

Thermal Environment Modeling Practices for the Descent Trajectory of Lunar Landers



Alex Szerszen, Jacobs MSFC ES22

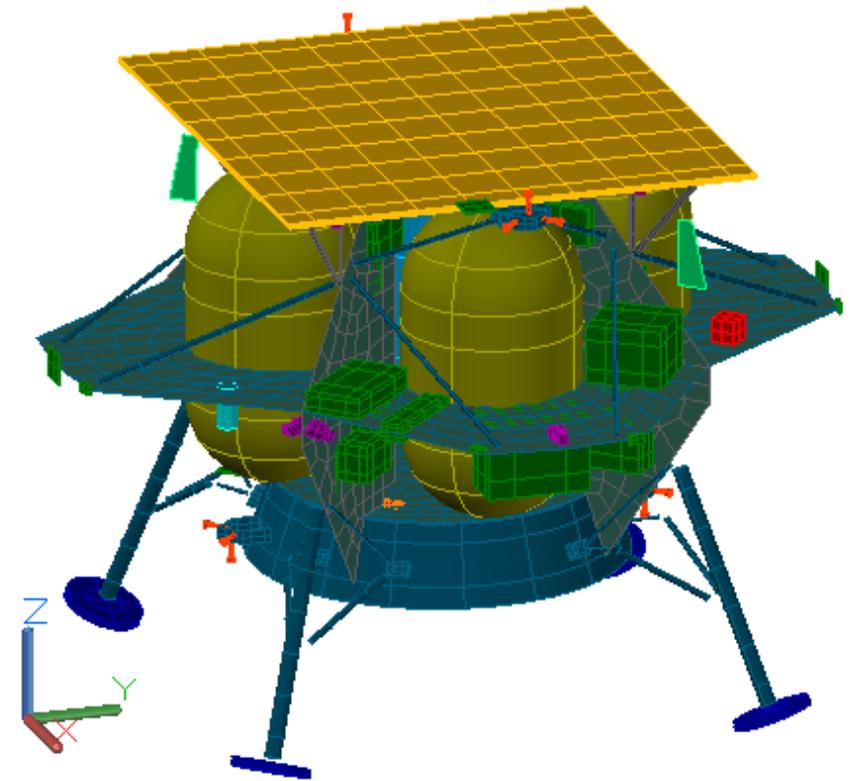
08-26-2019



Introduction



- This presentation will discuss only one method of modeling the thermal environment for descent trajectories in Thermal Desktop.
- The descent is arguably the most critical point in any lander mission
- The descent phase presents a unique thermal environment compared to the rest of the mission (launch, earth orbit, transit, moon orbit, descent, surface operation)
 - View factor to space decreases
 - Main thruster firing and plume add additional heat
 - All electrical components operating at max power level.
- Heat loads must be modeled properly to ensure that the lander doesn't fail catastrophically

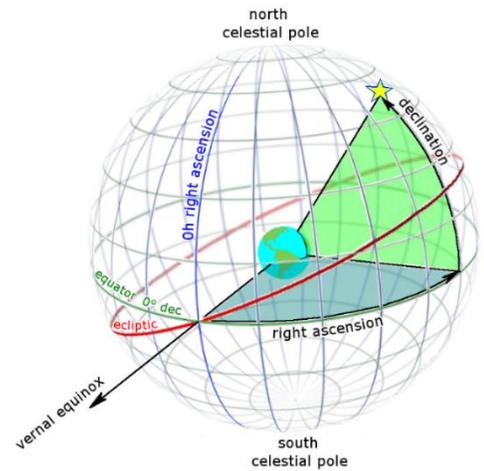




Building Thermal Desktop Model



- Terrestrial heating rate case used
- Right Ascension of sun and right ascension of prime meridian are the first inputs needed
 - Used to control and set the spatial time and location of the moon.
 - Determined using location of the sun moon-centered Cartesian coordinates
- Latitude, longitude and altitude versus time control the location of the lander for each time step



Orbit: test

Lat/Long Input Orientation Planetary Data Solar Diffuse Sky Solar Albedo Diffuse Sky IR Ground IR ASHRAE Fast Spin Comment

Right Ascension Definitions

User Specified

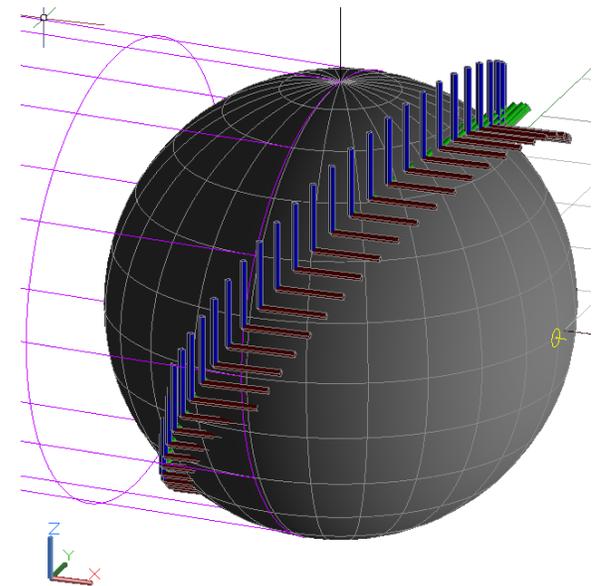
R.A. of Sun

R.A. of Prime Meridian

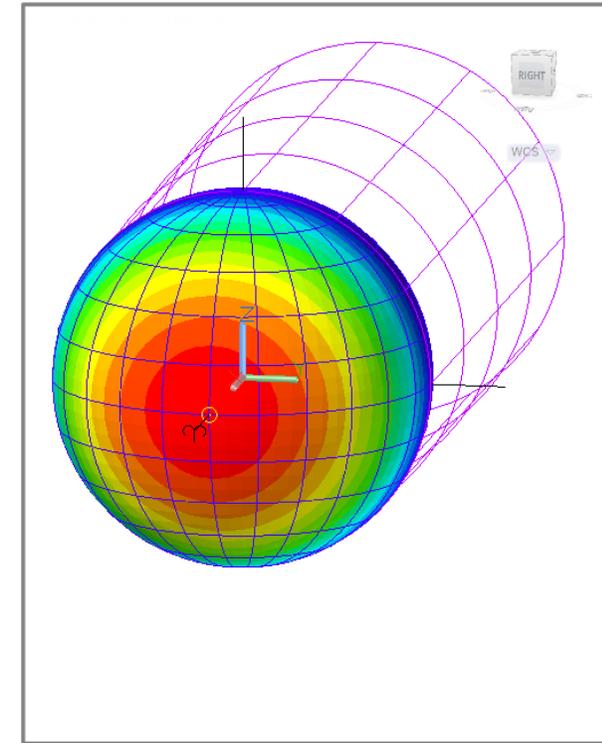
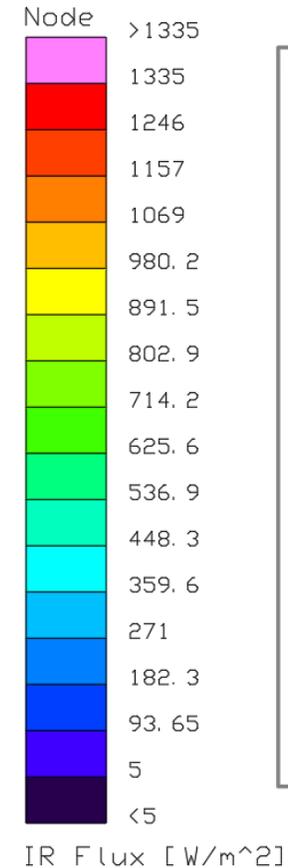
Use Date/Time

time [sec]	latitude [deg]	longitude [deg]	altitude [km]	z-rotation [deg]
0.1	-14.116433	75.499934	102.16025	0
116.5	-18.953012	79.061249	102.13733	0
232.9	-23.716957	82.835058	102.1171	0
349.3	-28.381661	86.893775	102.0997	0
465.7	-32.914116	91.322607	102.08526	0
582.1	-37.272477	96.222186	102.07394	0
698.5	-41.402994	101.70968	102.06587	0
814.9	-45.236457	107.91587	102.06111	0
931.3	-48.684779	114.97344	102.05972	0
1047.7	-51.639438	122.98973	102.06175	0
1164.1	-53.975105	131.99816	102.0672	0
1280.5	-55.562874	141.89458	102.07606	0
1396.9	-56.295141	152.39098	102.0883	0
1513.3	-56.115733	163.0393	102.10469	0
1629.7	-55.03895	173.34648	102.1239	0
1746.1	-53.144428	177.08163	102.14507	0
1862.5	-50.555423	168.46939	102.16254	0
1978.9	-47.434398	160.92168	101.88549	0
2095.3	-43.871666	154.27259	101.14808	0
2211.7	-39.96213	148.40341	99.95799	0

OK Cancel Help



- Orientation
 - Allows user to define orientation of Lander during descent
- Earth's Moon's planetary data
 - Radius, gravitational mass, inclination, sidereal period, and mean solar day
- Ground IR (seen to right)
 - Allows user to define planetshine vs. location

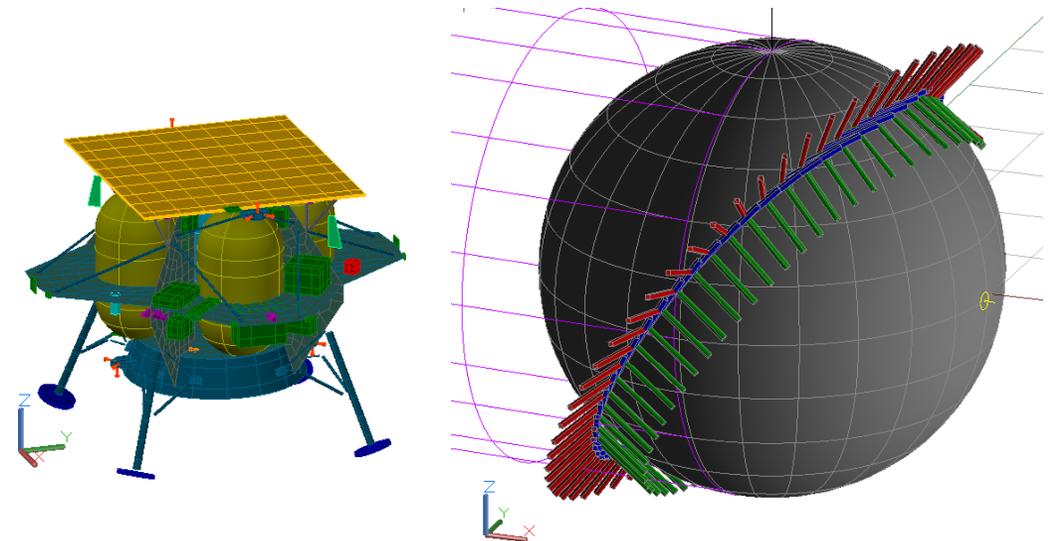
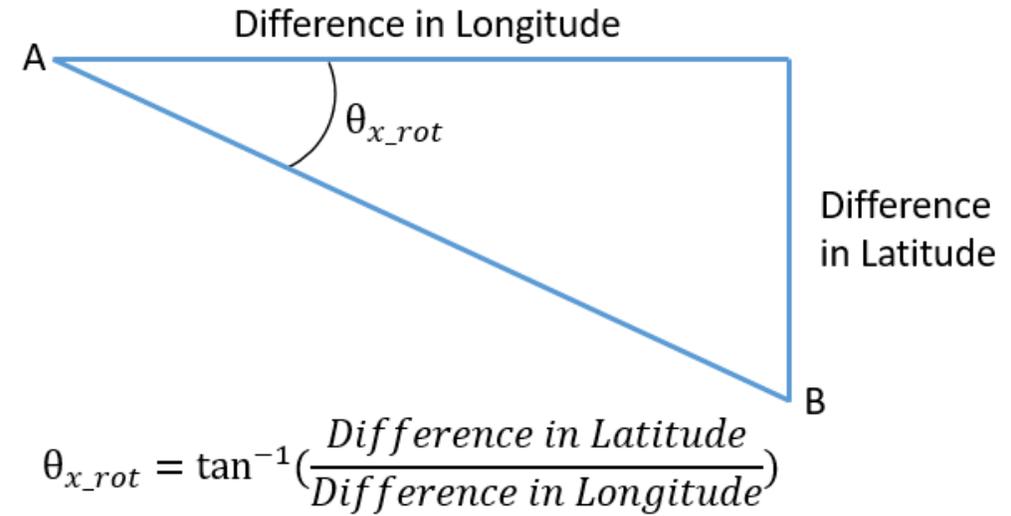




Ensuring Proper Rotation



- Rotate along Z-axis by longitude plus value of R.A. of the prime meridian
 - Result: X-axis of lander points through Z-axis of moon
- Rotate along Y-axis by value of latitude
 - Result: X-axis of lander points through center of moon
- Rotate along X-axis by the inverse tangent of change in latitude over change in longitude.
 - Result: Z-axis of lander points along velocity vector





Additional Rotations Required



- If more than 3 rotations are desired, then the use of rotation matrices is required.
- Rotation matrices allow the conversion of any number of rotations down to 3 base rotations.
- To do this you:
 - Rotate lander by any number of rotations at each time step
 - Obtain a 3X3 matrix for each time step
 - Equate the 3X3 matrix at each time step to the base rotation matrix seen below

$$R(i) = I_3 * R_z(\text{Longitude}(i)) * R_y(\text{Latitude}(i)) * R_x(\theta_{x_{rot}}(i)) * R_y(135^\circ)$$

$$R = R_z(\phi) * R_y(\theta) * R_x(\psi)$$

$$= \begin{bmatrix} \cos\theta \cos\phi & \sin\psi \sin\theta \cos\phi - \cos\psi \sin\phi & \cos\psi \sin\theta \cos\phi + \sin\psi \sin\phi \\ \cos\theta \sin\phi & \sin\psi \sin\theta \sin\phi + \cos\psi \cos\phi & \cos\psi \sin\theta \sin\phi - \sin\psi \cos\phi \\ -\sin\theta & \sin\psi \cos\theta & \cos\psi \cos\theta \end{bmatrix}$$

$$R_x(\theta) = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos\theta & -\sin\theta \\ 0 & \sin\theta & \cos\theta \end{bmatrix}$$

$$R_y(\theta) = \begin{bmatrix} \cos\theta & 0 & -\sin\theta \\ 0 & 1 & 0 \\ \sin\theta & 0 & \cos\theta \end{bmatrix}$$

$$R_z(\theta) = \begin{bmatrix} \cos\theta & -\sin\theta & 0 \\ \sin\theta & \cos\theta & 0 \\ 0 & 0 & 1 \end{bmatrix}$$



2-Argument Arctangent



- Equate the final matrix at each time step to the base rotation matrix below and solve for theta (θ), phi (ϕ), and psi (ψ)
- 2 solutions for both phi and psi
 - Must use 2-argument arctangent

$$\theta = \text{asin}(-r_{31})$$

$$\phi = \text{atan2}(r_{21}, r_{11})$$

$$\psi = \text{atan2}(r_{32}, r_{33})$$

$$\text{atan2}(y, x) = \begin{cases} \arctan\left(\frac{y}{x}\right) & \text{if } x > 0, \\ \arctan\left(\frac{y}{x}\right) + \pi & \text{if } x < 0 \text{ and } y \geq 0, \\ \arctan\left(\frac{y}{x}\right) - \pi & \text{if } x < 0 \text{ and } y < 0, \\ +\frac{\pi}{2} & \text{if } x = 0 \text{ and } y > 0, \\ -\frac{\pi}{2} & \text{if } x = 0 \text{ and } y < 0, \\ \text{undefined} & \text{if } x = 0 \text{ and } y = 0. \end{cases}$$

$$R = R_z(\phi) * R_y(\theta) * R_x(\psi)$$

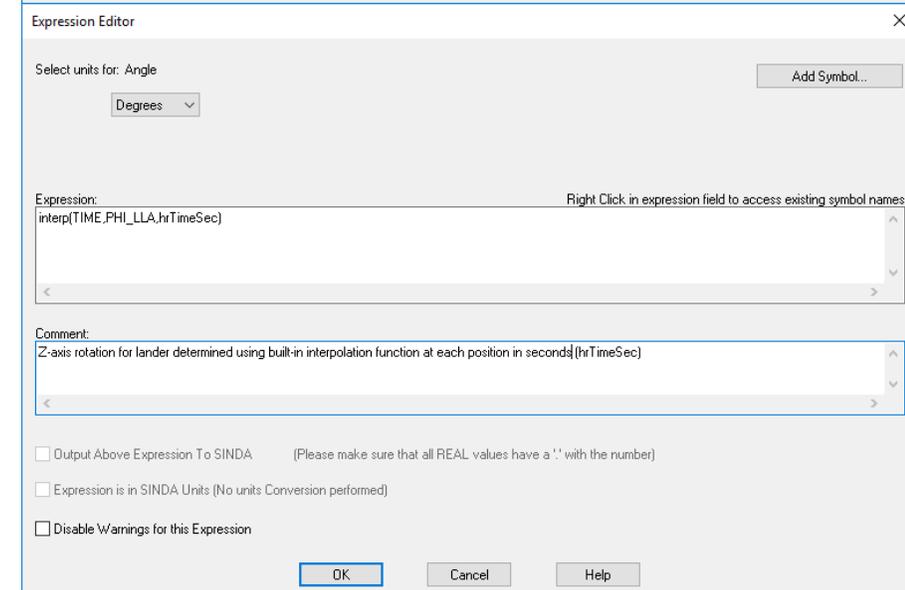
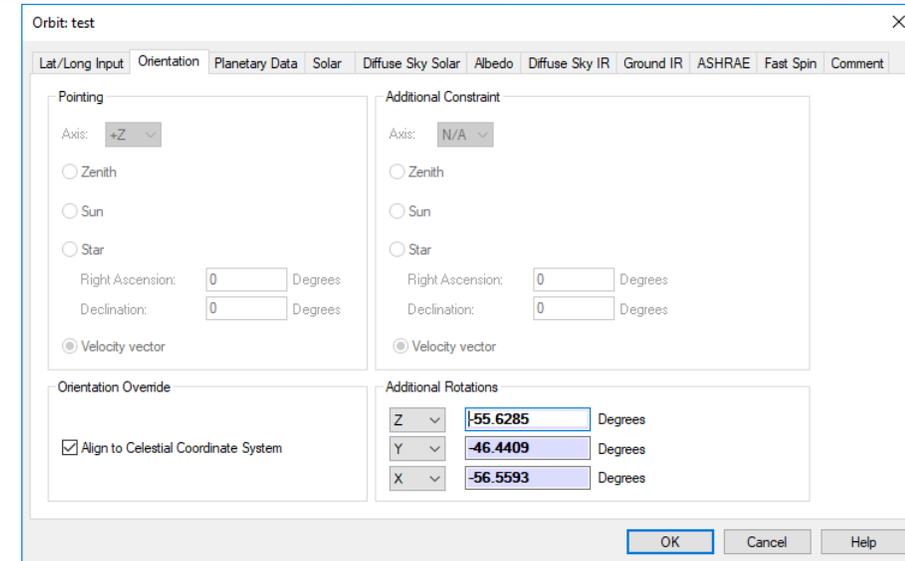
$$= \begin{bmatrix} \cos\theta \cos\phi & \sin\psi \sin\theta \cos\phi - \cos\psi \sin\phi & \cos\psi \sin\theta \cos\phi + \sin\psi \sin\phi \\ \cos\theta \sin\phi & \sin\psi \sin\theta \sin\phi + \cos\psi \cos\phi & \cos\psi \sin\theta \sin\phi - \sin\psi \cos\phi \\ -\sin\theta & \sin\psi \cos\theta & \cos\psi \cos\theta \end{bmatrix}$$



Building Thermal Desktop Model



- Create array symbols for theta, phi, and psi in the symbol manager
- Add in the additional rotations on the orientation tab for terrestrial heating rate cases
- Select “align to celestial coordinate system”
- Interpolate between time steps of heating rate case

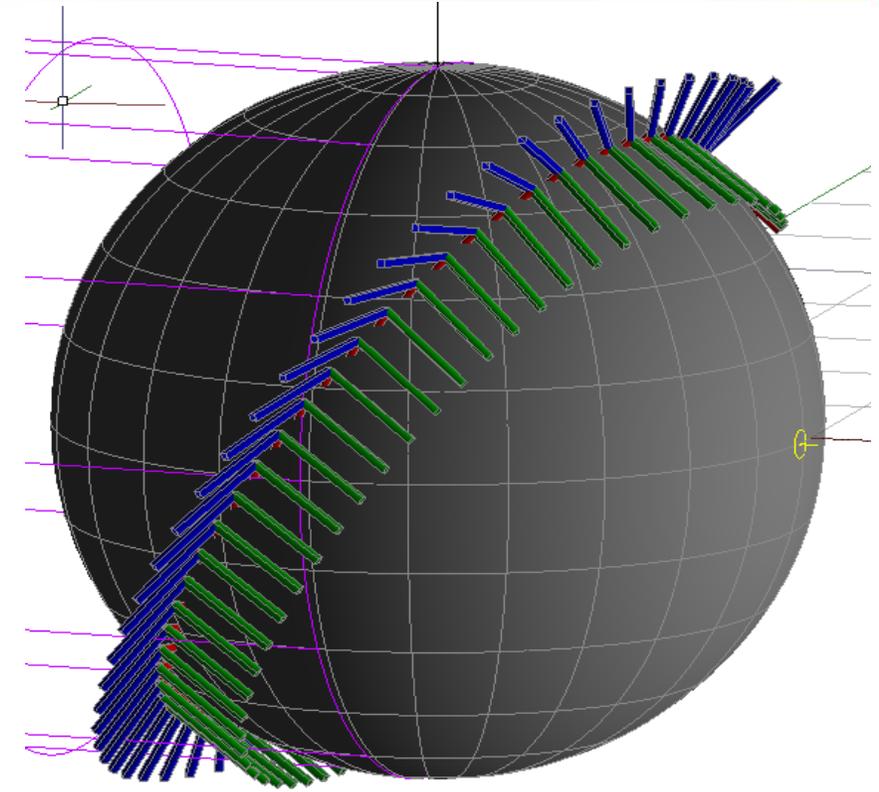
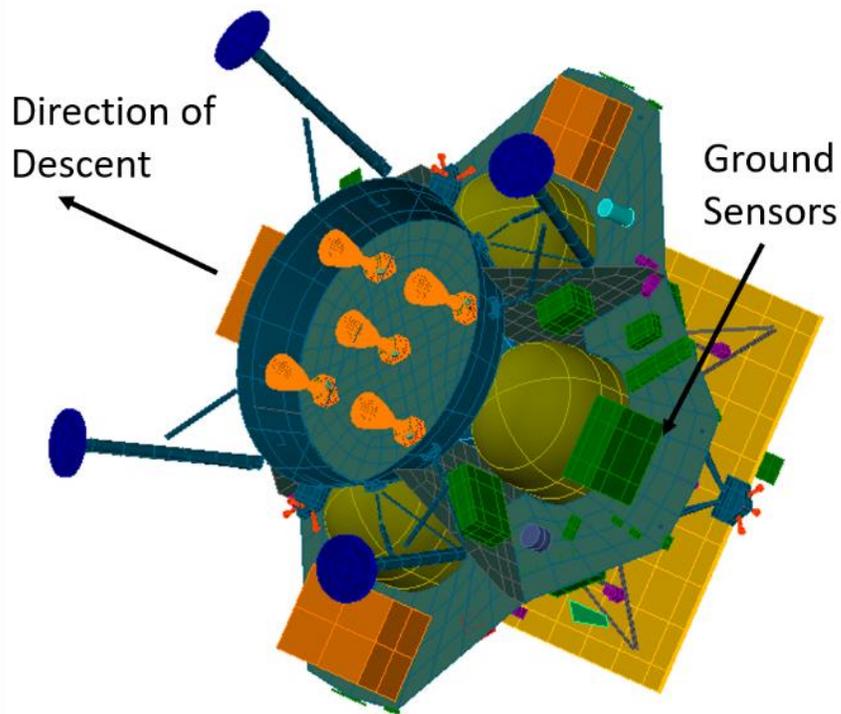
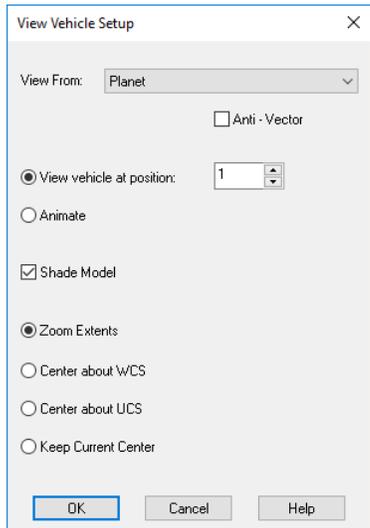
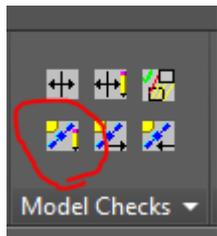




Quality Checks



- Two methods to check that the lander is properly oriented at each time step
 - Display the orbit in the heating rate case manager
 - View the lander from the planet



- Modeling the thermal environment for a lander descent correctly is essential for a successful mission. This can be difficult due to the transient nature of a descent and the addition of new thermal conditions such as component heat loads, changing view factors/radiative sink temperatures, and thruster/plume heat loads.
- The method shown above is one way to obtain the desired results but is very versatile and easy to use if more detailed rotations are required.

- Questions?
- Comments?
- Other ways of achieving desired effects?