

## Two-Phase Flow System Design Status of the Flow Boiling and Condensation Experiment

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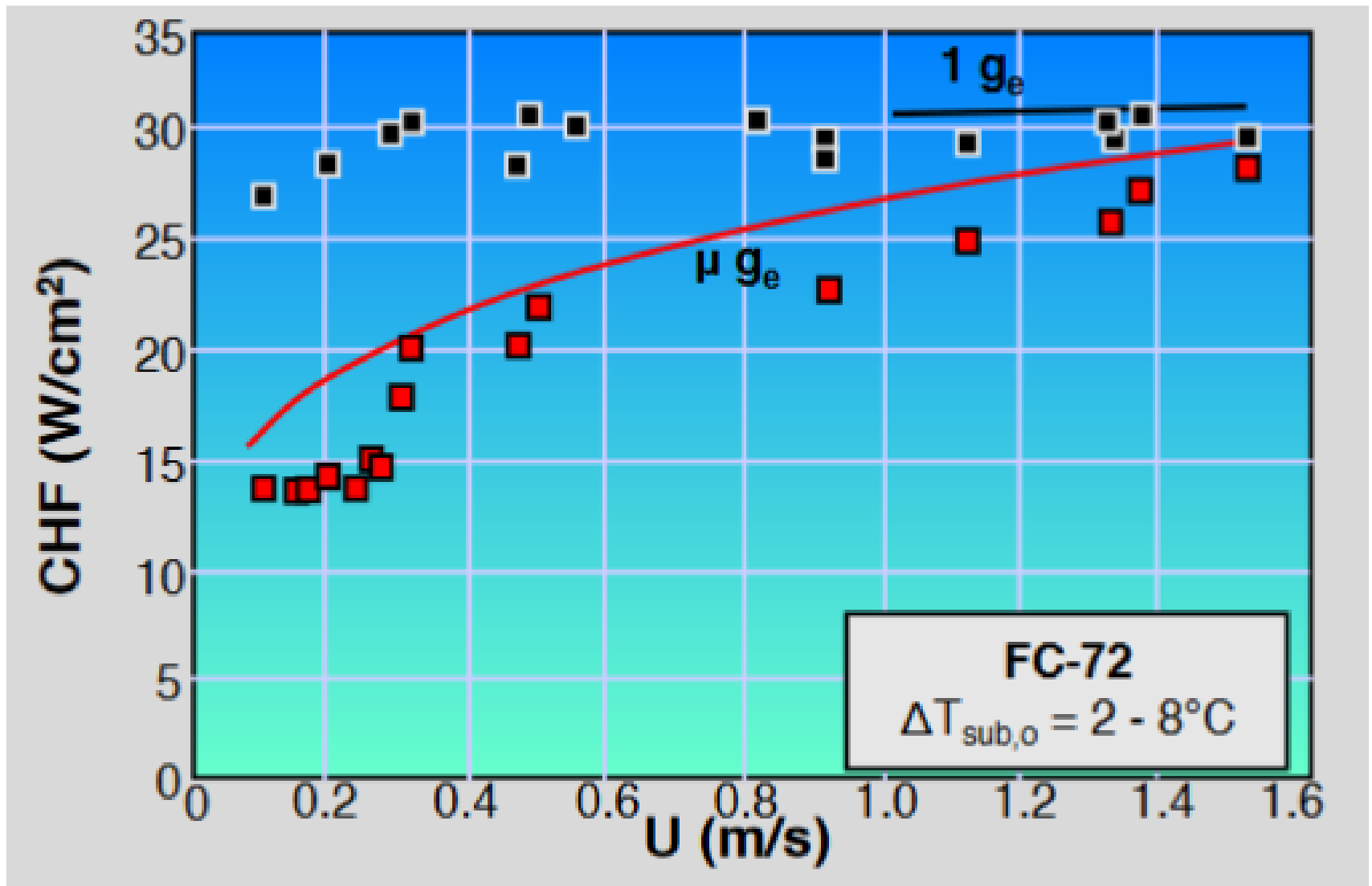


# Science Objectives



1. Develop an experimentally validated, mechanistic model for microgravity flow boiling Critical Heat Flux (CHF) with dimensionless criteria to predict minimum flow velocity required to ensure gravity independent CHF.
  - Obtain flow boiling data (heat flux, wall temperature difference, etc.) in long duration microgravity environments for a well characterized heating surface as functions of liquid inlet mass velocity and sub-cooling.
  
2. Develop an experimentally validated, mechanistic model for microgravity annular condensation with dimensionless criteria to predict minimum flow velocity required to ensure gravity independent annular condensation.
  - Obtain flow condensation data (heat flux, wall temperature difference, etc.) in long duration microgravity environments for a well-characterized condensing surface as functions of inlet quality and flow rate of condensing vapor.

# Science Objectives



**PURDUE**  
UNIVERSITY

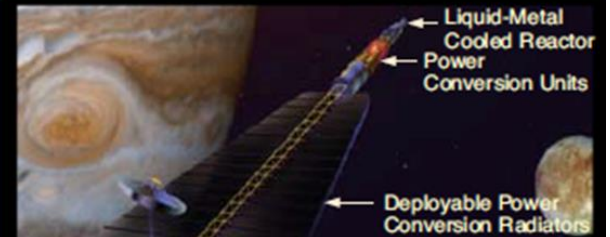
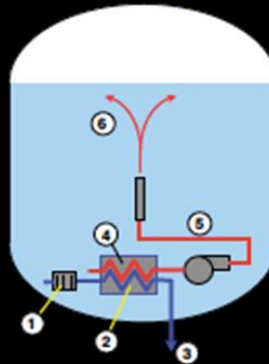
## Customer Technology Applications



**Vapor  
Compression  
Heat Pump for  
Future Space  
Vehicles  
Planetary Bases**

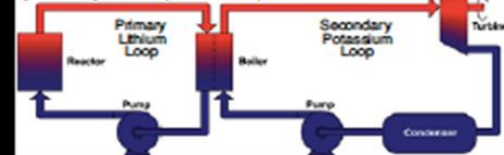


**Thermodynamic Vent  
System (TVS) for  
Cryogenic Liquid  
Storage**



**Project Prometheus:  
Developing means to efficiently  
power advanced spacecraft for  
Solar System exploration**

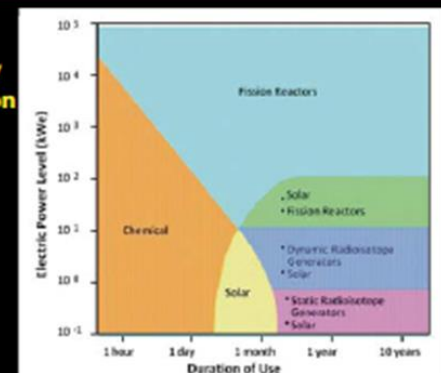
Rankine Cycle very attractive option for high power systems (> 100 kWe)



**Thermal Control Systems and  
Advanced Life Support Systems**

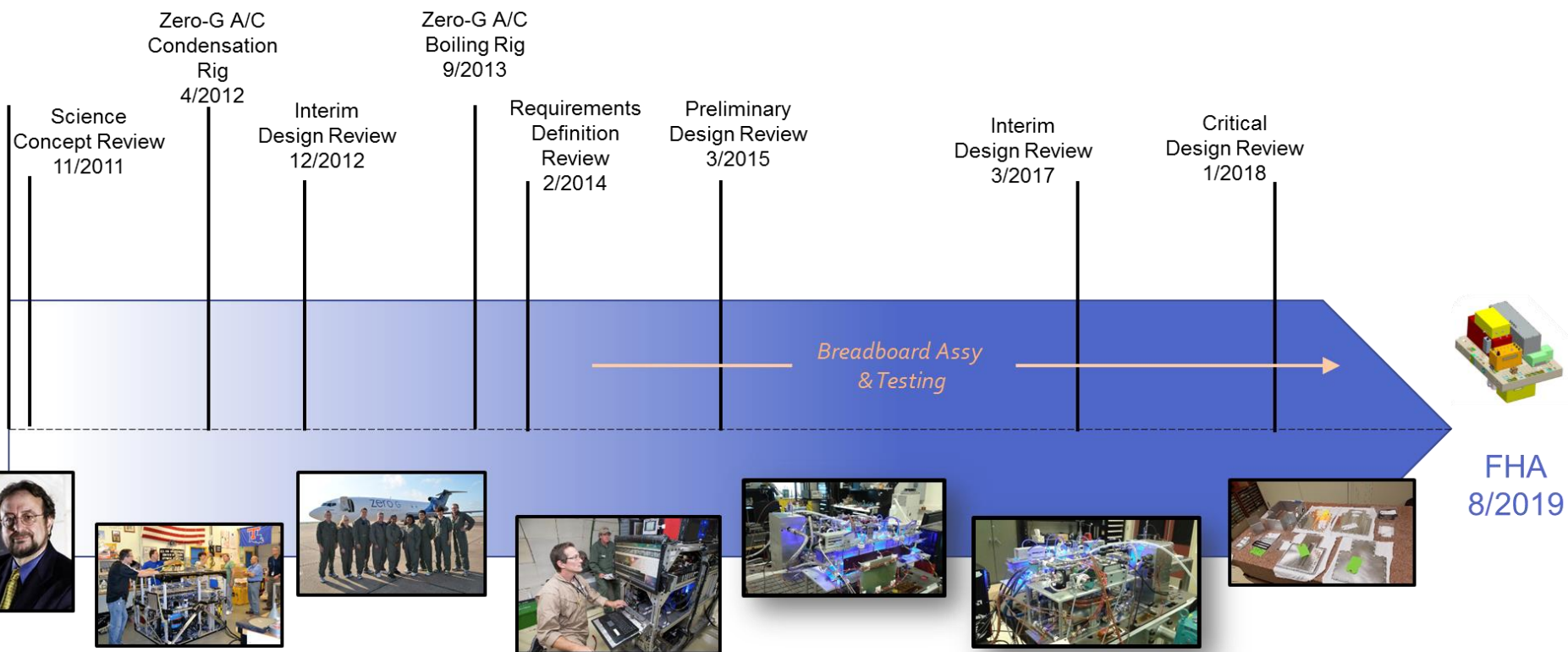
- Thermal Control System (TCS) to control temperature and humidity
- Refrigerator/freezer components
- Advanced water recovery systems

**Nuclear  
Fusion:  
High power/  
long duration  
missions**



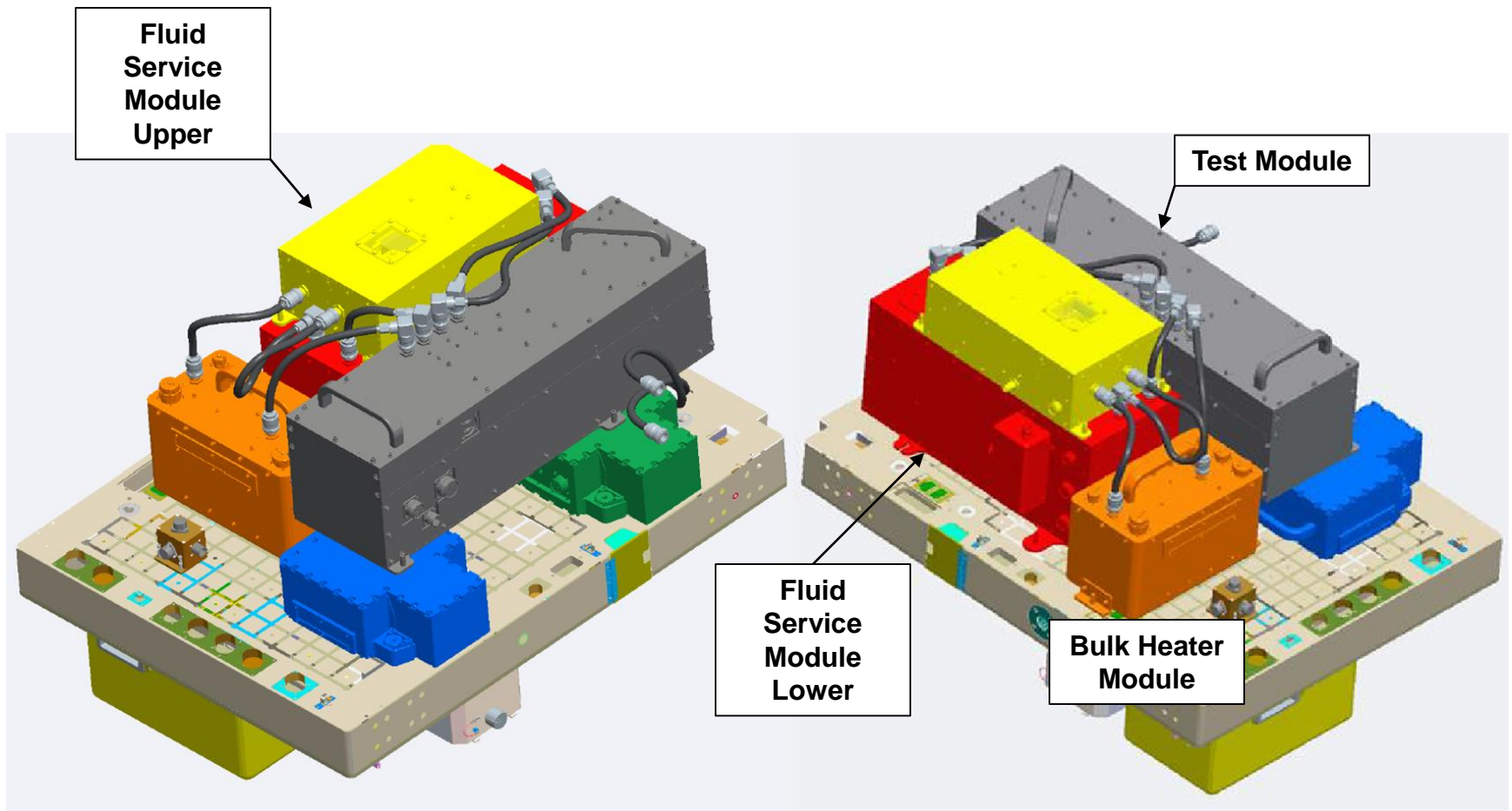


# Project Timeline



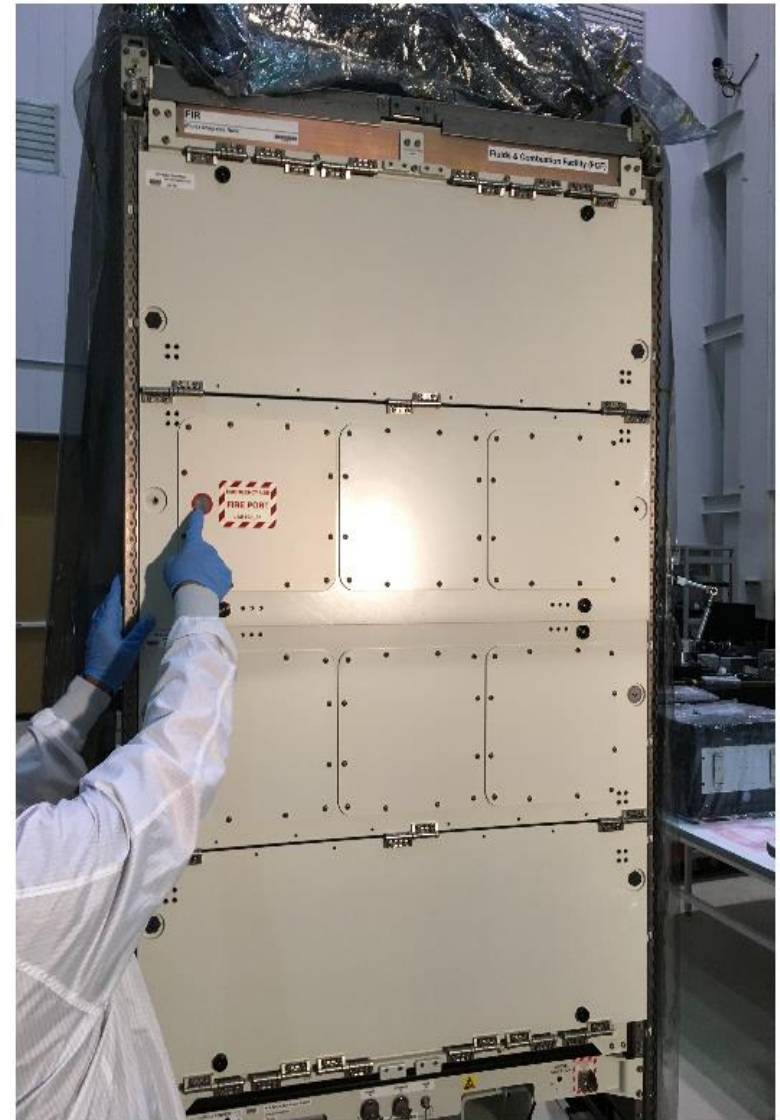
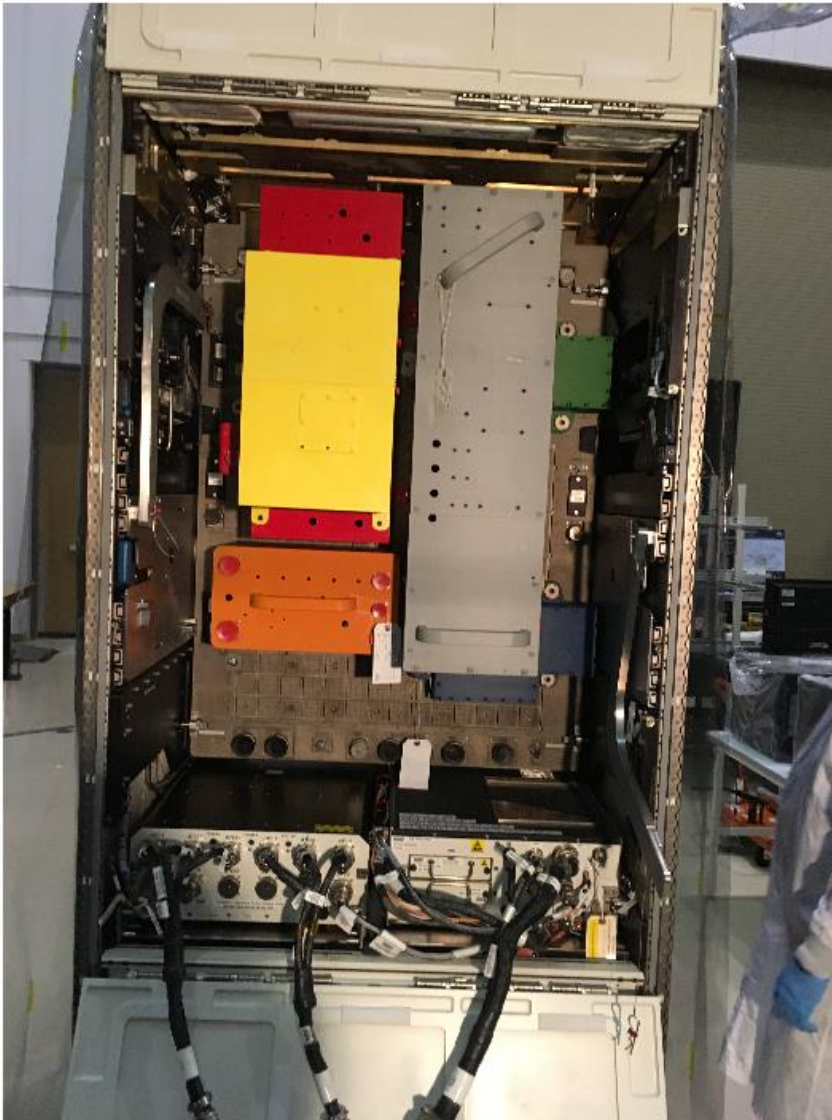


# System Configuration



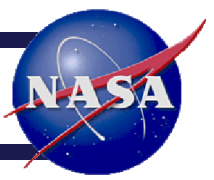


# Fluids Integration Rack



- Operations will be completely controlled from the Telescience Support Center at NASA GRC





# Flow Boiling Module Test Conditions

- **Coolant:** nPFH (normal-Perfluorohexane,  $C_6F_{14}$ )
- **Inlet quality:** 0 – 0.4
- **Inlet pressure:** 100 – 150  $\pm 20 kPa$
- **Liquid inlet velocity:**

$$U = 0.1 - 2.0 \frac{m}{s} \text{ for liquid inlet conditions}$$

- **Mass velocity:**

$$G = 180 - 3,200 \frac{kg}{m^2 s} \text{ for two phase inlet conditions}$$

- **Inlet subcooling:**

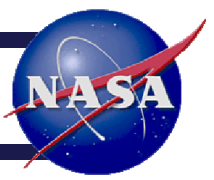
$$DT_{sub,i^*} = 0 - 54^{\circ}F (0 - 30^{\circ}C)$$

- **FBM heater heat flux:**

$$q'' = 0 - 60 \frac{W}{cm^2}$$



# Condensation Module Test Conditions



- **Condensing fluid:** nPFH
- **Cooling fluid:** Water
- **Condensing fluid inlet pressure:** 100 – 150 *kPa*
- **Cooling water inlet temperature:** 68°F (20°C)
- **Mass flow rate of nPFH:**

$$m_{nPFH} = 1 - 14 \frac{g}{s}$$

- **Mass flow rate of cooling water:**

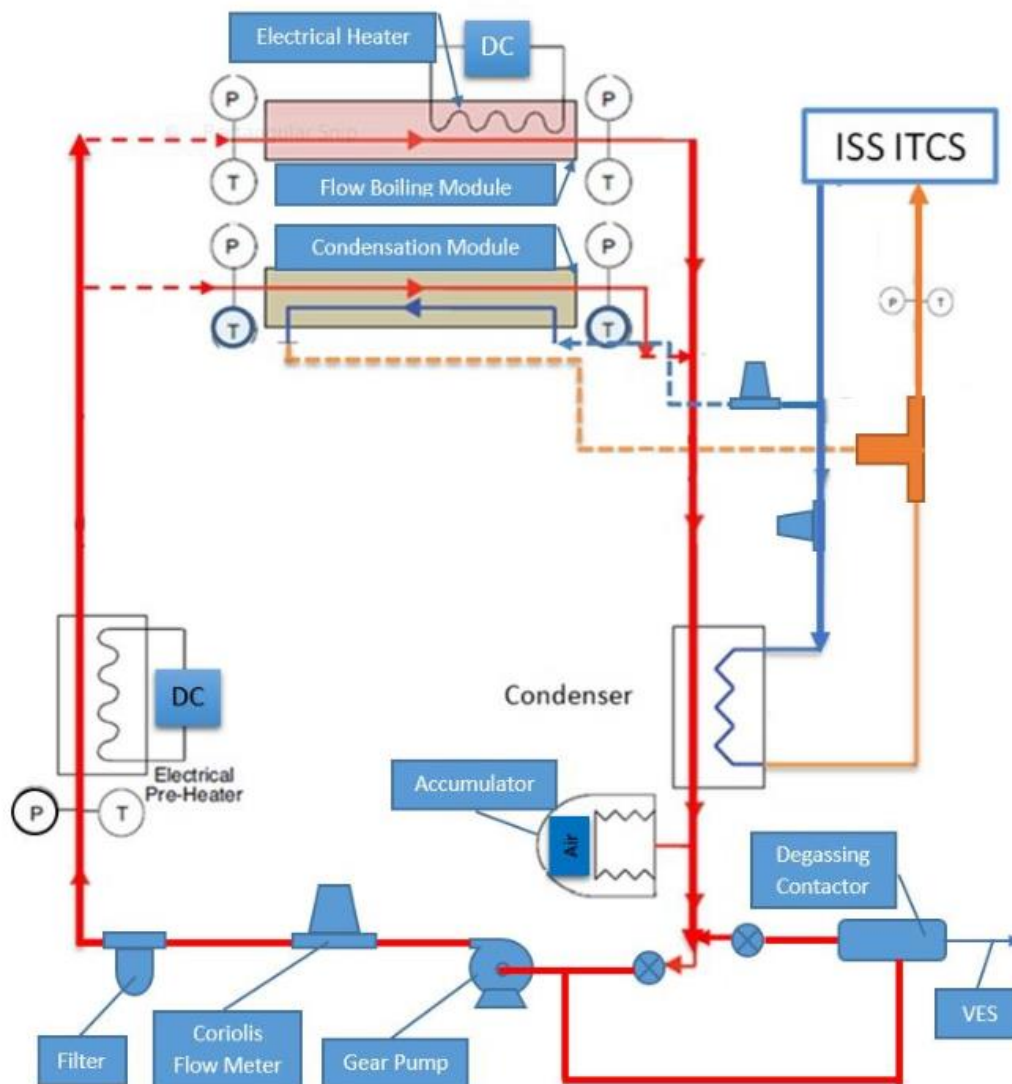
$$m_{water} = 10 - 40 \frac{g}{s}$$

- **Temperature rise of cooling water:**

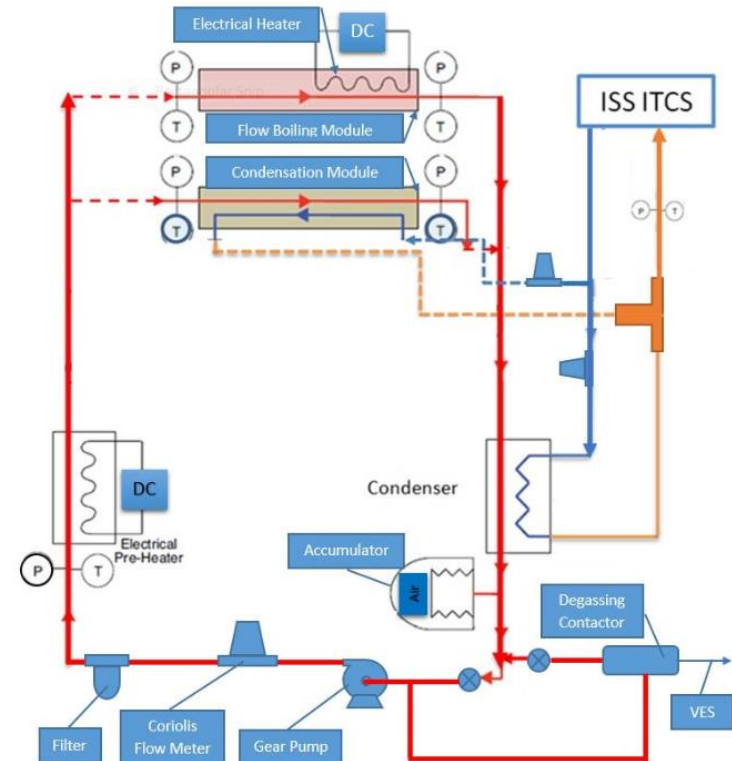
$$\Delta T_{water} = 9 - 54^{\circ}F \text{ (} 5 - 25^{\circ}C \text{)}$$



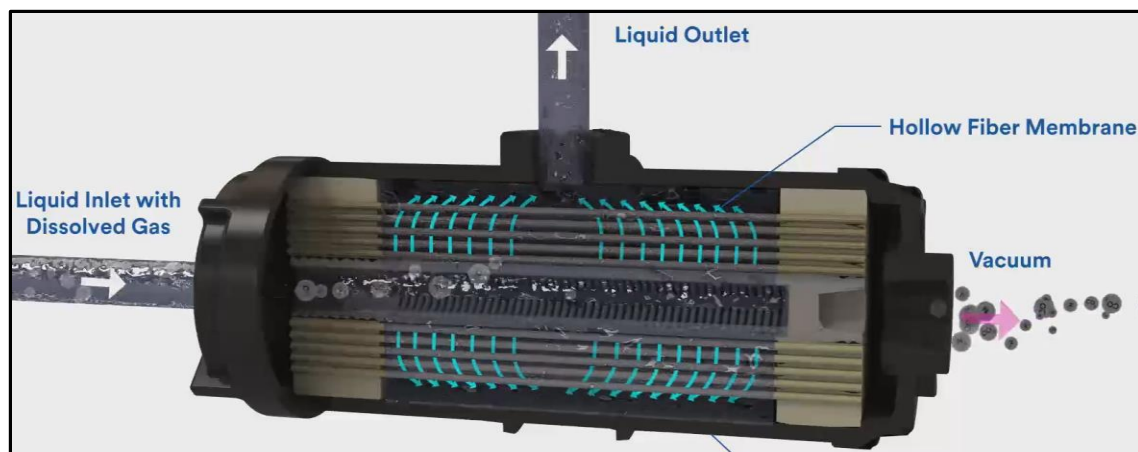
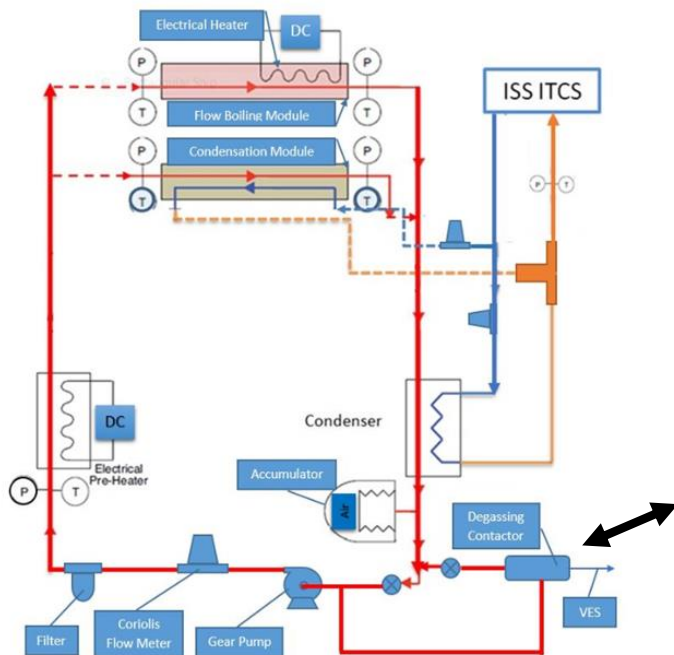
# Simplified Fluid Diagram



- Accumulator
- Condenser
- Pump/ Mass Flow Controller
- Mass Flow Meters
- Test Module Assemblies
- Heater
- Temperature Control

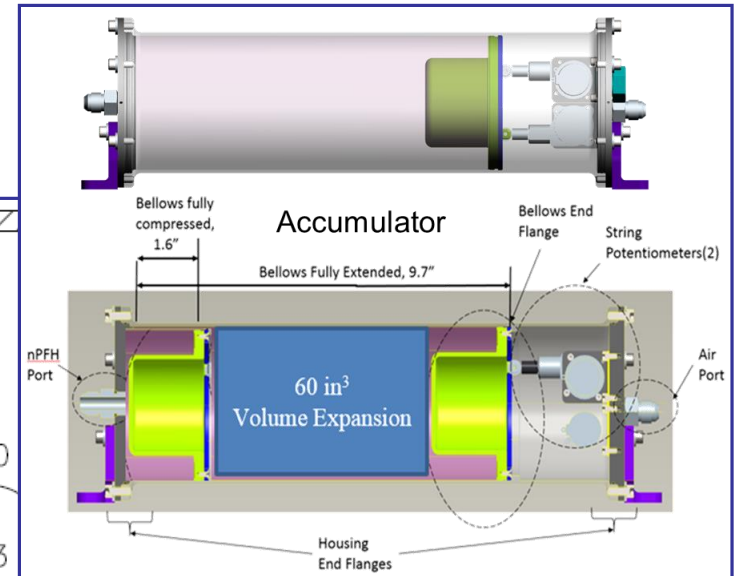
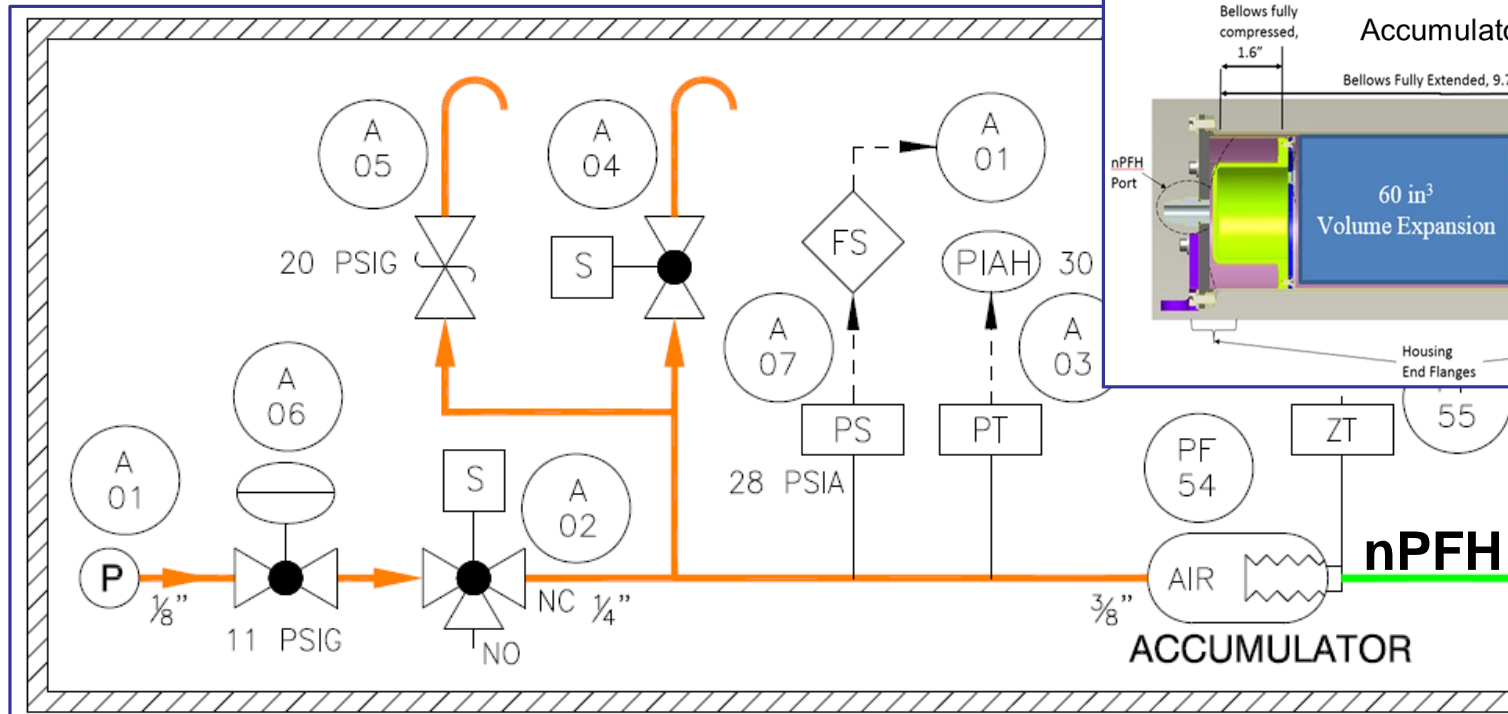


- The test fluid, normal-perfluorohexane (nPFH) has a high affinity for the absorption of oxygen and nitrogen. Small system leaks will cause build up over time of these noncondensable gases causing degradation in heat transfer. The degasser loop removes them.



# Pressure Control - Accumulator

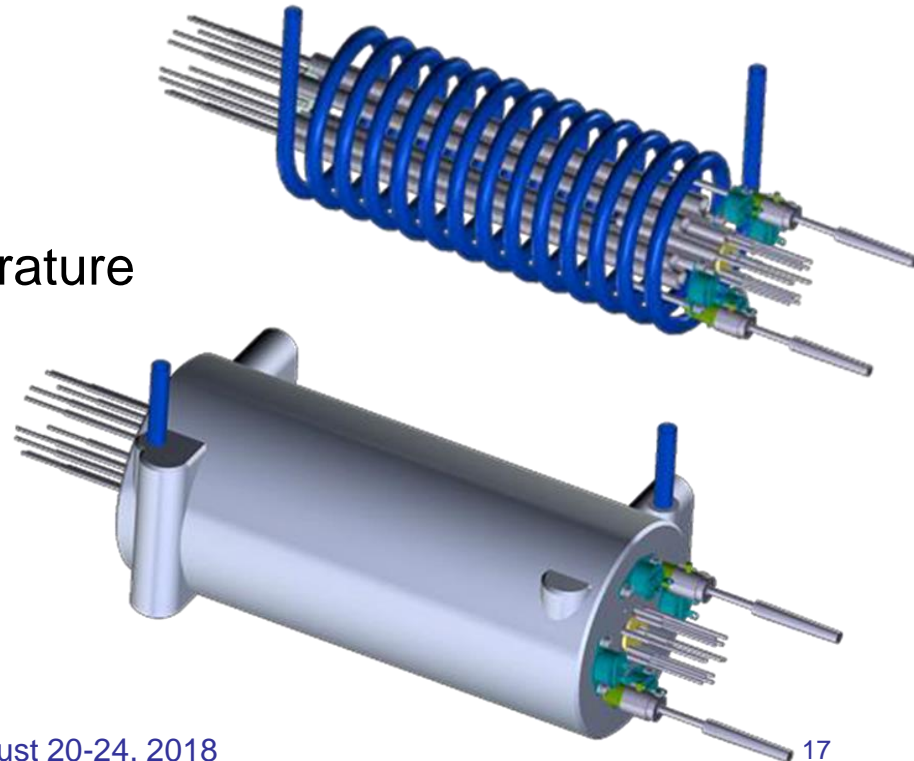
- To control system pressure an air adjustable bellows accumulator was designed.



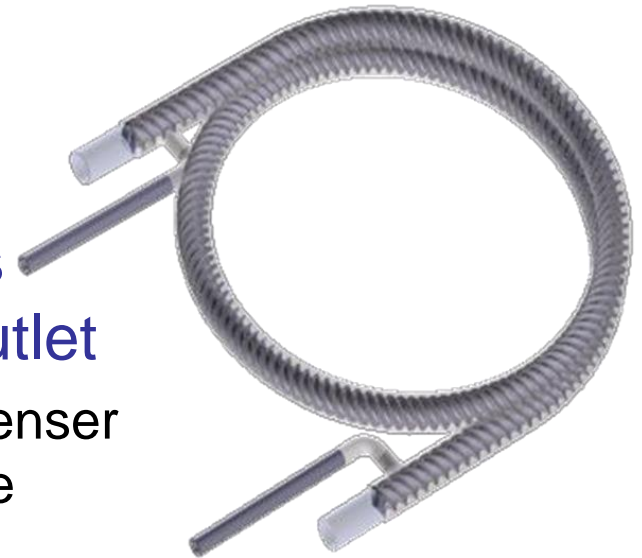


# Temperature Control

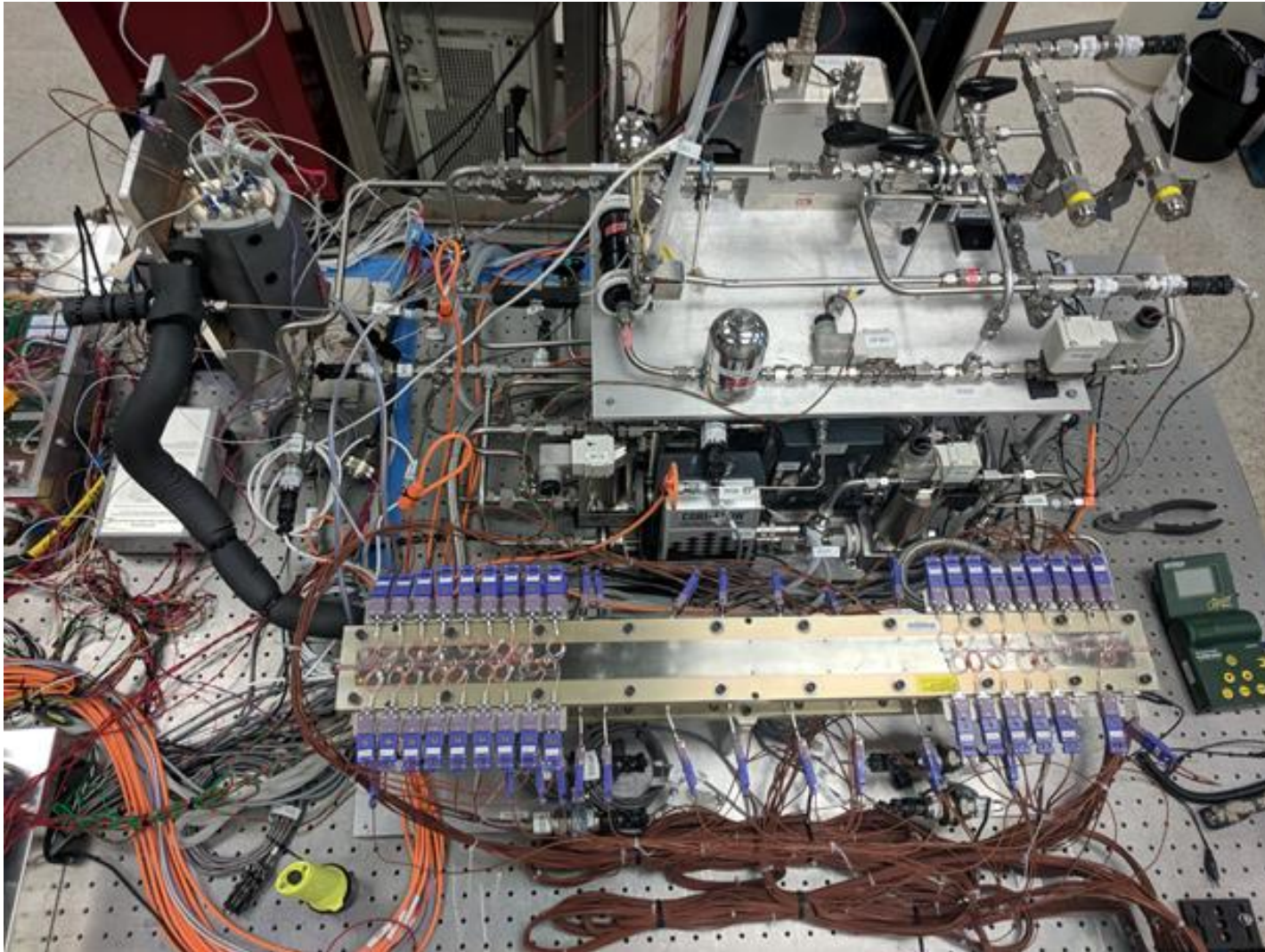
- The Bulk Heater heats the nPFH to provide the temperature needed at the inlet of the test module.
- Designed based on Lessons Learned from previous flight experiment to avoid direct contact of heaters with the nPFH fluid as a safety hazard mitigation
- Construction
  - Coiled stainless steel tubing
  - Cast aluminum thermal mass
  - Embedded heaters and temperature sensors.



- Original breadboard condenser material was copper
  - Great thermal conductivity properties
- Flight unit cannot be copper due to incompatibility with ISS coolant water
- Stainless steel was chosen for flight unit
  - Thermal conductivity < copper
  - Resulted in increased size/  
decreased thermal performance
- During brassboard testing, bubbles were observed in the condenser outlet
  - Theorized that slug flow through condenser combined with decreased performance resulted in some noncondensed vapor
  - Opposing theories suggest noncondensable gas presence due to incomplete degassing operations or transient heating



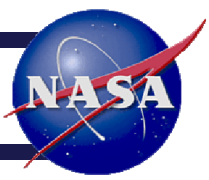
# Brassboard







# Findings During Brassboard Testing



- Precise control of conditions (temp, pressure, quality) at a given location in a closed two-phase flow loop is difficult and requires control of multiple variables (heater power, system pressure, flow rate)
  - Test matrix should be informed by analysis during requirements development to avoid having to make late changes to the design and/or requirements
- Essential to have flight-like hardware in an engineering brassboard as early as possible (i.e. condenser material change being a bigger issue than expected, etc.)
- Try to implement automated controls into an engineering brassboard as early as possible – transient response of a two-phase flow loop can cause surprises when switching from manual to automated control or anticipate transients when designing control loops





# Current Status



- All fluid procurements have been made.
  - Most have been delivered.
- Tube assemblies are being manufactured.
- The accumulator is being assembled.



# Summary



- Currently in hardware assembly phase
- System level testing scheduled to begin in January 2019
- Still targeting FHA of August 2019
- Anticipate test start aboard ISS in early 2020

# Questions?

