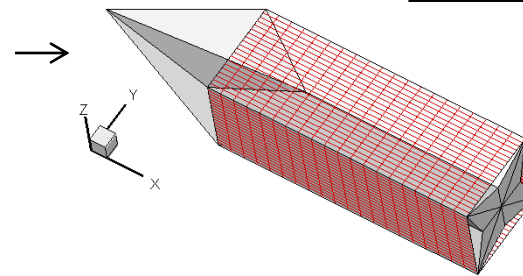
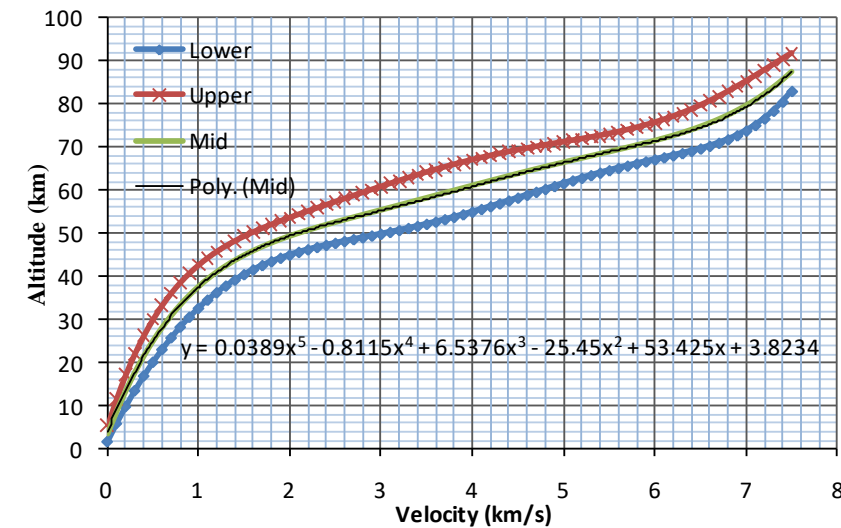
# Hypersonic Inlets



## Objective: Creation of Hypersonic Inlet Configurations with predictive performance capability

**Assumed: A Given Flight Path**

Design inputs	
Mach Number	5
Length of the Primary Shock Zone	1(m)
Shock Angle	17.5°
Cruising Flight Altitude	f(M)

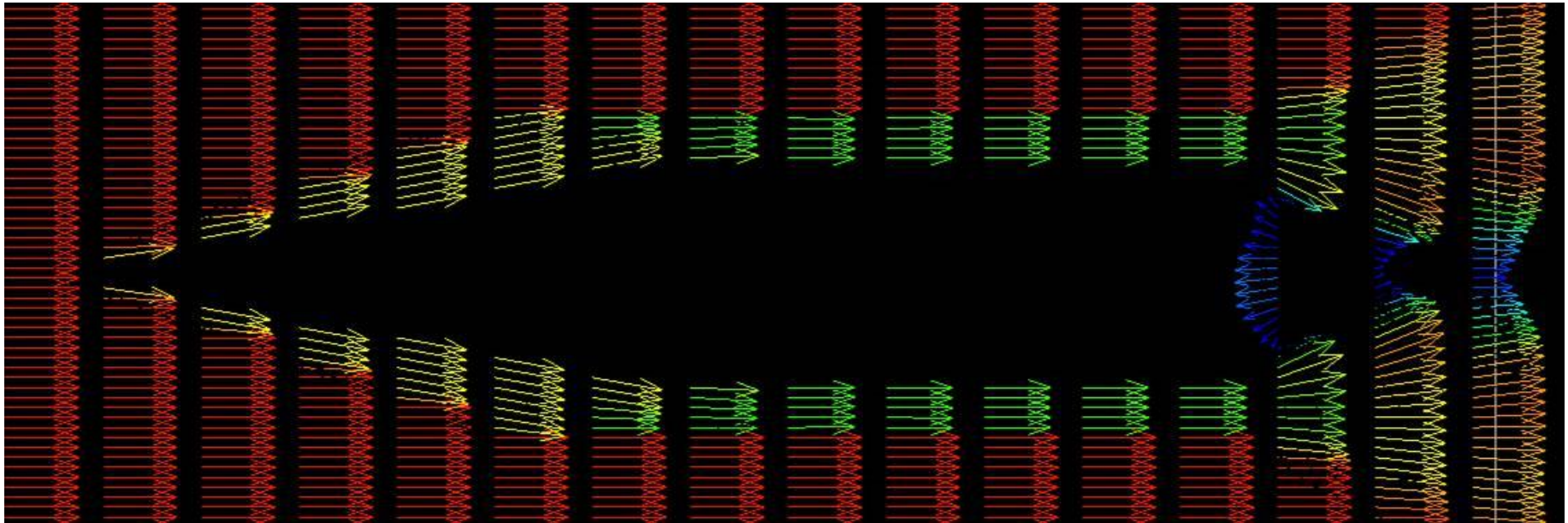


**Compare  
Design  
Predictions  
to CFD  
Evaluation**

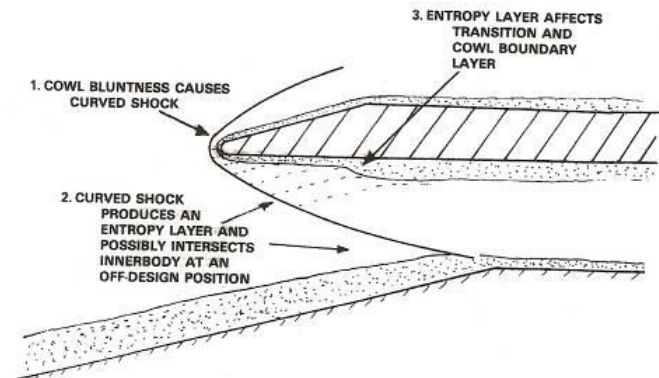
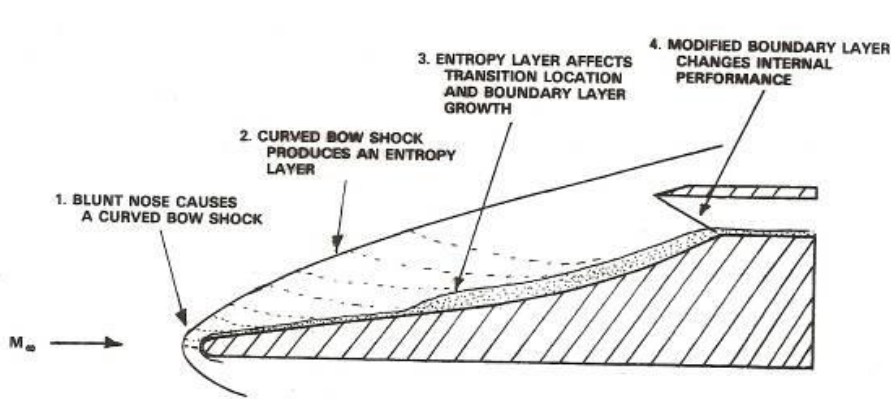
**Ideal: 2D & 3D  
Viscous: 2D & 3D**

- **Case 1: Ideal 3D**

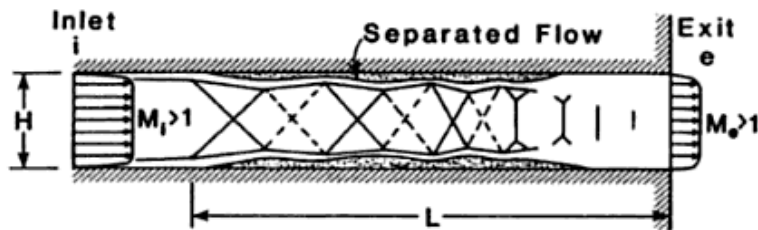
## Velocity Distribution – CFD Code



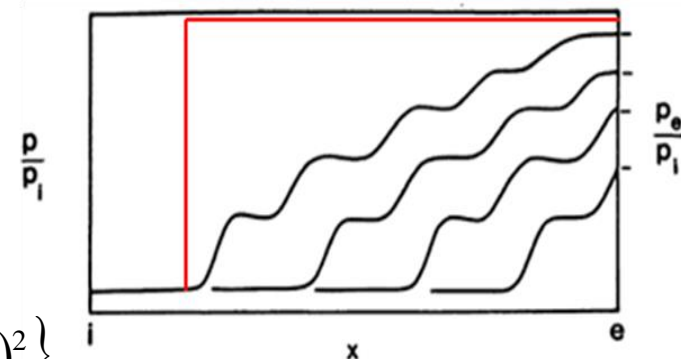
## 1. Leading Edge & SBLI Effects – Conduct Systematic Geometric Manipulations



## 2. Isolator Sizing - Validate/Improve Billig's ISTI Relations

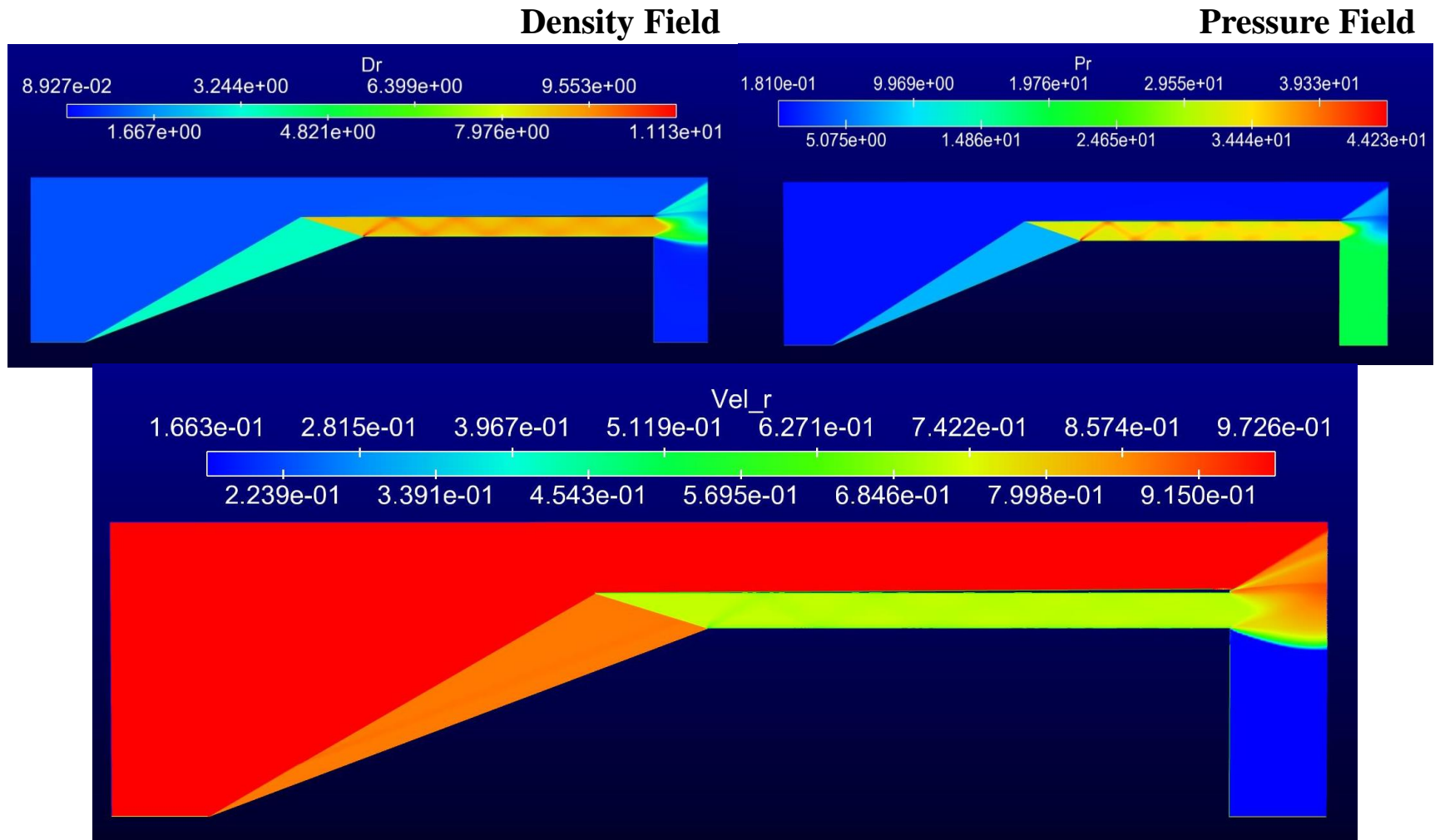


$$\left(\frac{L}{H}\right)_{\text{Isolator}} = \frac{\sqrt{\theta/H}}{(\text{Re}_\theta)^{1/4}} \frac{\{50((P_{\text{out}}/P_{\text{in}})+1)+170((P_{\text{out}}/P_{\text{in}})-1)^2\}}{M_{\text{in}}^2 - 1}$$





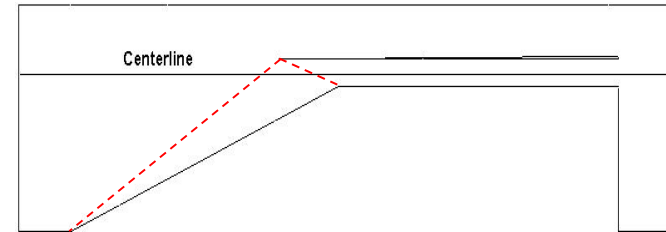
## Case 2: viscous effect



\* Predictions

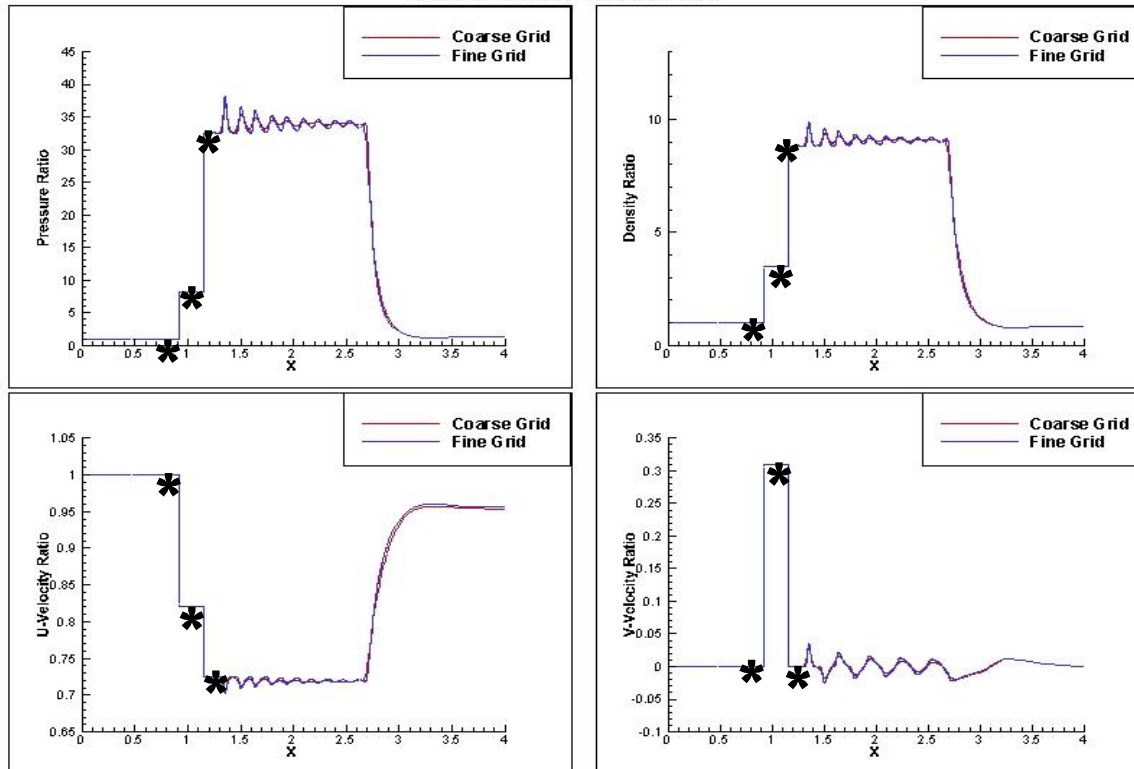
**Fine Grid = 1,474,442 cells**

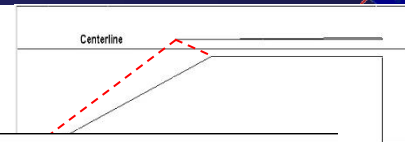
**Coarse Grid = 272,432 cells**



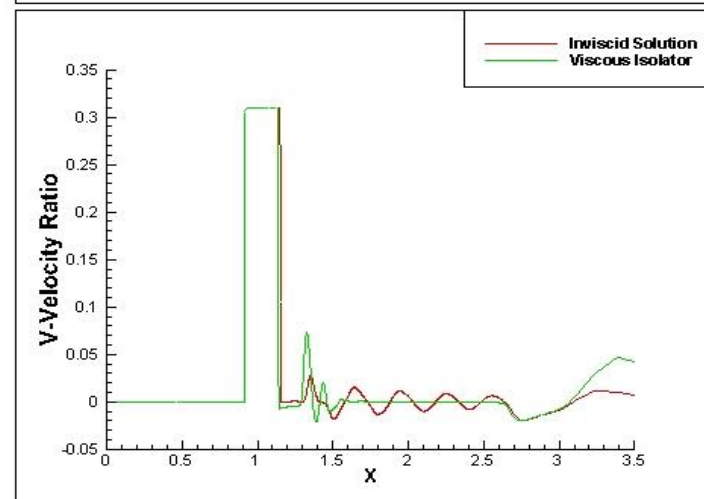
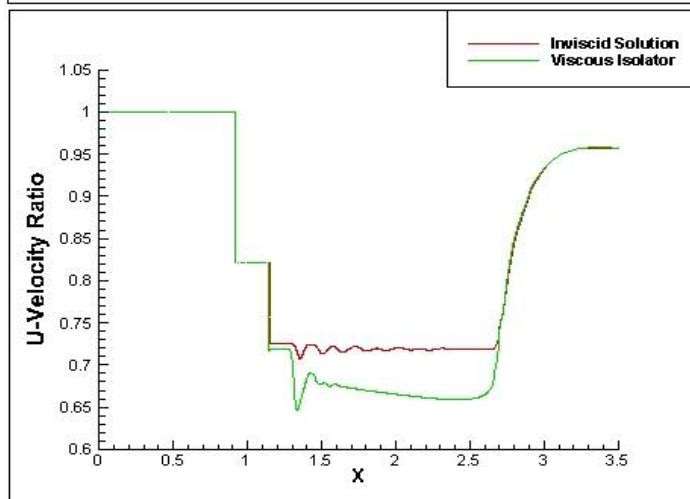
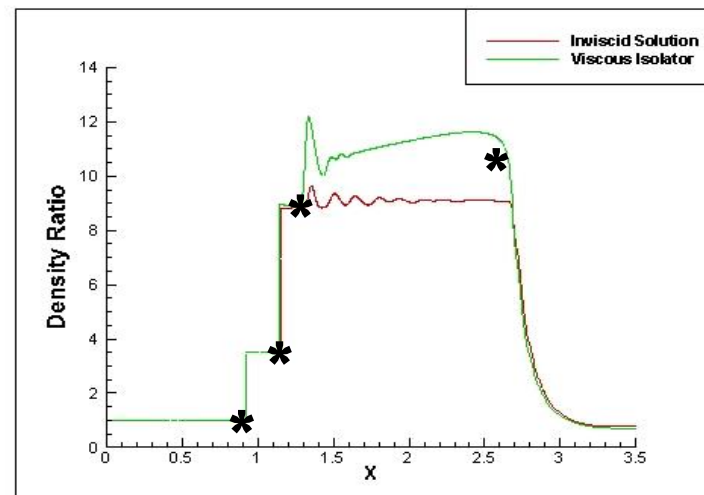
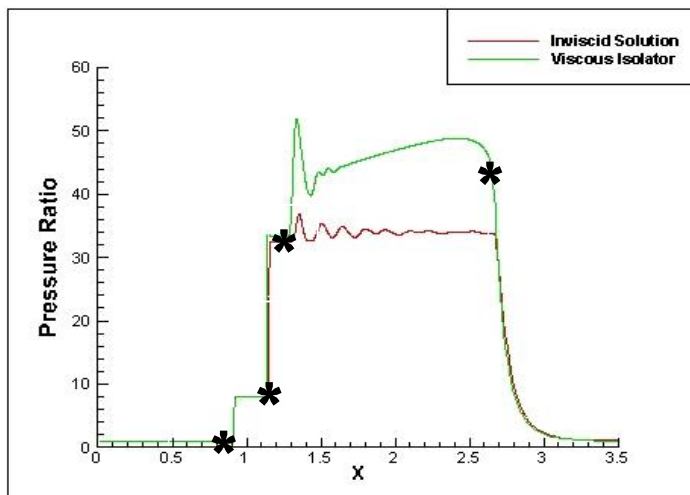
## Zoomed: Isolator Validation Data

Case 2: Coarse vs. Fine Grid





Case 2: Isolator Performance



## Case 4

### ➤ Elements

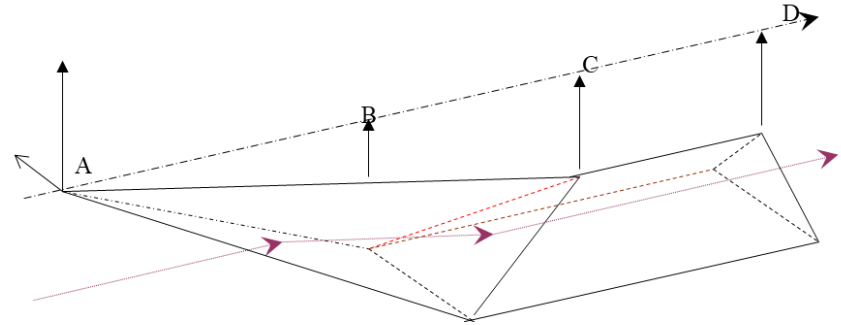
- 6.7 M

### ➤ Nodes

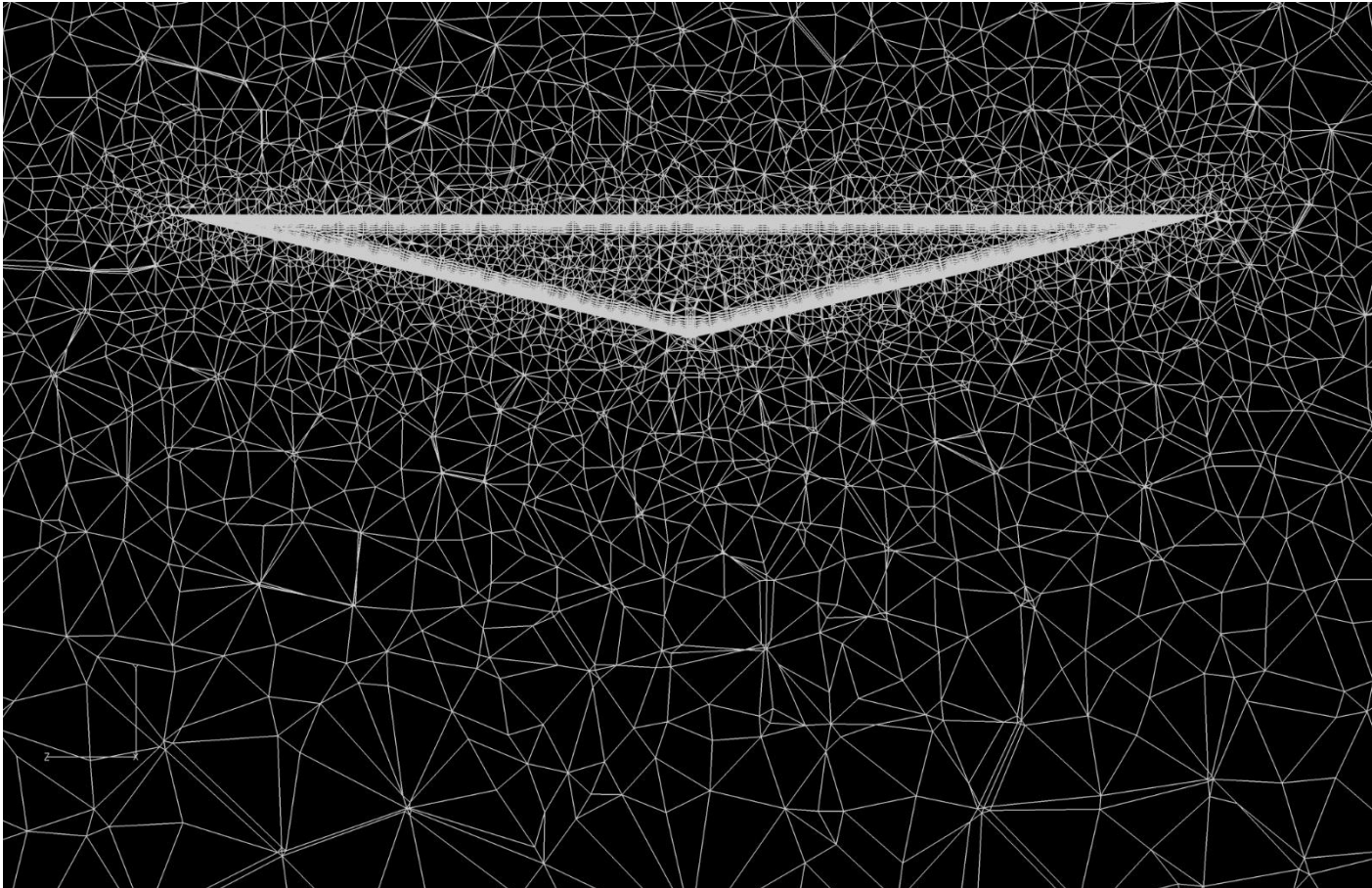
- 1,165,267

### ➤ Estimated Memory

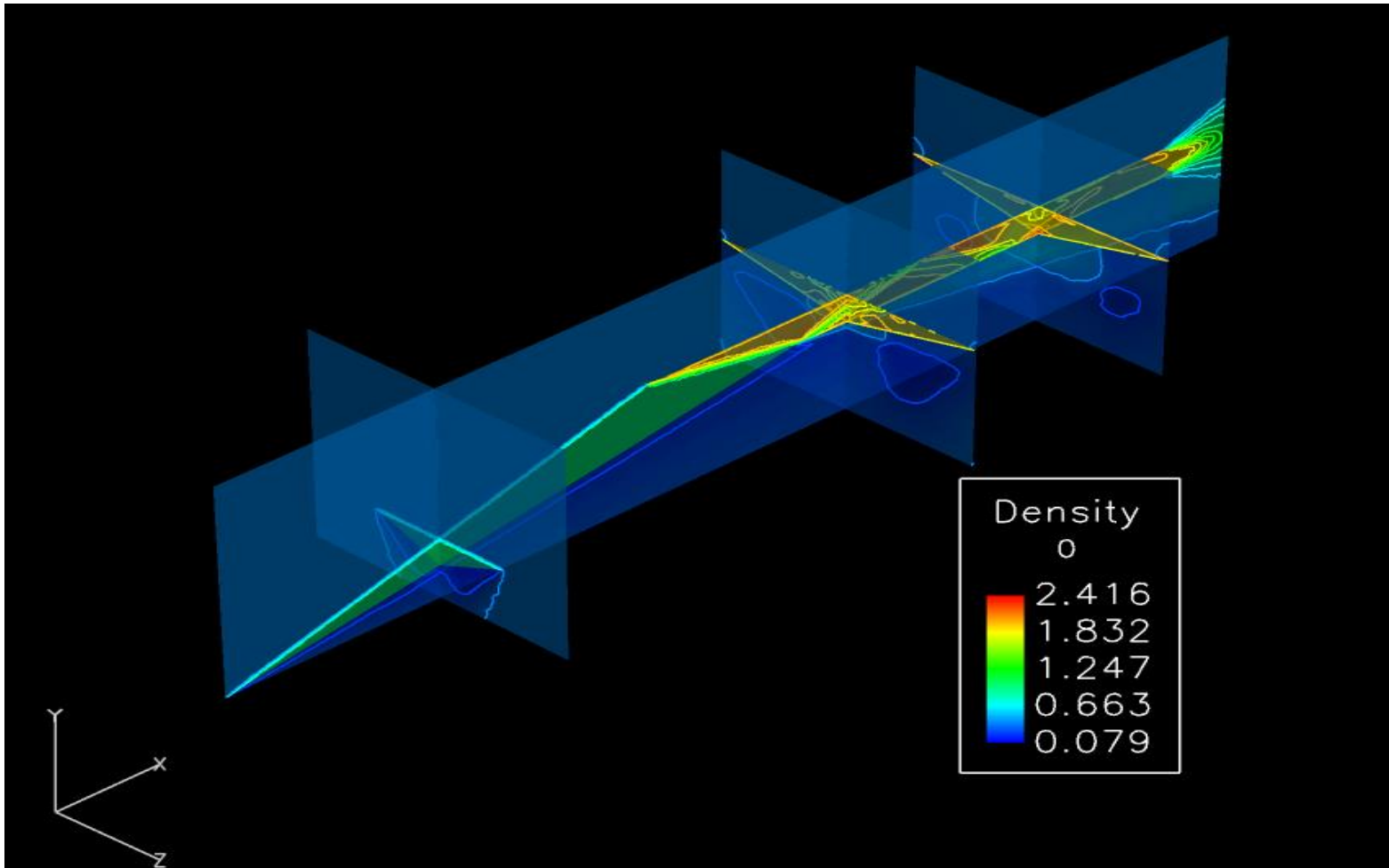
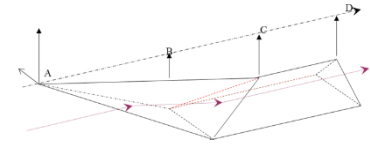
- 14.75 GB





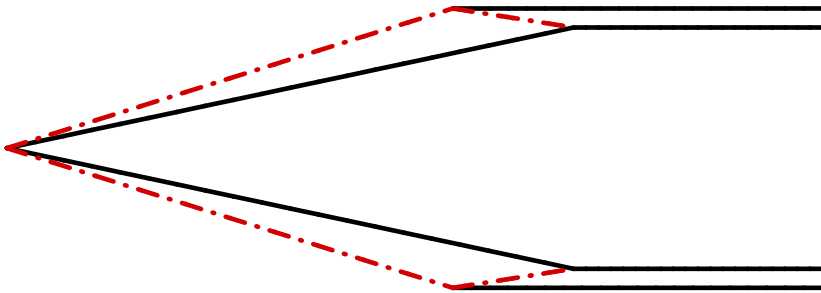


Irregular grid with clustering

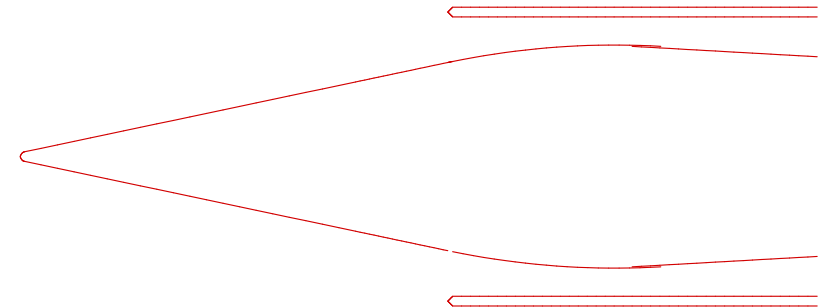
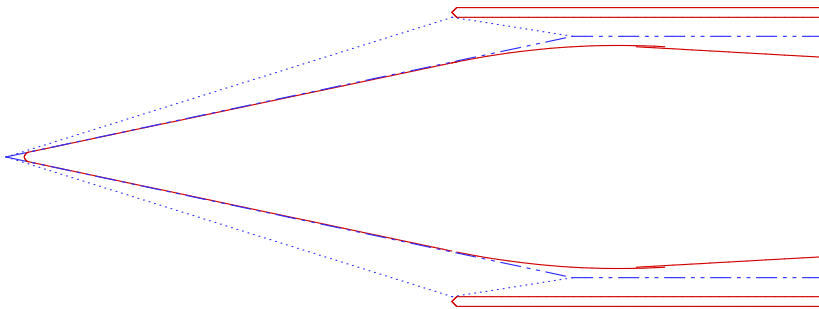
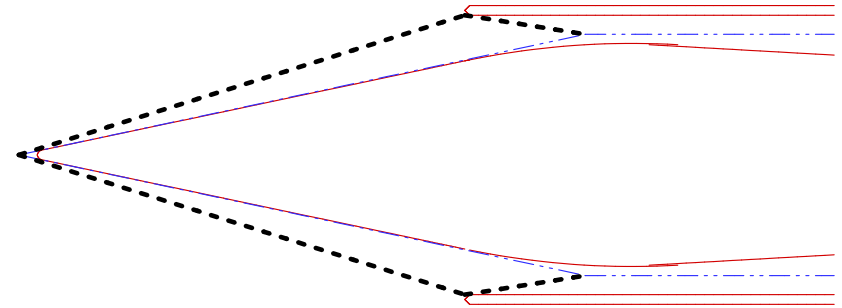


# Summary of Forebody Design & Analysis

## Viscous Modification of the Hypersonic Inlet



**Inverse Design – Euler Model**



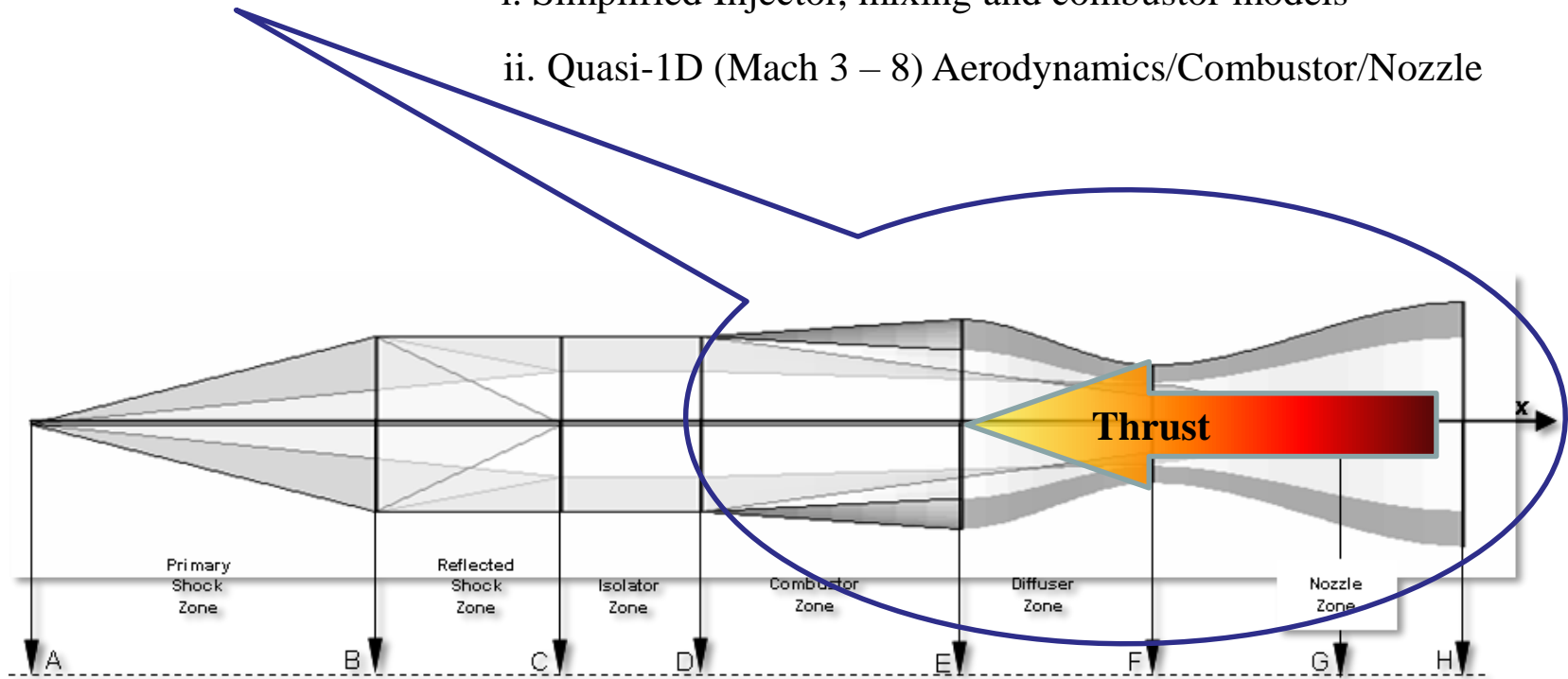
**Inverse Design – w/ Viscous Modifications**

Transformed model based off viscous effects

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## 2. Create A Internal 3D-Shape generator that incorporates

- i. Simplified Injector, mixing and combustor models
- ii. Quasi-1D (Mach 3 – 8) Aerodynamics/Combustor/Nozzle



Responsible for Thrust generation

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## Taylor Series

Solution: (a) Euler Method, (b)  
Runge-Kutta (Thomas)

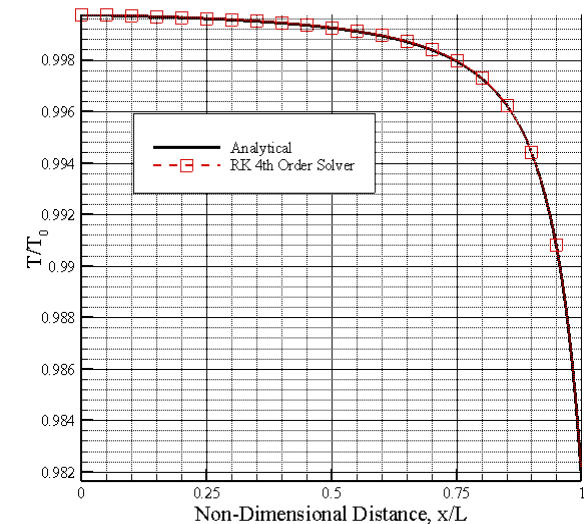
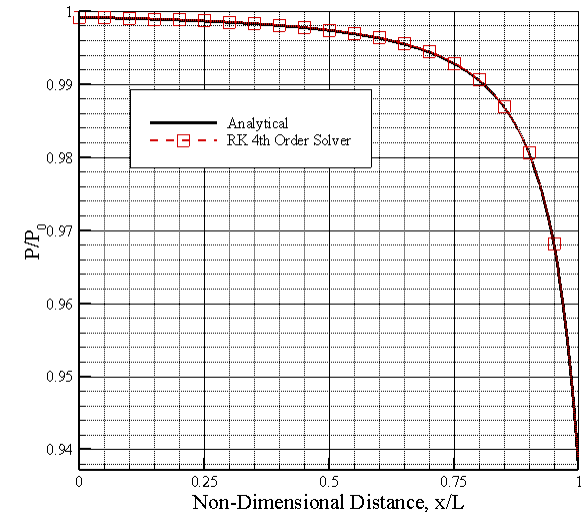
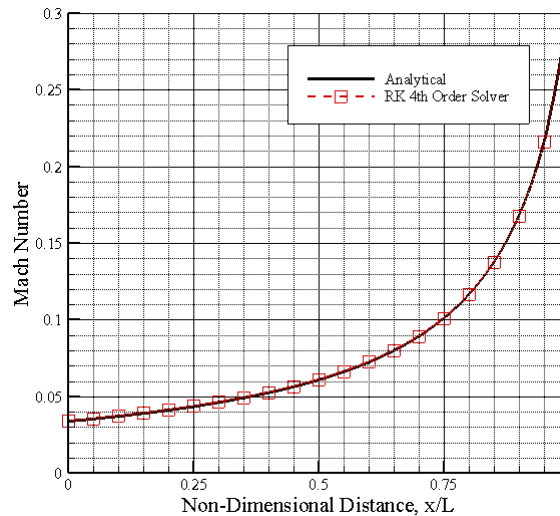
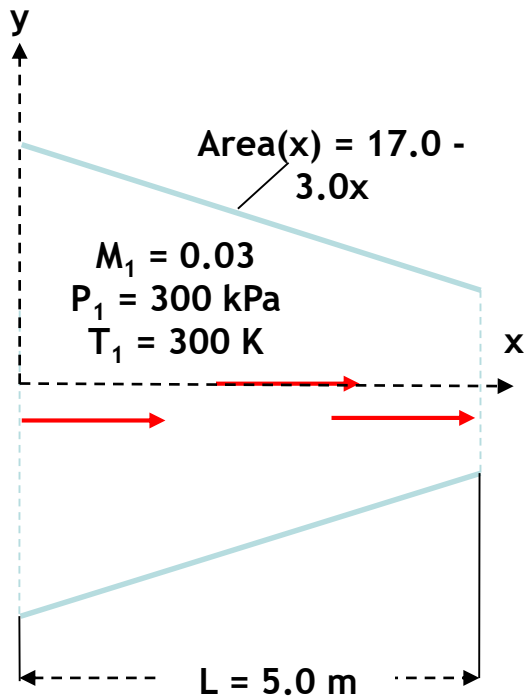
Description	Aerodynamic Quantities	Symbols
Area Influence	$\frac{1}{A} \frac{dA}{dx}$	$\frac{1}{y_1} \frac{dy_1}{dx}$
Heating Influence	$\frac{1}{c_p T} \frac{\partial Q - dH_0}{dx}$	$\frac{1}{y_2} \frac{dy_2}{dx}$
Friction Influence	$\frac{4C_f}{D_h} - 2\gamma \frac{1}{\dot{m}_{av}} \frac{d\dot{m}_{fuel}}{dx}$	$\frac{1}{y_3} \frac{dy_3}{dx}$
Fuel Injection Influence	$\frac{1}{\dot{m}_{av}} \frac{d\dot{m}_{fuel}}{dx}$	$\frac{1}{y_4} \frac{dy_4}{dx}$
Combustion Chemistry Influence	$\frac{1}{W_M} \frac{\partial W_M}{dx}$	$\frac{1}{y_5} \frac{dy_5}{dx}$
High Temperature Influence	$\frac{1}{\gamma} \frac{\delta \gamma}{dx}$	$\frac{1}{y_6} \frac{dy_6}{dx}$

$$\frac{1}{M} \frac{dM}{dx} = C_{1,1} \frac{1}{y_1} \frac{dy_1}{dx} + C_{1,2} \frac{1}{y_2} \frac{dy_2}{dx} + C_{1,3} \frac{1}{y_3} \frac{dy_3}{dx} + C_{1,4} \frac{1}{y_4} \frac{dy_4}{dx} + C_{1,5} \frac{1}{y_5} \frac{dy_5}{dx} + C_{1,6} \frac{1}{y_6} \frac{dy_6}{dx}$$

$$\frac{1}{T} \frac{dT}{dx} = C_{2,1} \frac{1}{y_1} \frac{dy_1}{dx} + C_{2,2} \frac{1}{y_2} \frac{dy_2}{dx} + C_{2,3} \frac{1}{y_3} \frac{dy_3}{dx} + C_{2,4} \frac{1}{y_4} \frac{dy_4}{dx} + C_{2,5} \frac{1}{y_5} \frac{dy_5}{dx} + C_{2,6} \frac{1}{y_6} \frac{dy_6}{dx}$$

$$\frac{1}{P} \frac{dP}{dx} = C_{3,1} \frac{1}{y_1} \frac{dy_1}{dx} + C_{3,2} \frac{1}{y_2} \frac{dy_2}{dx} + C_{3,3} \frac{1}{y_3} \frac{dy_3}{dx} + C_{3,4} \frac{1}{y_4} \frac{dy_4}{dx} + C_{3,5} \frac{1}{y_5} \frac{dy_5}{dx} + C_{3,6} \frac{1}{y_6} \frac{dy_6}{dx}$$

## Area Only, Convergent Duct, Subsonic



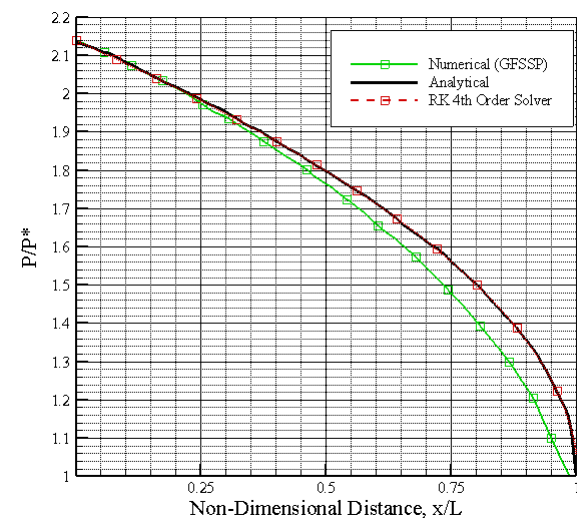
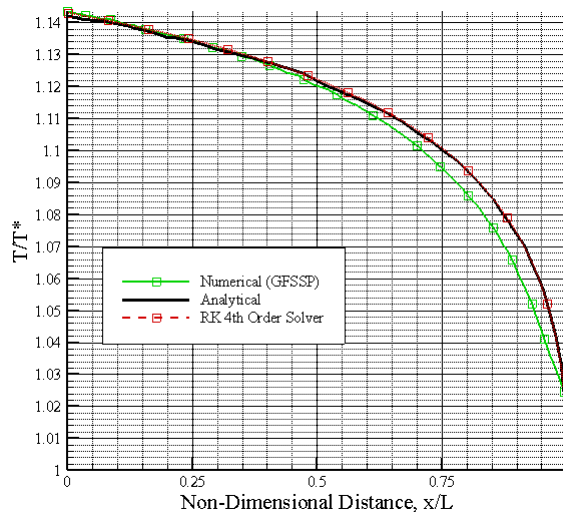
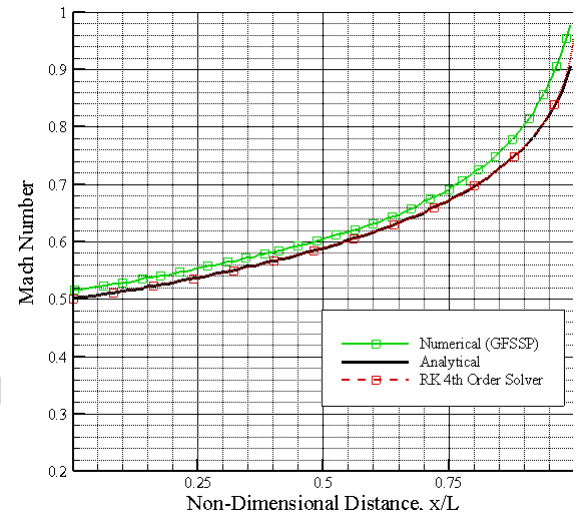
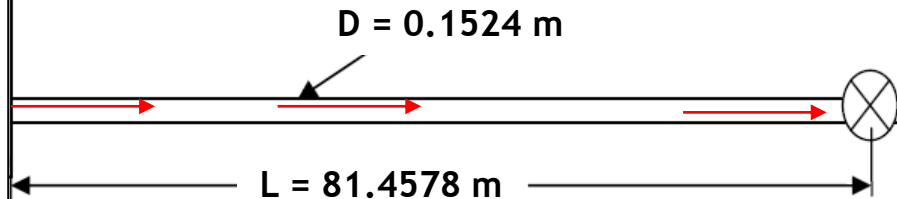
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## Fanno Flow

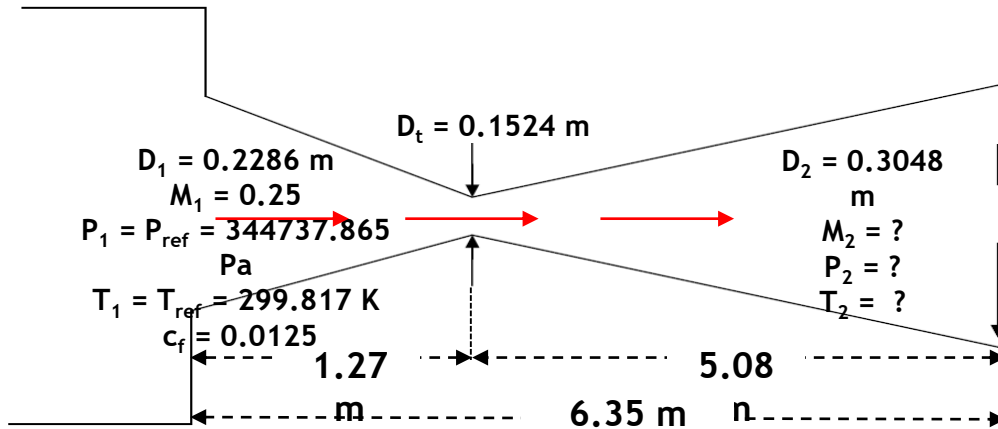
$M_1 = 0.5$   
 $P_1 = 344737.865 \text{ Pa}$   
 $T_1 = 299.817 \text{ K}$   
 $c_f = 0.0005$   
 $P^* = 161235.613 \text{ Pa}$   
 $T^* = 262.315 \text{ K}$

Schematic of a constant area pipe (Bandyopadhyay, 2007)

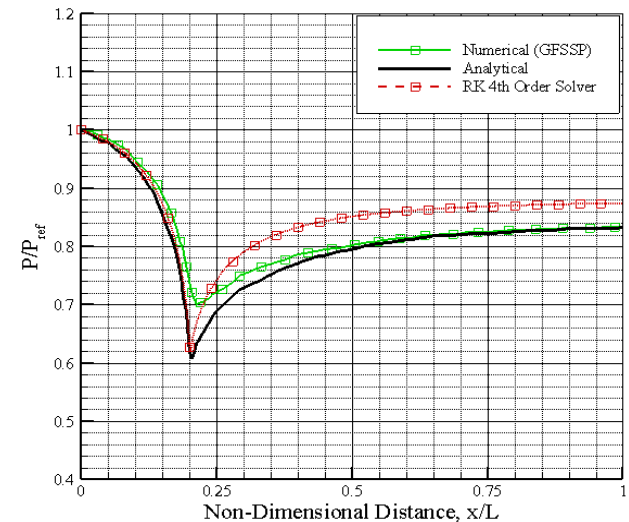
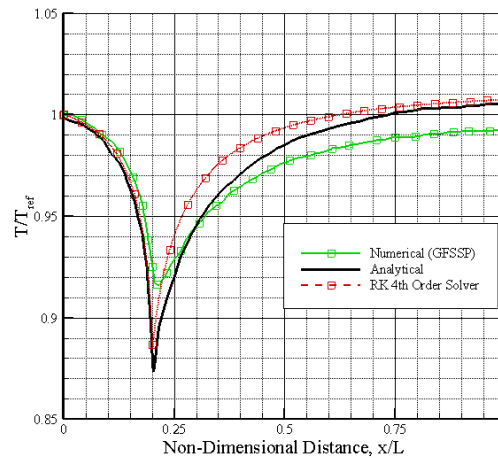
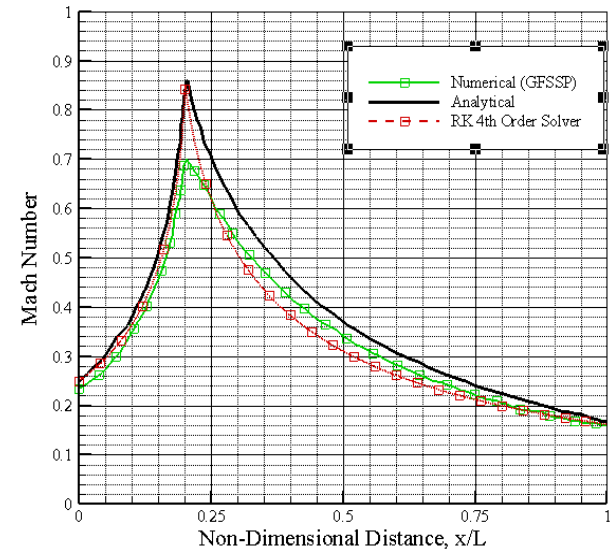


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## Quasi 1D with Friction



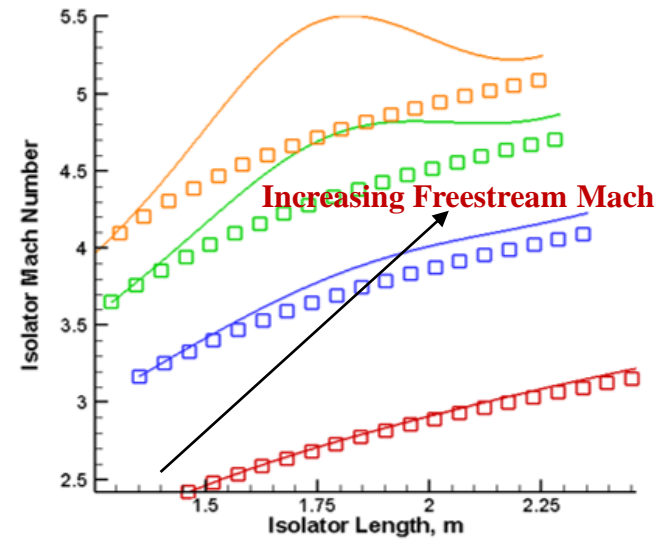
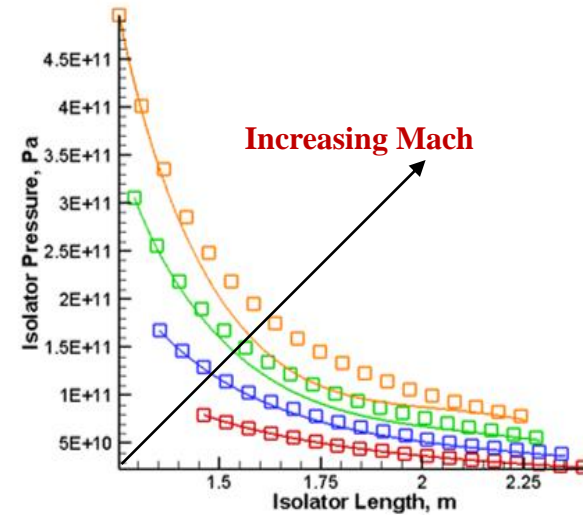
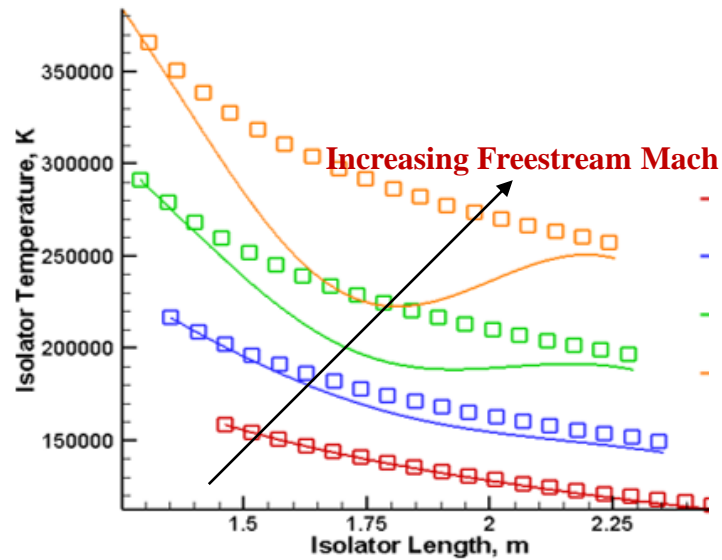
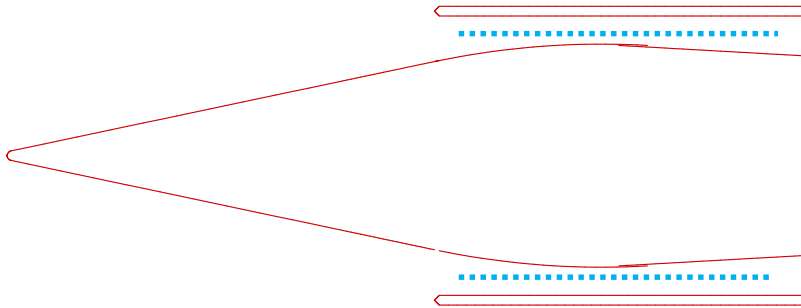
Ref. Bandyopadhyay, 2007



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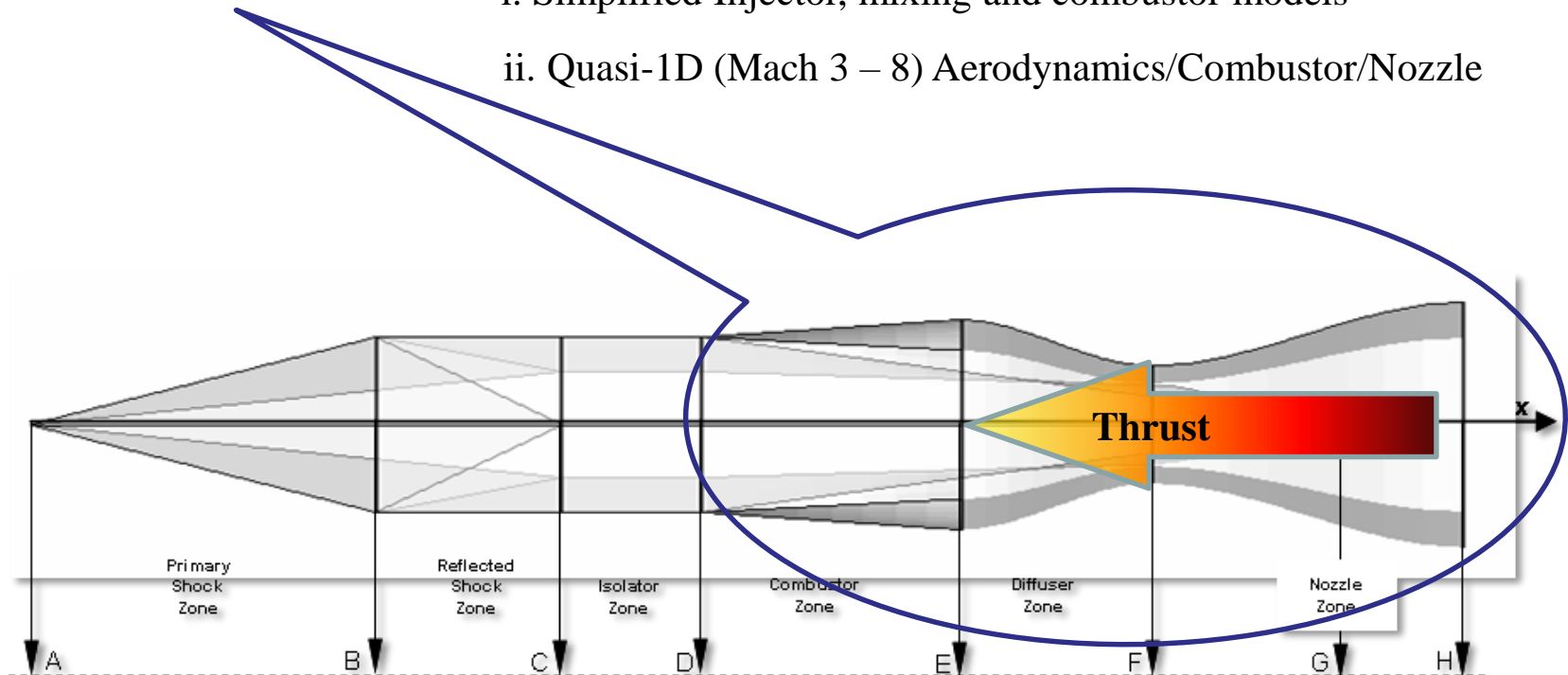
## Quasi 1-D Inlet Evaluation ( $M = 5-8$ )



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## 2. Create A Internal 3D-Shape generator that incorporates

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Responsible for Thrust generation

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## Taylor Series

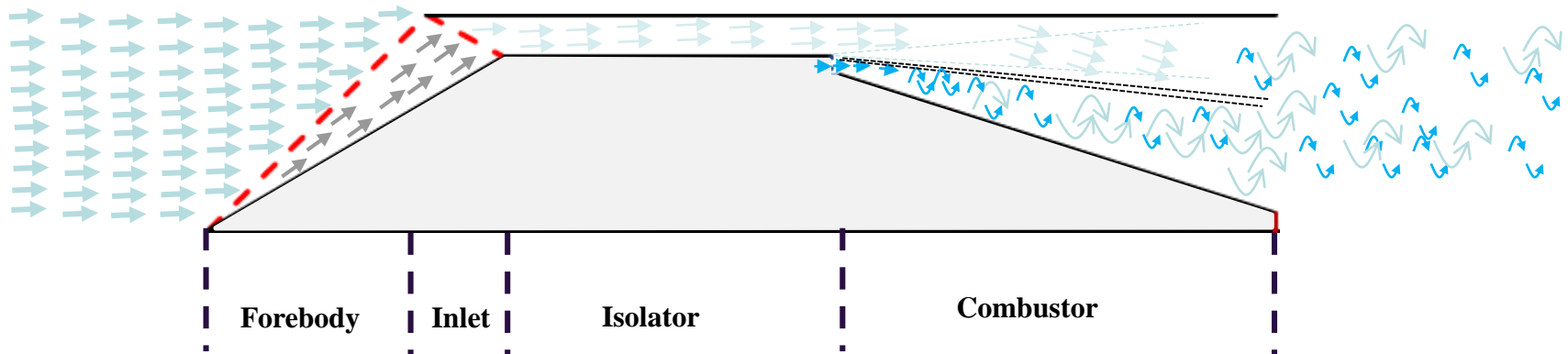
**Solution: (a) Euler Method, (b) Runge-Kutta (Thomas)**

Description	Aerodynamic Quantities	Symbols
Area Influence	$\frac{1}{A} \frac{dA}{dx}$	$\frac{1}{y_1} \frac{dy_1}{dx}$
Heating Influence	$\frac{1}{c_p T} \frac{\partial Q - dH_0}{dx}$	$\frac{1}{y_2} \frac{dy_2}{dx}$
Friction Influence	$\frac{4C_f}{D_h} - 2\gamma \frac{1}{\dot{m}_{av}} \frac{d\dot{m}_{fuel}}{dx}$	$\frac{1}{y_3} \frac{dy_3}{dx}$
Fuel Injection Influence	$\frac{1}{\dot{m}_{av}} \frac{d\dot{m}_{fuel}}{dx}$	$\frac{1}{y_4} \frac{dy_4}{dx}$
Combustion Chemistry Influence	$\frac{1}{W_M} \frac{\partial W_M}{dx}$	$\frac{1}{y_5} \frac{dy_5}{dx}$
High Temperature Influence	$\frac{1}{\gamma} \frac{\delta \gamma}{dx}$	$\frac{1}{y_6} \frac{dy_6}{dx}$

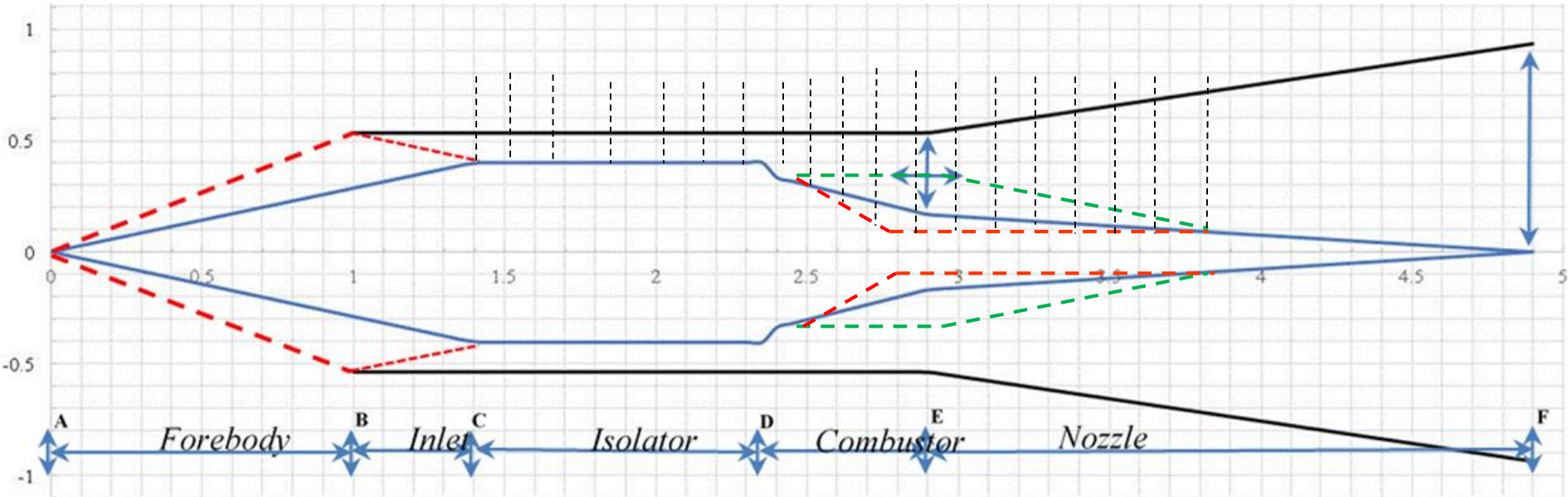
$$\frac{1}{M} \frac{dM}{dx} = C_{1,1} \frac{1}{y_1} \frac{dy_1}{dx} + C_{1,2} \frac{1}{y_2} \frac{dy_2}{dx} + C_{1,3} \frac{1}{y_3} \frac{dy_3}{dx} + C_{1,4} \frac{1}{y_4} \frac{dy_4}{dx} + C_{1,5} \frac{1}{y_5} \frac{dy_5}{dx} + C_{1,6} \frac{1}{y_6} \frac{dy_6}{dx}$$

$$\frac{1}{T} \frac{dT}{dx} = C_{2,1} \frac{1}{y_1} \frac{dy_1}{dx} + C_{2,2} \frac{1}{y_2} \frac{dy_2}{dx} + C_{2,3} \frac{1}{y_3} \frac{dy_3}{dx} + C_{2,4} \frac{1}{y_4} \frac{dy_4}{dx} + C_{2,5} \frac{1}{y_5} \frac{dy_5}{dx} + C_{2,6} \frac{1}{y_6} \frac{dy_6}{dx}$$

$$\frac{1}{P} \frac{dP}{dx} = C_{3,1} \frac{1}{y_1} \frac{dy_1}{dx} + C_{3,2} \frac{1}{y_2} \frac{dy_2}{dx} + C_{3,3} \frac{1}{y_3} \frac{dy_3}{dx} + C_{3,4} \frac{1}{y_4} \frac{dy_4}{dx} + C_{3,5} \frac{1}{y_5} \frac{dy_5}{dx} + C_{3,6} \frac{1}{y_6} \frac{dy_6}{dx}$$



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- High speed aerodynamics is driving this design.
- This section is dominated by viscous effects, which results in a very complicated flow field.
- Conventional CFD tools cannot capture the flow physics we're after.

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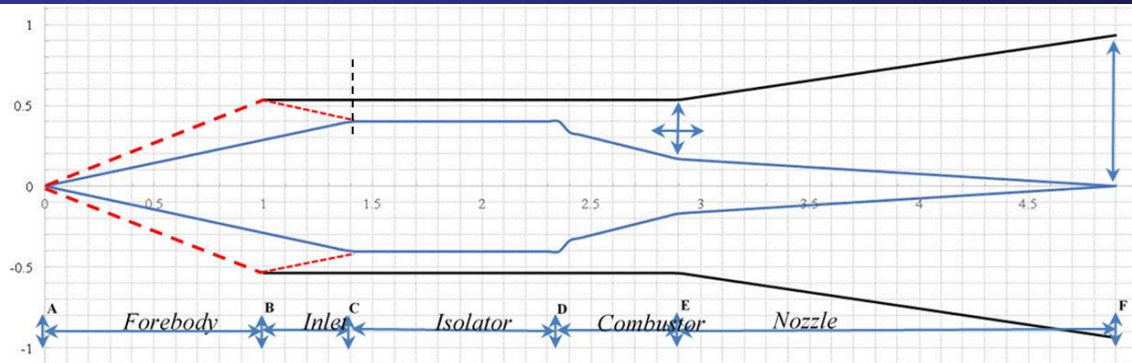
We have Six influence coefficients :

Design inputs:

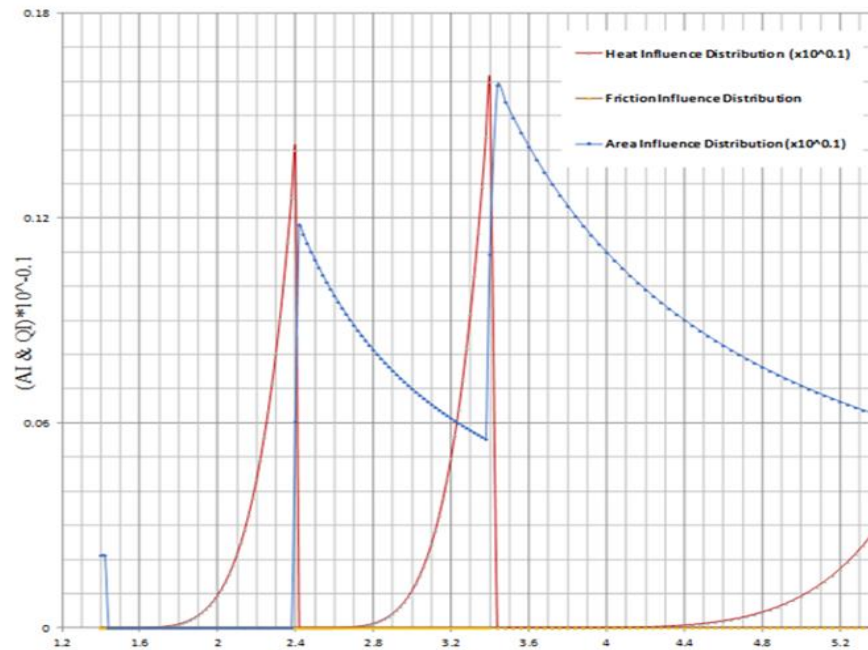
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Heating Influence	$\frac{1}{c_p T} \frac{\delta Q - dH_0}{dx}$	$\frac{1}{y_2} \frac{dy_2}{dx}$
Friction Influence	$\frac{4C_f}{D_h} - 2\chi \frac{1}{\dot{m}_{air}} \frac{d\dot{m}_{fuel}}{dx}$	$\frac{1}{y_3} \frac{dy_3}{dx}$
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Combustion Chemistry Influence	$\frac{1}{W_M} \frac{\delta W_M}{dx}$	$\frac{1}{y_5} \frac{dy_5}{dx}$
High Temperature Influence	$\frac{1}{\gamma} \frac{\delta \gamma}{dx}$	$\frac{1}{y_6} \frac{dy_6}{dx}$

Description	Numbers		Dimension
Flight Altitude	30.0		km
Mach Number	5.0		
Wedge Angle	16.0		Degrees
Forebody Length	1.0		m
Fractional x & y Lengths of ID Values			
Isolator Design Parameters	1.0	0.9	
Combustor Design Parameters	1.0	0.8	
Nozzle Design Parameters	1.0	0.0	

# Three Influences for Testing

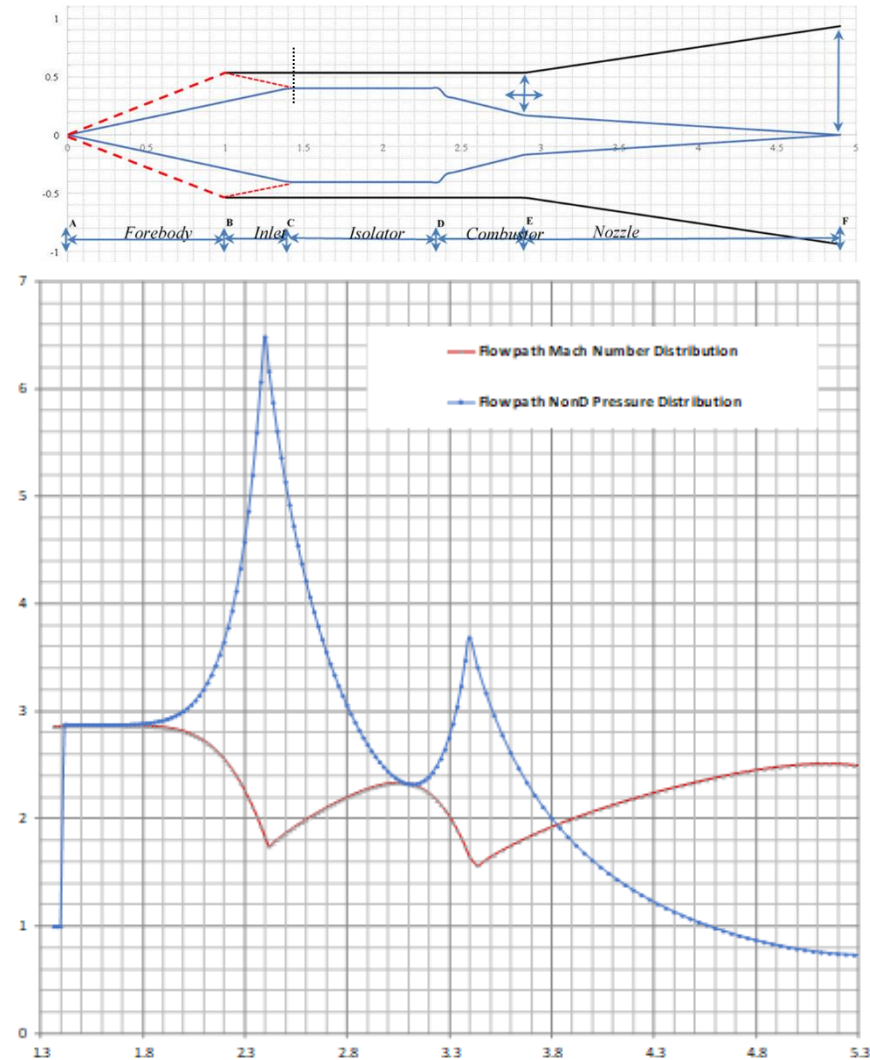
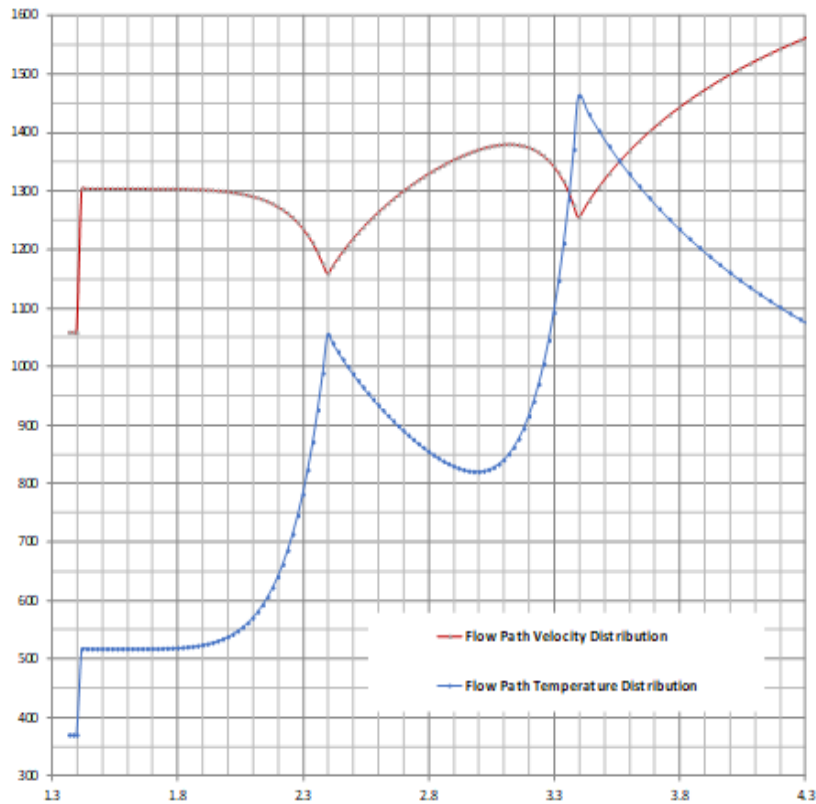


## Example with 3 different influences



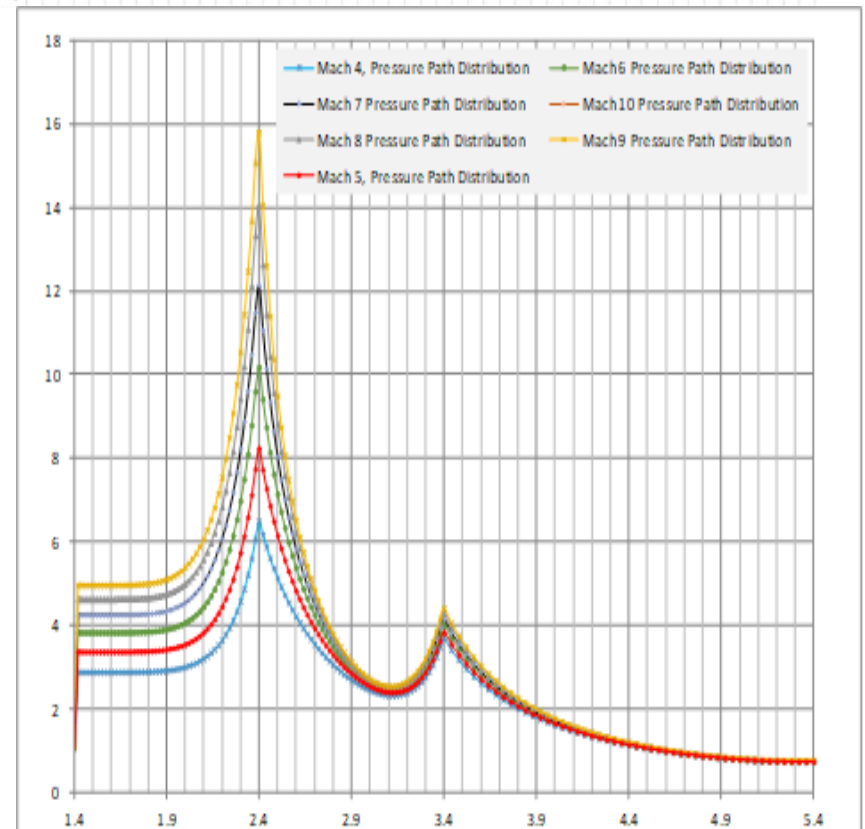
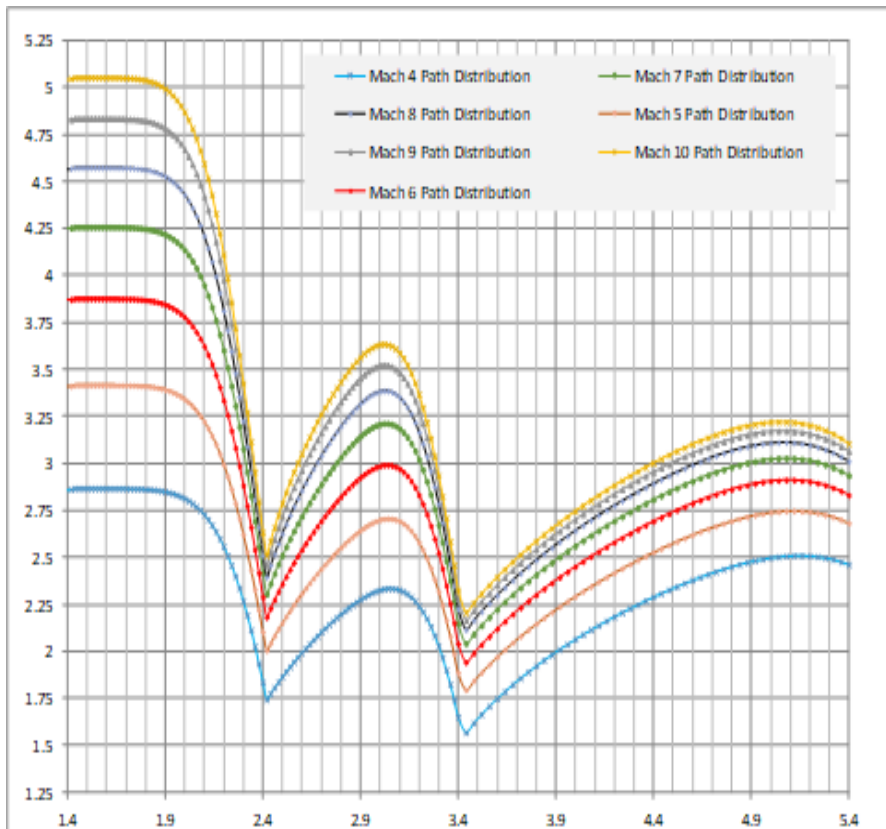
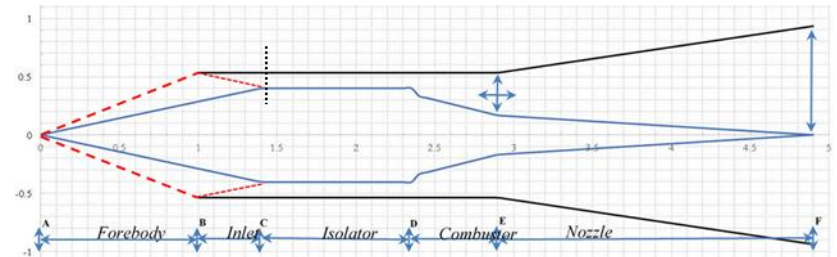
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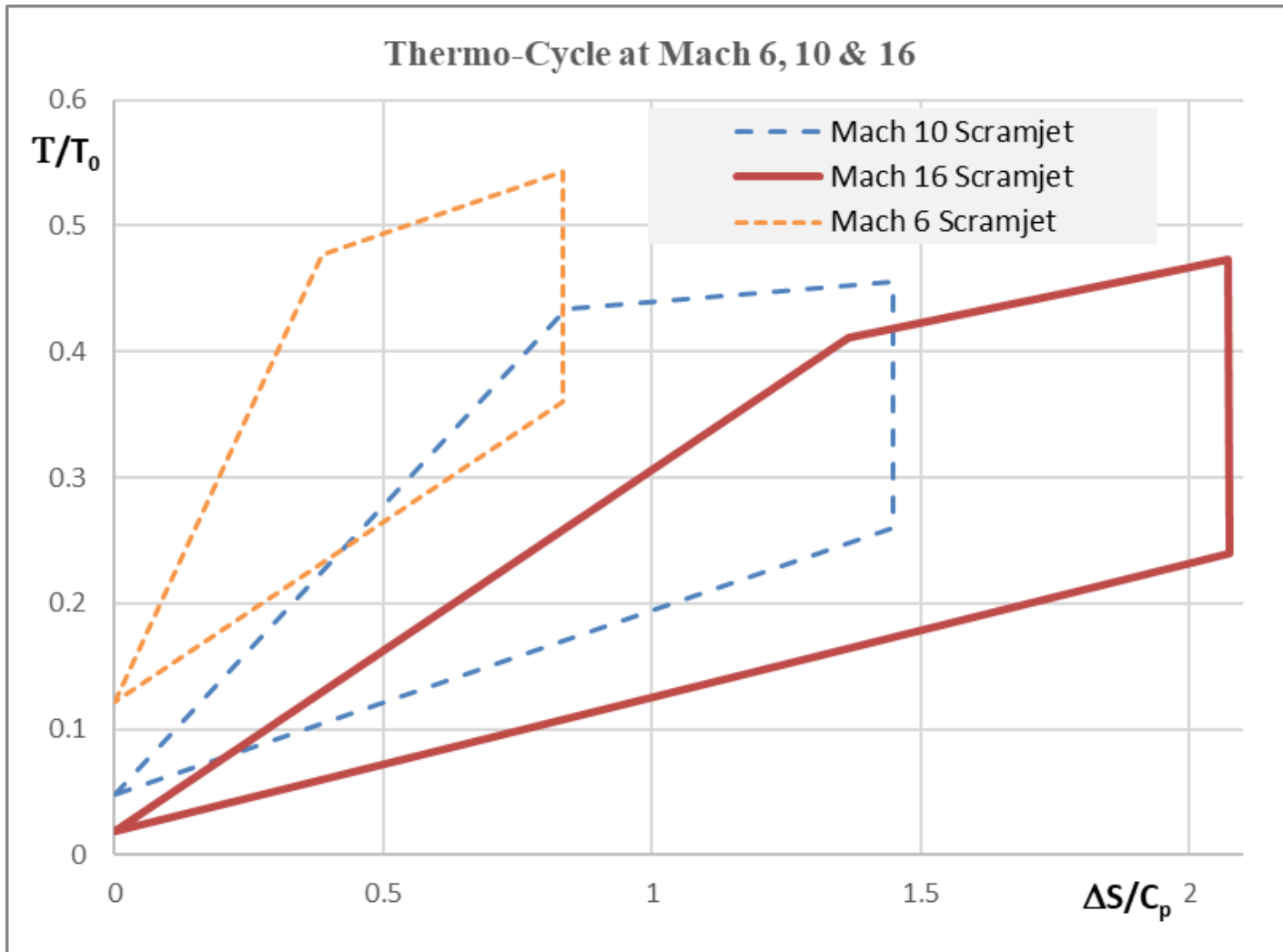




# Distribution For Various Mach Number



# Thermo-Cycle For The Engine





# Thank You Questions?