

# Thermal Environment Modeling Practices for the Descent Trajectory of Lunar Landers



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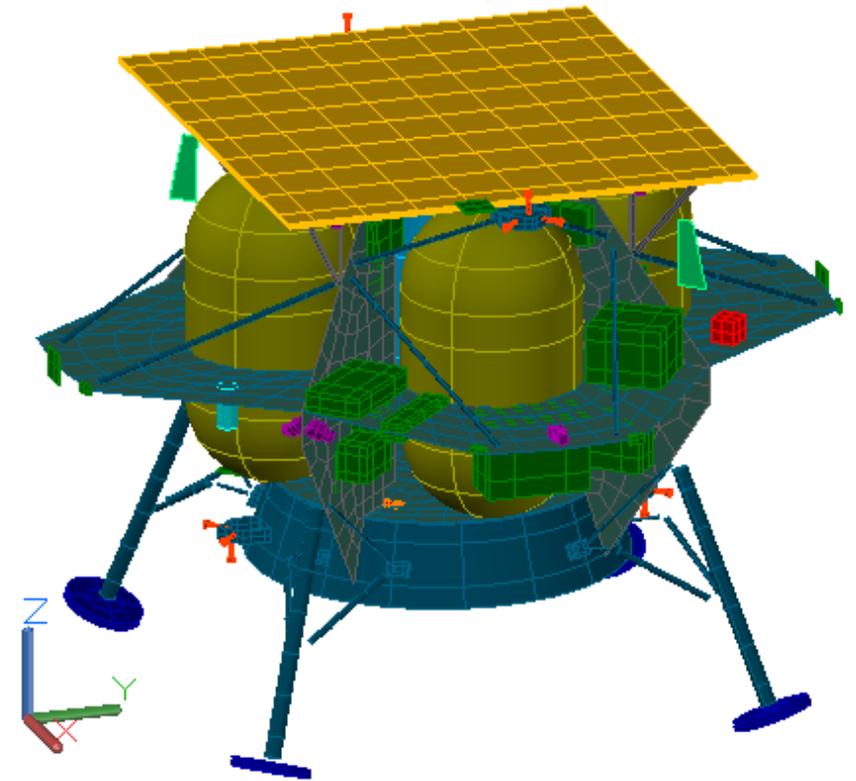
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# Introduction



- This presentation will discuss only one method of modeling the thermal environment for descent trajectories in Thermal Desktop.
- The descent is arguably the most critical point in any lander mission
- The descent phase presents a unique thermal environment compared to the rest of the mission (launch, earth orbit, transit, moon orbit, descent, surface operation)
  - View factor to space decreases
  - Main thruster firing and plume add additional heat
  - All electrical components operating at max power level.
- Heat loads must be modeled properly to ensure that the lander doesn't fail catastrophically

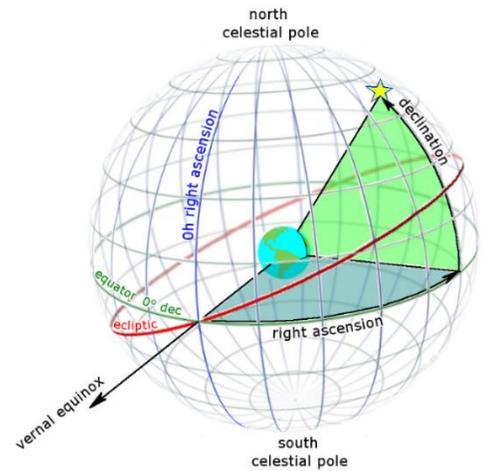




# Building Thermal Desktop Model



- Terrestrial heating rate case used
- Right Ascension of sun and right ascension of prime meridian are the first inputs needed
  - Used to control and set the spatial time and location of the moon.
  - Determined using location of the sun moon-centered Cartesian coordinates
- Latitude, longitude and altitude versus time control the location of the lander for each time step



Orbit: test

Lat/Long Input   Orientation   Planetary Data   Solar   Diffuse Sky Solar   Albedo   Diffuse Sky IR   Ground IR   ASHRAE   Fast Spin   Comment

Right Ascension Definitions

User Specified

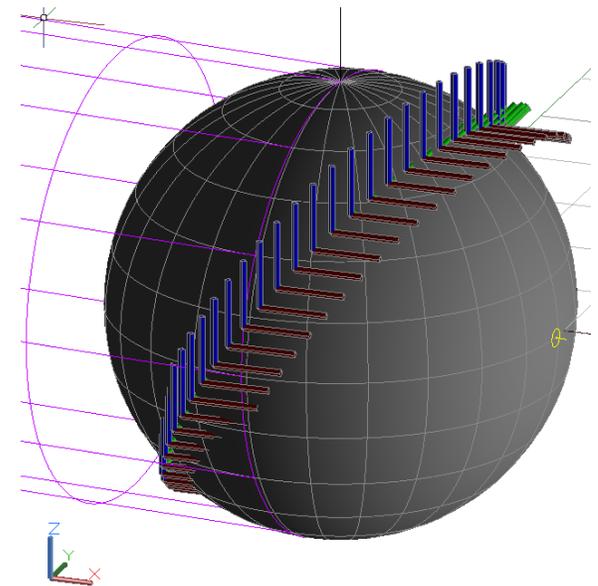
R.A. of Sun:

R.A. of Prime Meridian:

Use Date/Time

| time [sec] | latitude [deg] | longitude [deg] | altitude [km] | z-rotation [deg] |
|------------|----------------|-----------------|---------------|------------------|
| 0.1        | -14.116433     | 75.499934       | 102.16025     | 0                |
| 116.5      | -18.953012     | 79.061249       | 102.13733     | 0                |
| 232.9      | -23.716957     | 82.835058       | 102.1171      | 0                |
| 349.3      | -28.381661     | 86.893775       | 102.0997      | 0                |
| 465.7      | -32.914116     | 91.322607       | 102.08526     | 0                |
| 582.1      | -37.272477     | 96.222186       | 102.07394     | 0                |
| 698.5      | -41.402994     | 101.70968       | 102.06587     | 0                |
| 814.9      | -45.236457     | 107.91587       | 102.06111     | 0                |
| 931.3      | -48.684779     | 114.97344       | 102.05972     | 0                |
| 1047.7     | -51.639438     | 122.98973       | 102.06175     | 0                |
| 1164.1     | -53.975105     | 131.99816       | 102.0672      | 0                |
| 1280.5     | -55.562874     | 141.89458       | 102.07606     | 0                |
| 1396.9     | -56.295141     | 152.39098       | 102.0883      | 0                |
| 1513.3     | -56.115733     | 163.0393        | 102.10469     | 0                |
| 1629.7     | -55.03895      | 173.34648       | 102.1239      | 0                |
| 1746.1     | -53.144428     | 177.08163       | 102.14507     | 0                |
| 1862.5     | -50.555423     | 168.46939       | 102.16254     | 0                |
| 1978.9     | -47.434398     | 160.92168       | 101.88549     | 0                |
| 2095.3     | -43.871666     | 154.27259       | 101.14808     | 0                |
| 2211.7     | -39.96213      | 148.40341       | 99.95799      | 0                |

OK   Cancel   Help

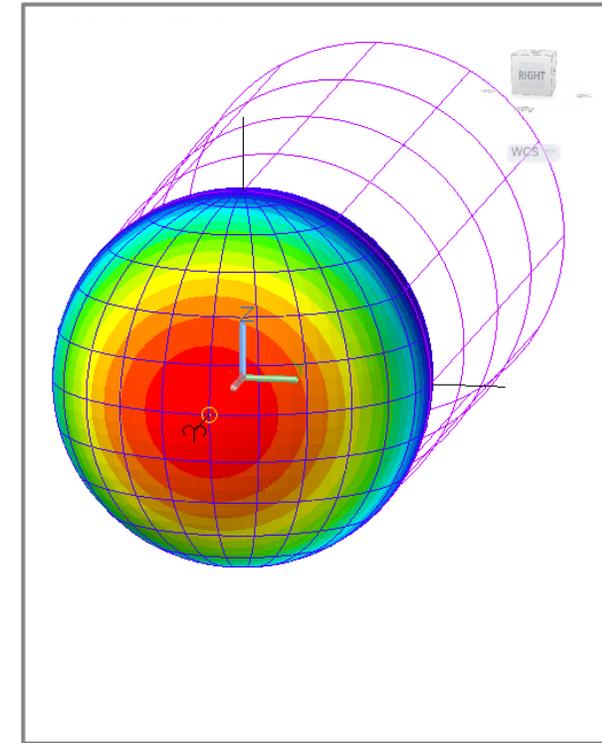
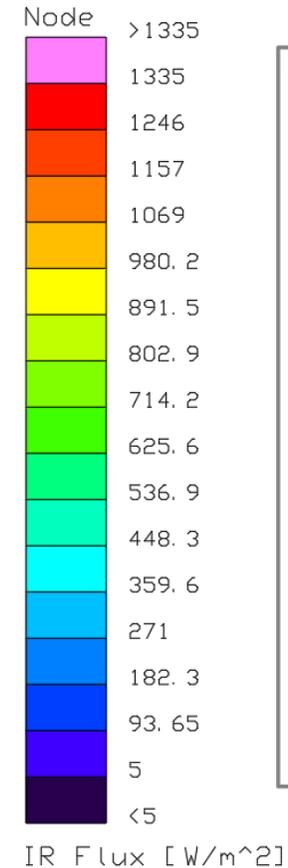




# Defining Thermal Environment



- Orientation
  - Allows user to define orientation of Lander during descent
- Earth's Moon's planetary data
  - Radius, gravitational mass, inclination, sidereal period, and mean solar day
- Ground IR (seen to right)
  - Allows user to define planetshine vs. location

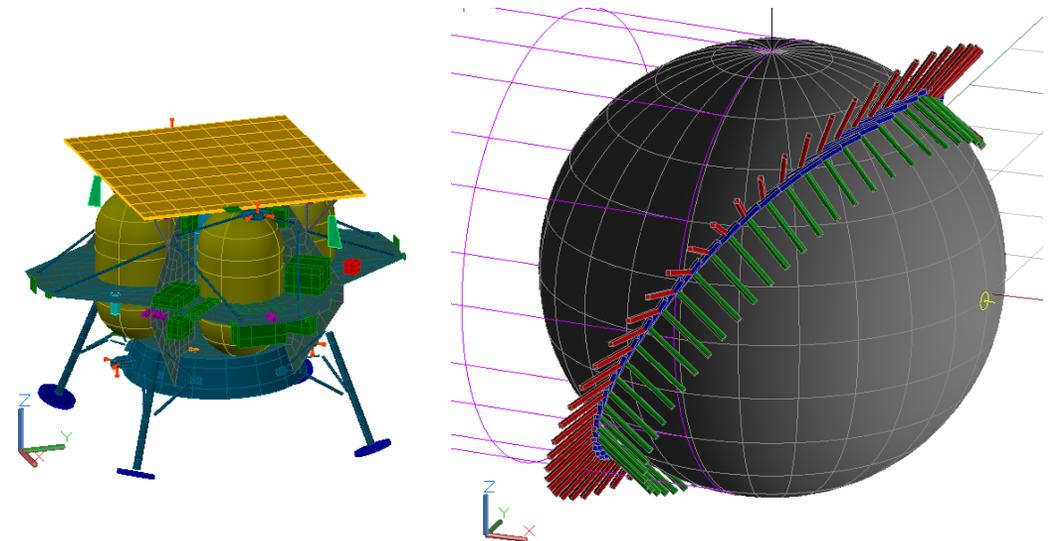
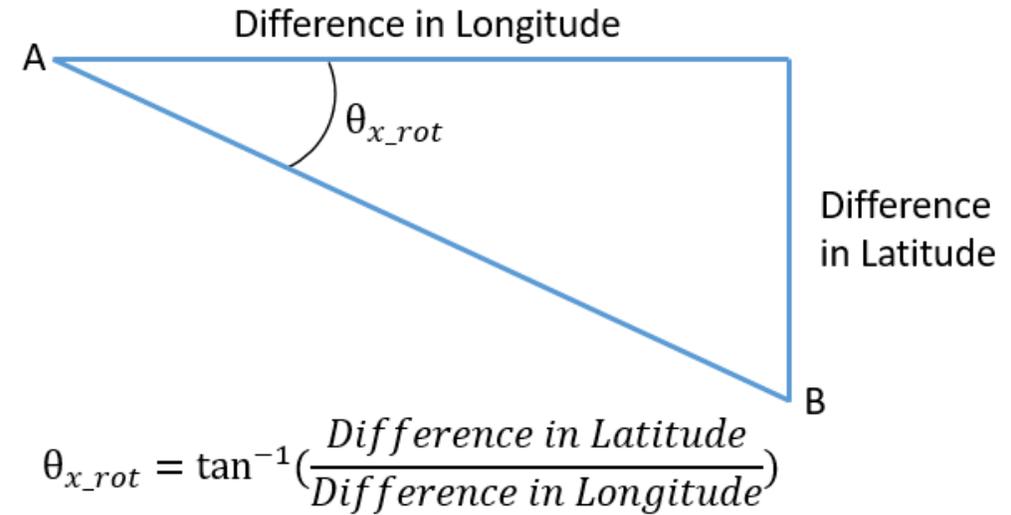




# Ensuring Proper Rotation



- Rotate along Z-axis by longitude plus value of R.A. of the prime meridian
  - Result: X-axis of lander points through Z-axis of moon
- Rotate along Y-axis by value of latitude
  - Result: X-axis of lander points through center of moon
- Rotate along X-axis by the inverse tangent of change in latitude over change in longitude.
  - Result: Z-axis of lander points along velocity vector





# Additional Rotations Required



- If more than 3 rotations are desired, then the use of rotation matrices is required.
- Rotation matrices allow the conversion of any number of rotations down to 3 base rotations.
- To do this you:
  - Rotate lander by any number of rotations at each time step
  - Obtain a 3X3 matrix for each time step
  - Equate the 3X3 matrix at each time step to the base rotation matrix seen below

$$R(i) = I_3 * R_z(\text{Longitude}(i)) * R_y(\text{Latitude}(i)) * R_x(\theta_{x_{rot}}(i)) * R_y(135^\circ)$$

$$R_x(\theta) = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos \theta & -\sin \theta \\ 0 & \sin \theta & \cos \theta \end{bmatrix}$$

$$R_y(\theta) = \begin{bmatrix} \cos \theta & 0 & -\sin \theta \\ 0 & 1 & 0 \\ \sin \theta & 0 & \cos \theta \end{bmatrix}$$

$$R_z(\theta) = \begin{bmatrix} \cos \theta & -\sin \theta & 0 \\ \sin \theta & \cos \theta & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

$$R = R_z(\phi) * R_y(\theta) * R_x(\psi)$$

$$= \begin{bmatrix} \cos \theta \cos \phi & \sin \psi \sin \theta \cos \phi - \cos \psi \sin \phi & \cos \psi \sin \theta \cos \phi + \sin \psi \sin \phi \\ \cos \theta \sin \phi & \sin \psi \sin \theta \sin \phi + \cos \psi \cos \phi & \cos \psi \sin \theta \sin \phi - \sin \psi \cos \phi \\ -\sin \theta & \sin \psi \cos \theta & \cos \psi \cos \theta \end{bmatrix}$$



# 2-Argument Arctangent



- Equate the final matrix at each time step to the base rotation matrix below and solve for theta ( $\theta$ ), phi ( $\phi$ ), and psi ( $\psi$ )
- 2 solutions for both phi and psi
  - Must use 2-argument arctangent

$$\theta = \text{asin}(-r_{31})$$

$$\phi = \text{atan2}(r_{21}, r_{11})$$

$$\psi = \text{atan2}(r_{32}, r_{33})$$

$$\text{atan2}(y, x) = \begin{cases} \arctan\left(\frac{y}{x}\right) & \text{if } x > 0, \\ \arctan\left(\frac{y}{x}\right) + \pi & \text{if } x < 0 \text{ and } y \geq 0, \\ \arctan\left(\frac{y}{x}\right) - \pi & \text{if } x < 0 \text{ and } y < 0, \\ +\frac{\pi}{2} & \text{if } x = 0 \text{ and } y > 0, \\ -\frac{\pi}{2} & \text{if } x = 0 \text{ and } y < 0, \\ \text{undefined} & \text{if } x = 0 \text{ and } y = 0. \end{cases}$$

$$R = R_z(\phi) * R_y(\theta) * R_x(\psi)$$

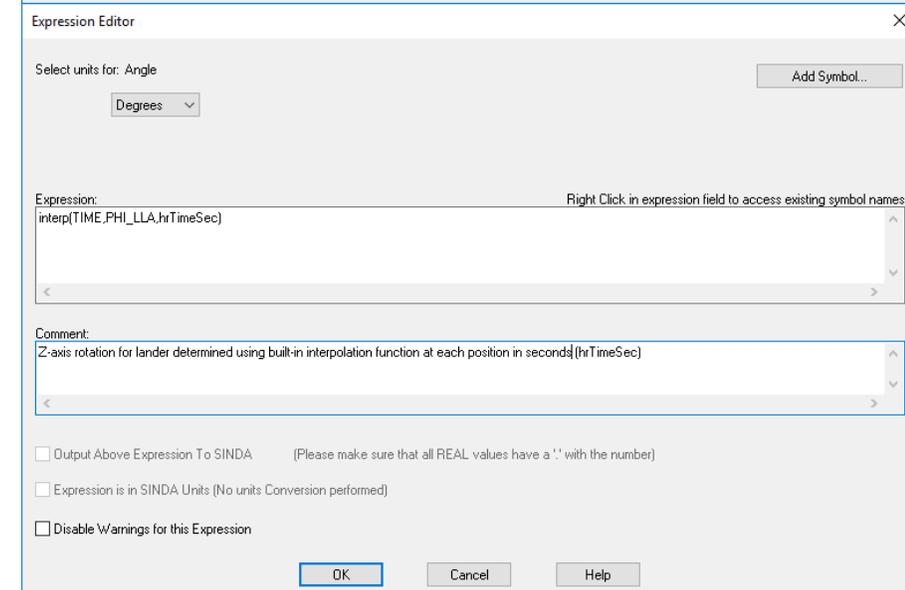
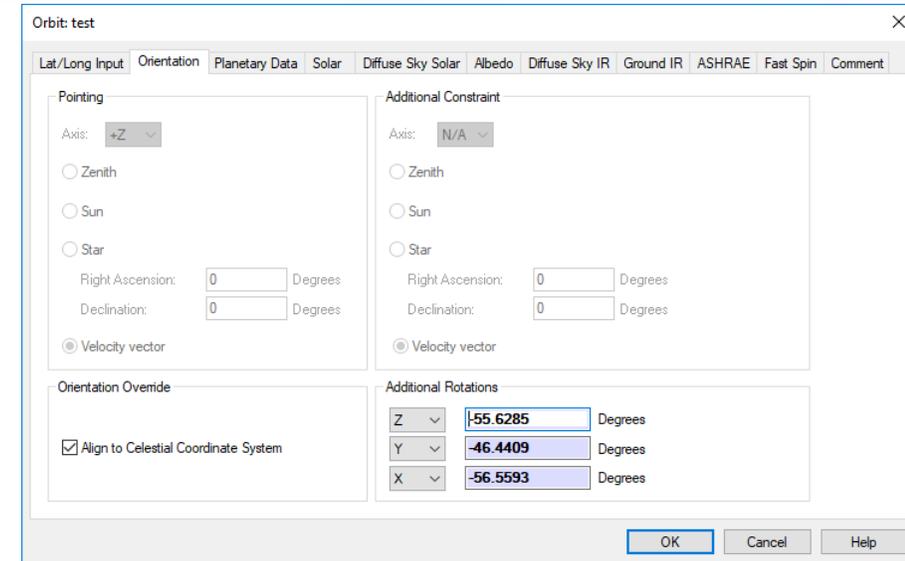
$$= \begin{bmatrix} \cos\theta \cos\phi & \sin\psi \sin\theta \cos\phi - \cos\psi \sin\phi & \cos\psi \sin\theta \cos\phi + \sin\psi \sin\phi \\ \cos\theta \sin\phi & \sin\psi \sin\theta \sin\phi + \cos\psi \cos\phi & \cos\psi \sin\theta \sin\phi - \sin\psi \cos\phi \\ -\sin\theta & \sin\psi \cos\theta & \cos\psi \cos\theta \end{bmatrix}$$



# Building Thermal Desktop Model



- Create array symbols for theta, phi, and psi in the symbol manager
- Add in the additional rotations on the orientation tab for terrestrial heating rate cases
- Select “align to celestial coordinate system”
- Interpolate between time steps of heating rate case

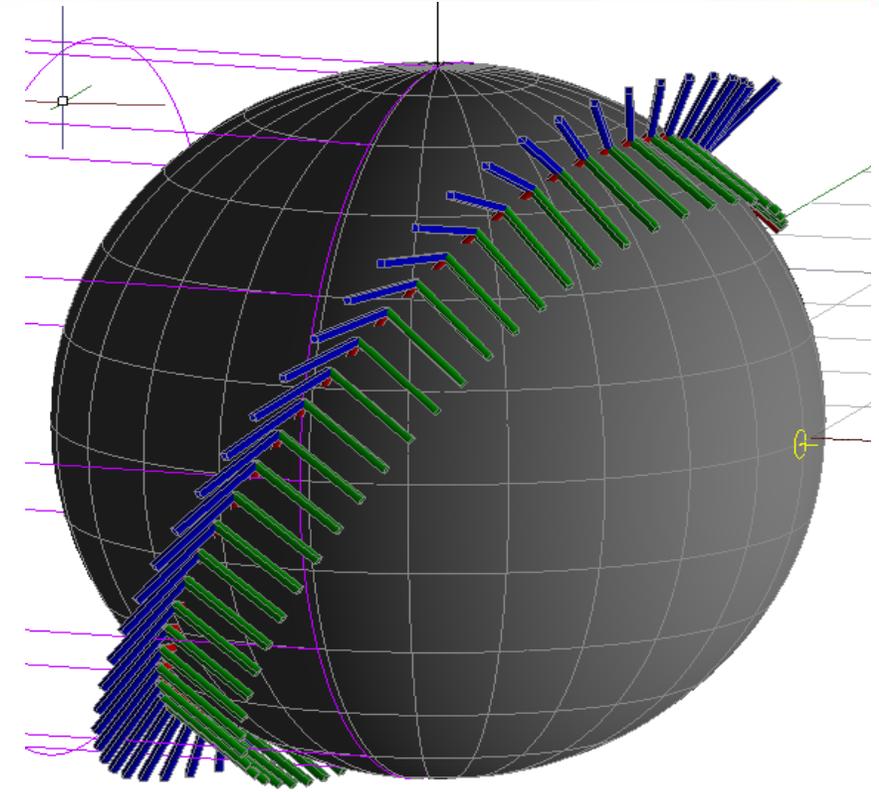
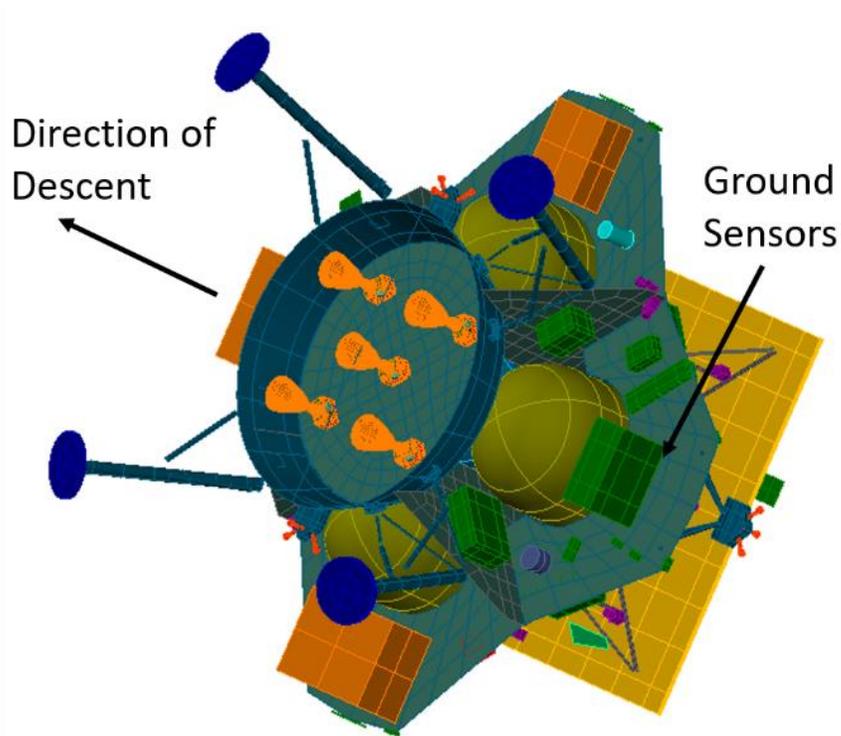
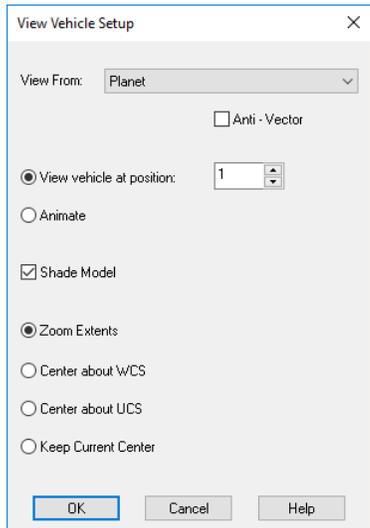
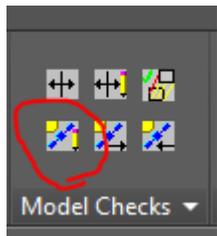




# Quality Checks



- Two methods to check that the lander is properly oriented at each time step
  - Display the orbit in the heating rate case manager
  - View the lander from the planet



- Modeling the thermal environment for a lander descent correctly is essential for a successful mission. This can be difficult due to the transient nature of a descent and the addition of new thermal conditions such as component heat loads, changing view factors/radiative sink temperatures, and thruster/plume heat loads.
- The method shown above is one way to obtain the desired results but is very versatile and easy to use if more detailed rotations are required.

- Questions?
- Comments?
- Other ways of achieving desired effects?