



## Thermal Correlation of Reduced Models Using an Adjoint-Based Solver

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Thermal & Fluids Analysis Workshop  
TFAWS 2024  
August 26-30, 2024  
NASA Glenn Research Center  
Cleveland, OH

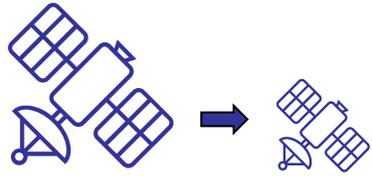


# Agenda



- Introduction
- Overview of detailed and reduced models
- Thermal correlation of the reduced model
- Conclusion

## Less expensive satellites in shorter periods of time



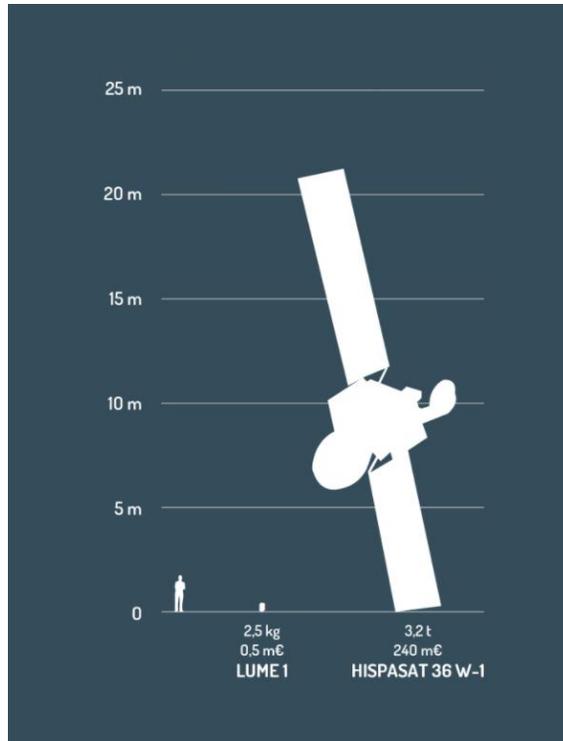
Smaller



Faster

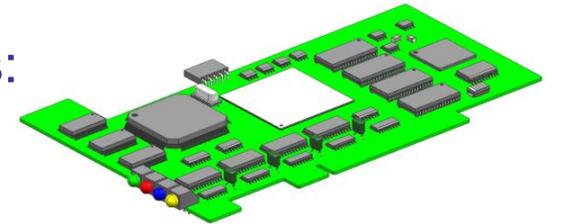


Cheaper

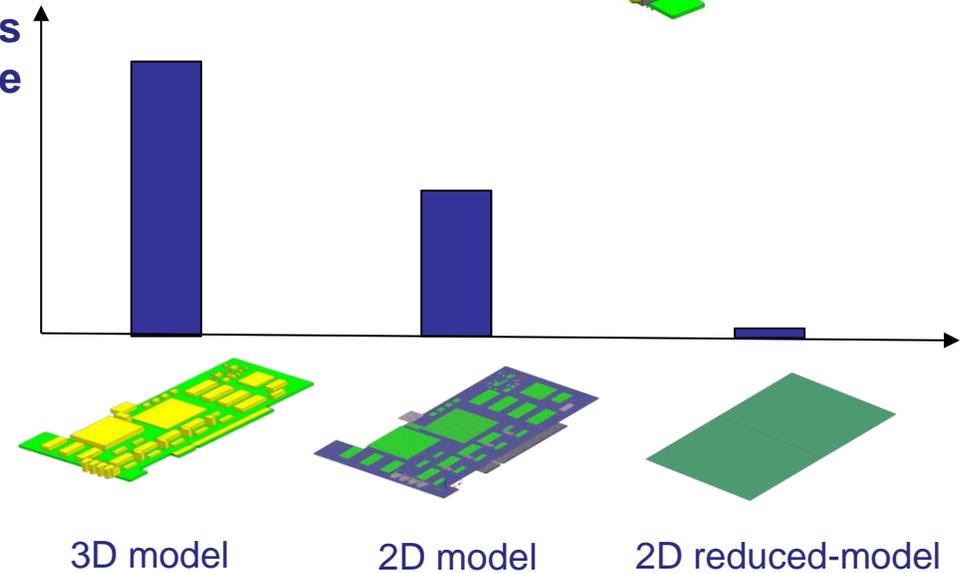


## Reduced-models helpful to shorten analysis time

- PCB with components:



Analysis time

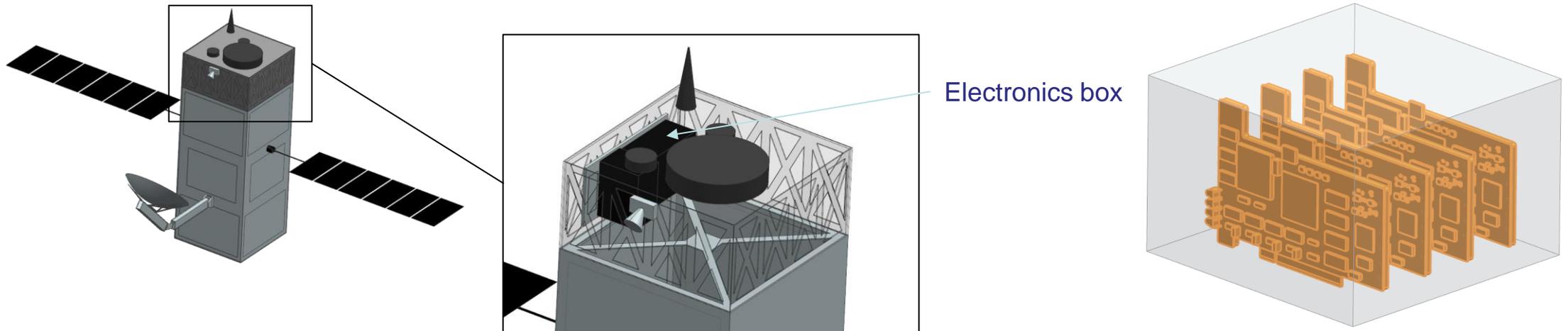


# Introduction: Thermal models of electronics boxes

- **Challenges:**

- Fidelity level of PCB and components thermal models affect the accuracy of temperature predictions for spacecraft electronics boxes
- Development of reduced-models of electronics boxes require extensive correlation analyses with detailed models

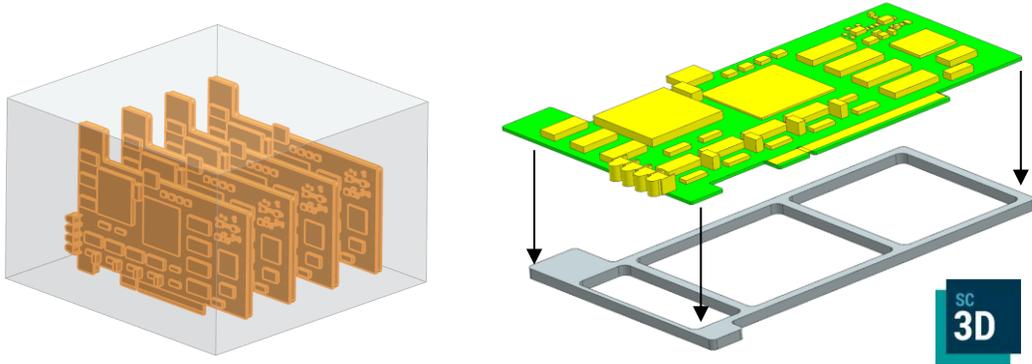
- **In this presentation:** Development of an accurate reduced-model of an electronics box using an adjoint-based thermal correlation solver



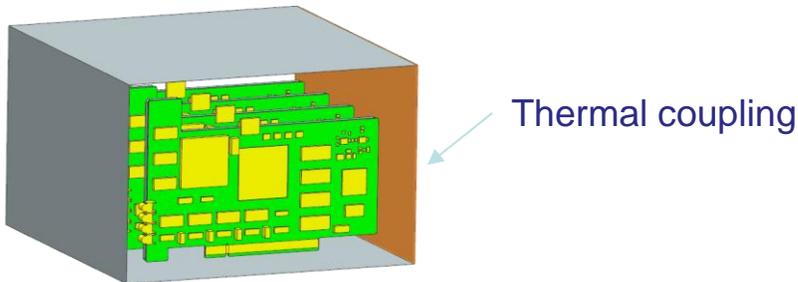


# OVERVIEW OF DETAILED AND REDUCED MODELS OF THE ELECTRONICS BOX

- 3D thermal model contains:
  - Four PCBs and components (2 main + 2 backup) mounted on a frame

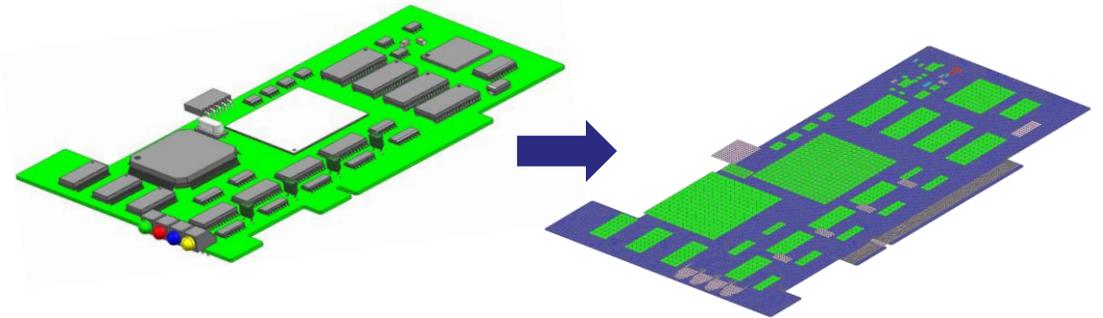


- The frames are thermally connected to one side of an enclosure

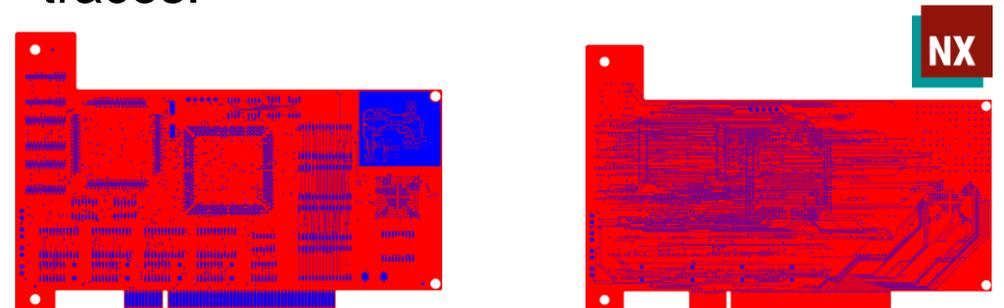


- 220,000 elements (3D & 2D) in total

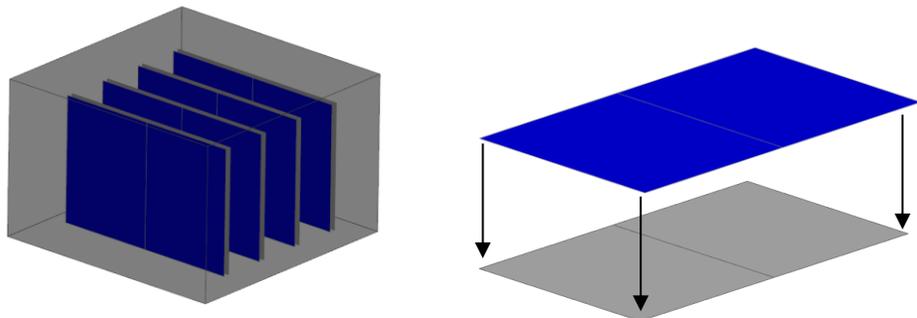
- Each PCB involves:
  - 121 components with associated dissipation models and 2D meshes



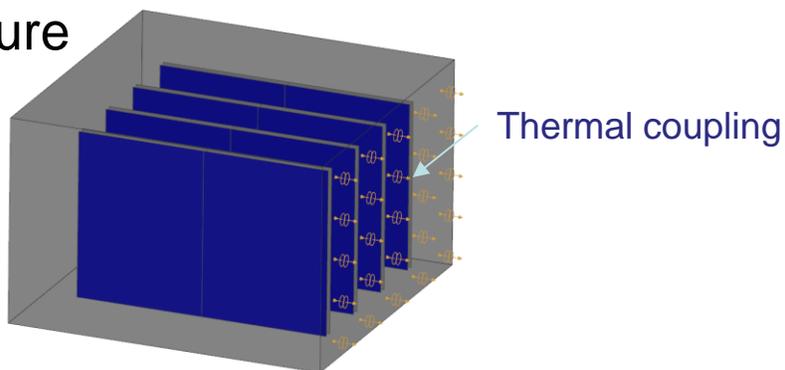
- 2D fields material properties for each PCB layer to model vias and copper traces.



- Electronics box contains:
  - 2 x 2D null shell elements for each PCB and frame

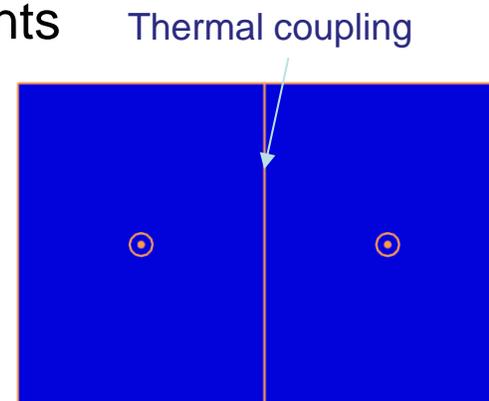


- The edges of the frame elements are thermally connected to one side of the enclosure

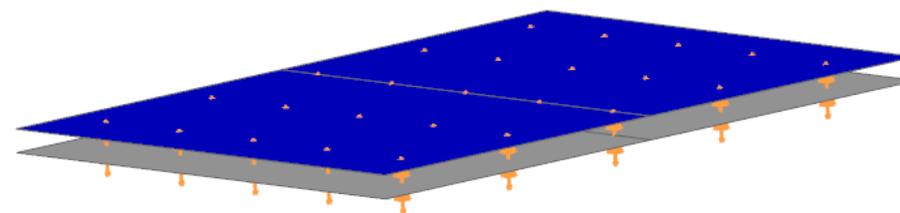


- 500 elements (2D) in total

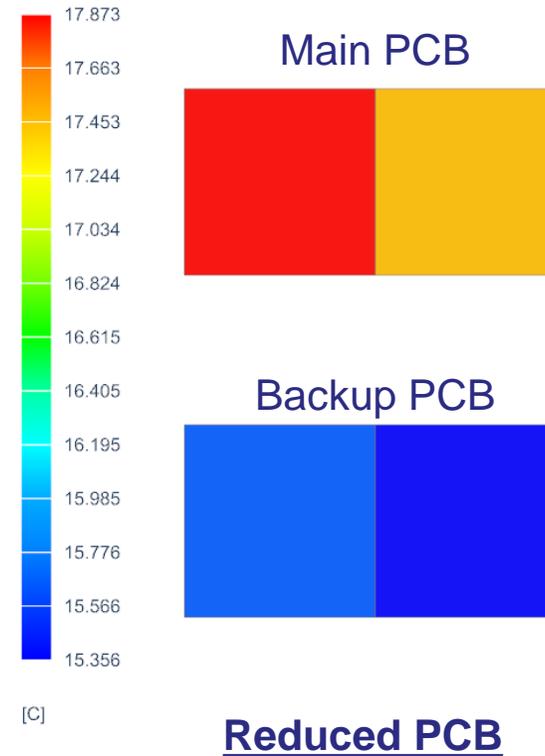
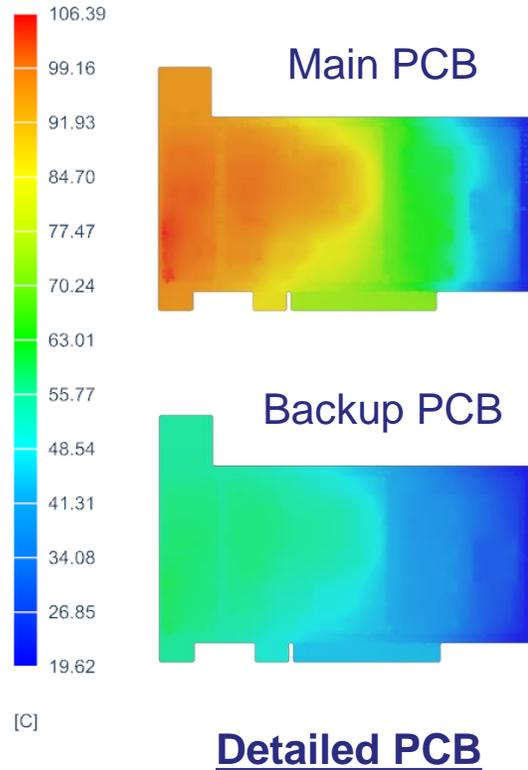
- Each PCB & frame involves:
  - One contact between the 2D null shell elements



- One thermal coupling for each PCB-Frame pair



- Temperature contours for cold case scenario (Enclosure wall at 15 °C)



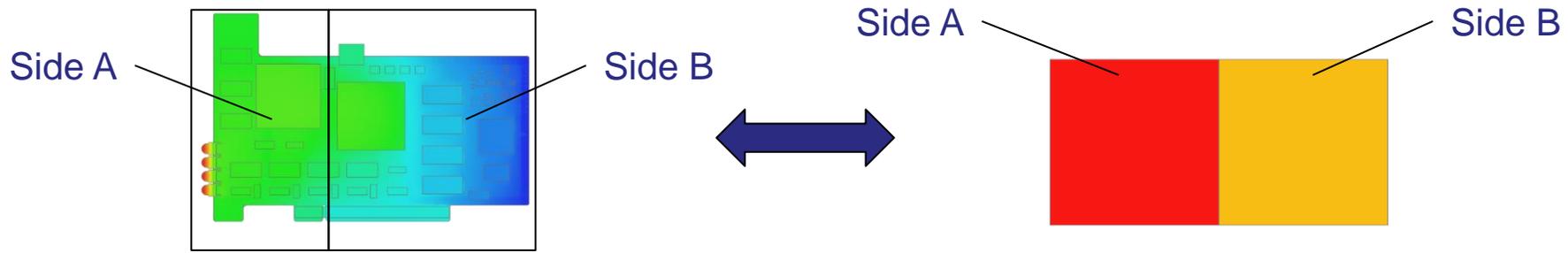
**Simplification/Reduction requires updating all thermal contacts to match detailed model results**



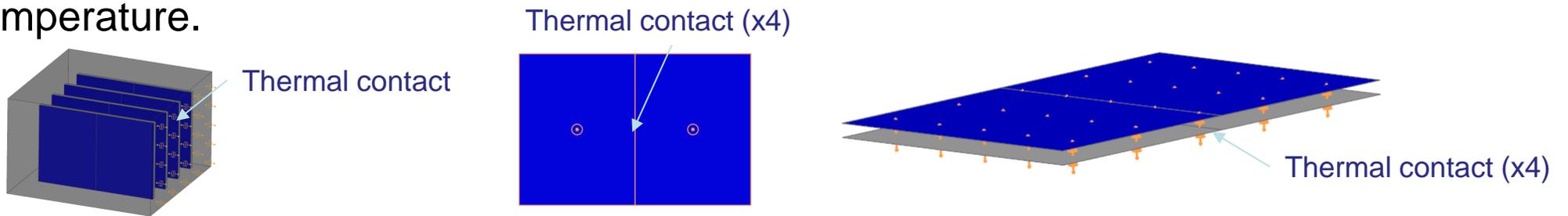
# THERMAL CORRELATION

- Objectives:

- The temperature of the reduced PCB elements must match the respective averaged temperature on each side of the PCBs

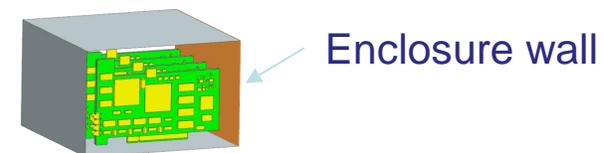


- Finding the right thermal contact values for matching the detailed PCB model averaged-temperature.



- Thermal contacts of the reduced model must be valid for hot and cold case scenarios

- Cold case scenario: Enclosure wall @ 15 °C
- Hot case scenario: Enclosure wall @ 55 °C



- TMG Correlation is an add-on to Simcenter 3D Space Systems Thermal.

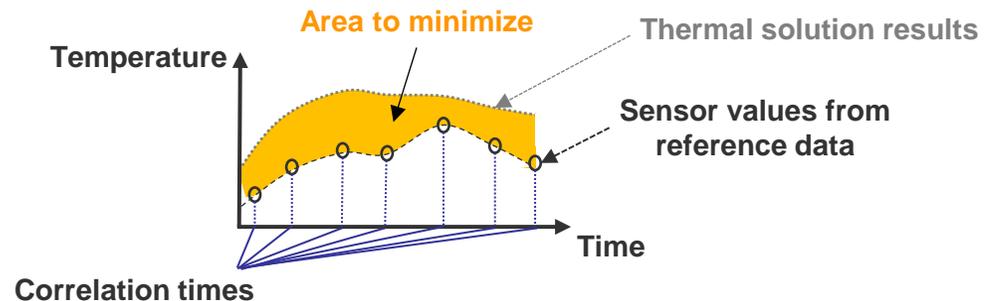


- It combines the adjoint-method and gradient-based optimization algorithms to correlate models by minimizing the following objective function:

$$F = \sqrt{\frac{1}{N_{times} * \sum(W_{target})} \times \sum_{times} \left( \sum_{target} W_{target} (T - T_{target})^2 \right)}$$

$N_{times}$ : number of correlation times  
 $\sum(W_{target})$ : Total weight factors defined on the targets  
 $W_{target}$ : weight factor on the targets (sensors)

- For transient problems, the correlation times define the times at which the model calibration is performed



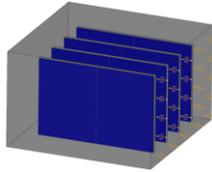
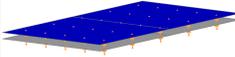
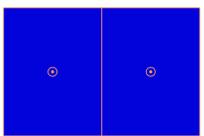
# TMG Correlation: An adjoint-based solver for correlation

- The adjoint method [1,2] is used to compute the gradients  $\vec{G}$  that are passed to an optimization algorithm, which updates the design variables  $\vec{h}$  at each design cycle  $i$ .
  - Adjoint equation:  $\left(\frac{\partial R}{\partial \vec{h}}\right)^T \vec{\psi} = -\frac{\partial F}{\partial T}$
  - Gradient:  $\vec{G} = \frac{\partial F}{\partial \vec{h}} + \psi^T \frac{\partial R}{\partial \vec{h}}$
  - Update of the design variables by the optimization algorithm:  $\vec{h}^{i+1} = \vec{h}^i - \alpha \vec{G}$
- Why use the adjoint method?
  - Classic gradient computation based on finite differences requires solving  $N + 1$  times the system for  $N$  design variables.
  - Using the adjoint method, we only solve 2 systems: the original system (energy equation) + the adjoint system

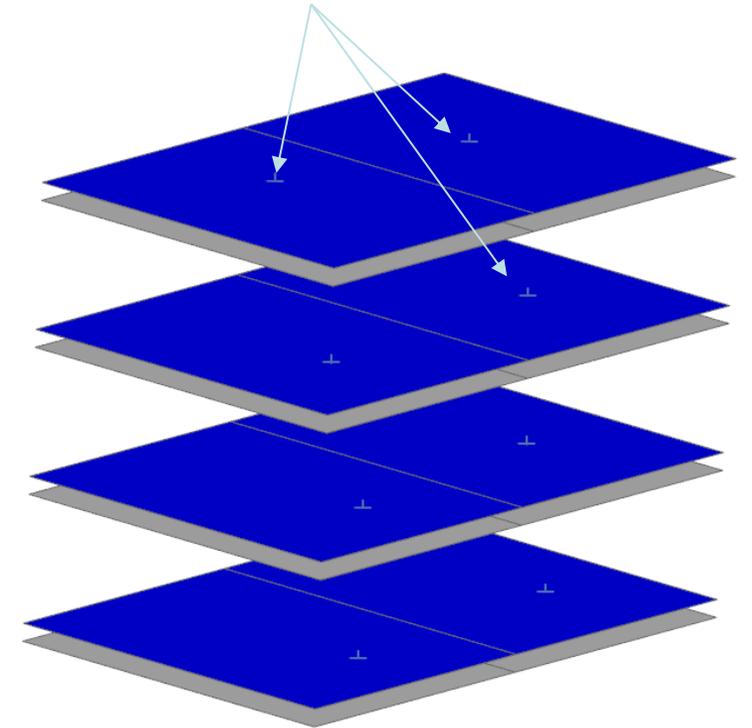
[1] Michaleris, P., Tortorelli, D. A., & Vidal, C. A. (1994). Tangent operators and design sensitivity formulations for transient non-linear coupled problems with applications to elastoplasticity. *International Journal for Numerical Methods in Engineering*, 37(14), 2471-2499.

[2] Kast, S. M. (2017). An introduction to adjoints and output error estimation in computational fluid dynamics. *arXiv preprint arXiv:1712.00693*.

- Convergence Criterion: 0.01 °C
- Optimization algorithm: Sequential Least Square Programming

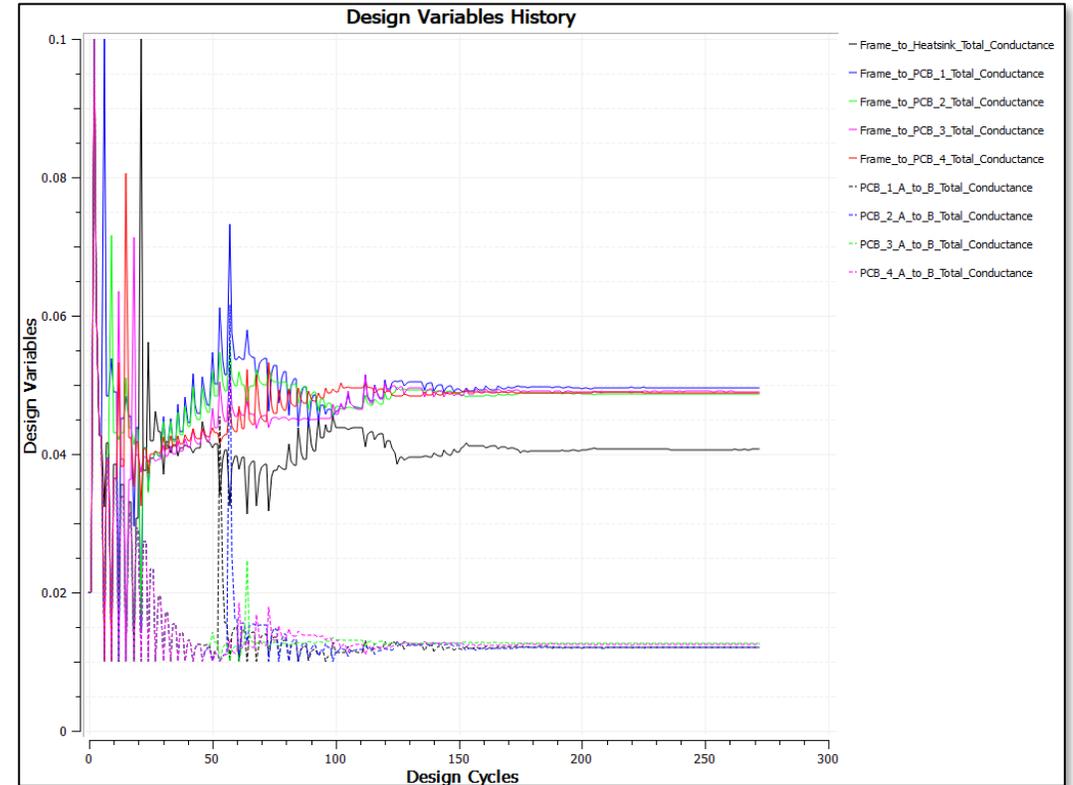
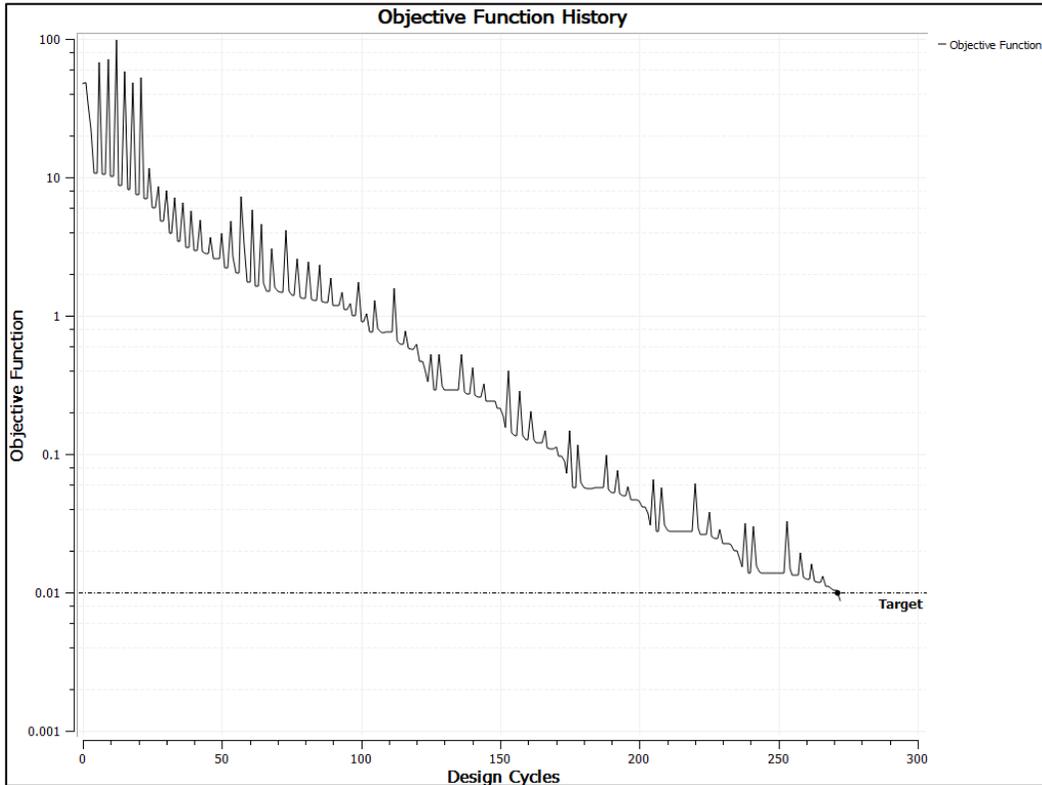
Design Variable	Initial value	Min - Max	Location
Frame_to_Heatsink_Total_Conductance	30 W/C	0.3 – 3000	
Frame_to_PCB_1_Total_Conductance	5 W/C	0.05 – 500	
Frame_to_PCB_2_Total_Conductance	5 W/C	0.05 – 500	
Frame_to_PCB_3_Total_Conductance	5 W/C	0.05 – 500	
Frame_to_PCB_4_Total_Conductance	5 W/C	0.05 – 500	
PCB_1_A_to_B_Total_Conductance	5 W/C	0.05 – 500	
PCB_2_A_to_B_Total_Conductance	5 W/C	0.05 – 500	
PCB_3_A_to_B_Total_Conductance	5 W/C	0.05 – 500	
PCB_4_A_to_B_Total_Conductance	5 W/C	0.05 – 500	

8 targets defined using points

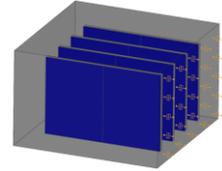
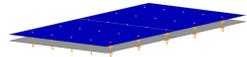
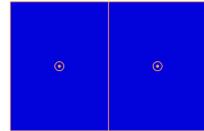


Correlation run took **11 seconds** to converge under **0.01 °C** after **272 design cycles**

Design variables reached **stable** values



- The tool reduced all conductance values to match detailed model results.
- Similar thermal contact implies similar conductance value.

Design Variable	Initial value [W/C]	Final Value [W/C]	Location
Frame_to_Heatsink_Total_Conductance	30	1.221	
Frame_to_PCB_1_Total_Conductance	5	0.247	
Frame_to_PCB_2_Total_Conductance	5	0.243	
Frame_to_PCB_3_Total_Conductance	5	0.245	
Frame_to_PCB_4_Total_Conductance	5	0.244	
PCB_1_A_to_B_Total_Conductance	5	0.060	
PCB_2_A_to_B_Total_Conductance	5	0.060	
PCB_3_A_to_B_Total_Conductance	5	0.063	
PCB_4_A_to_B_Total_Conductance	5	0.062	

- Reduced model results match detailed model averaged temperatures.

Target	Detailed model		Reduced model		Absolute Errors [C]
	Averaged Temperature [C]	Contours for PCB 1 & 3	Temperature [C]	Contours for PCB 1 & 3	
PCB_1_A	64.61		64.63		0.015
PCB_1_B	97.45		97.45		-0.003
PCB_2_A	65.26		65.26		0.001
PCB_2_B	97.53		97.53		-0.003
PCB_3_A	39.77		39.78		0.008
PCB_3_B	56.40		56.40		0.0007
PCB_4_A	39.83		39.83		-0.003
PCB_4_B	56.43		56.45		0.017

- Reduced model slightly overpredicts temperatures for the hot case scenario

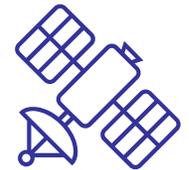
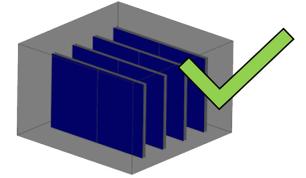
Target	Detailed model		Reduced model		Absolute Errors [C]
	Averaged Temperature [C]	Contours for PCB 1 & 3	Temperature [C]	Contours for PCB 1 & 3	
PCB_1_A	101.91		104.62		2.712
PCB_1_B	136.03		137.45		1.418
PCB_2_A	102.07		105.26		3.188
PCB_2_B	136.27		137.52		1.247
PCB_3_A	78.49		79.78		1.289
PCB_3_B	95.79		96.40		0.614
PCB_4_A	78.53		79.83		1.296
PCB_4_B	95.83		96.45		0.621



# CONCLUSION

# Conclusion and Perspectives

- Using **TMG Correlation**, an adjoint-based solver, we successfully correlated the reduced-model of an electronics box
  - Reduced model **predictions are accurate** even on a different operating case
  - The entire **correlation procedure took less than one hour** in total
- The **same approach** can be used for correlating **larger systems** or spacecraft for **steady-state and transient** operation cases.
- The procedure can be enhanced by **automating the generation of the reduced model to save engineering time**



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