



Passively Deployed Radiators for Transfer and Rejection of CubeSat Waste Heat

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Presented By
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Cleveland, OH

Biography

- PhD from Brigham Young University in 2019
- Assistant Professor at the University of Dayton Department of Mechanical Engineering since 2019
- Published areas of interest include: **Spacecraft thermal control**, High-speed vehicle power production (coordinating with JHAPL), PV panel orientation optimization and Greenhouse production optimization.

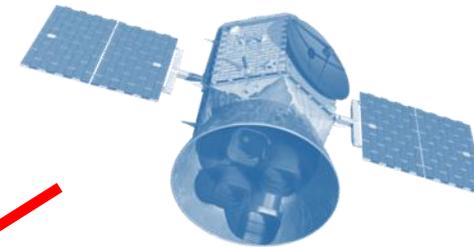


Introduction



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Introduction – Motivation



High Heating Loads:
Encourage Radiator Heat
Rejection

- Increase emissivity
- Increase surface area

Spacecraft experience temperature variation while orbiting the Earth

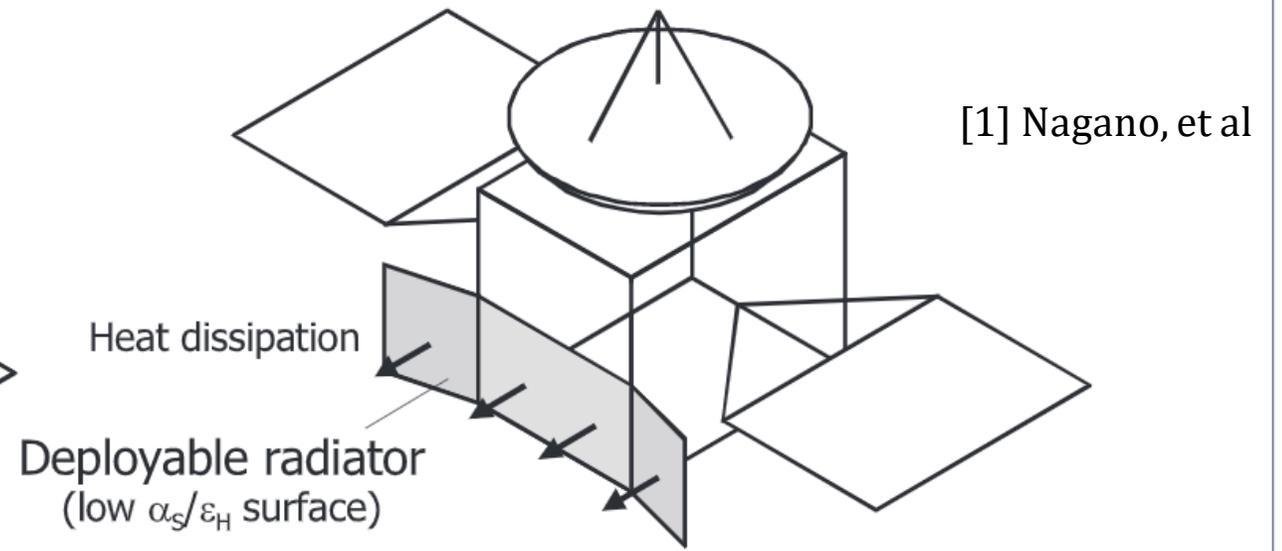
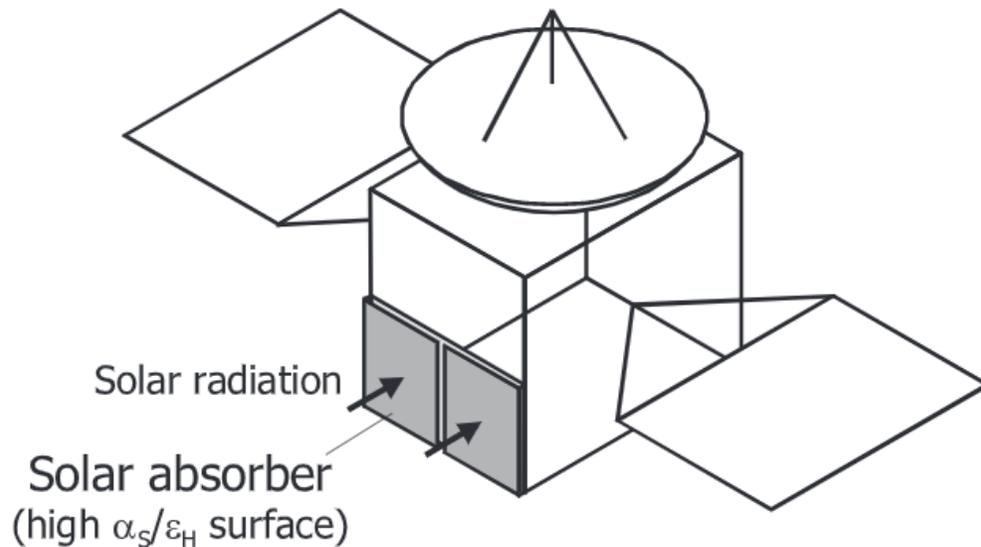
CubeSats, with low thermal mass and no thermal control, experience the largest temperature swings

Low Heating Loads:
Discourage Radiator Heat
Rejection

- Decrease emissivity
- Decrease surface area

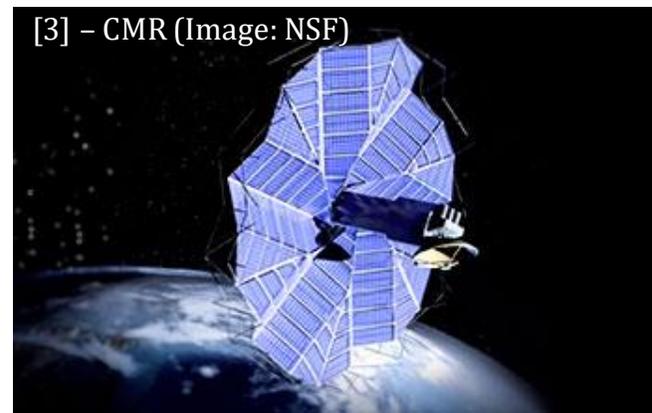
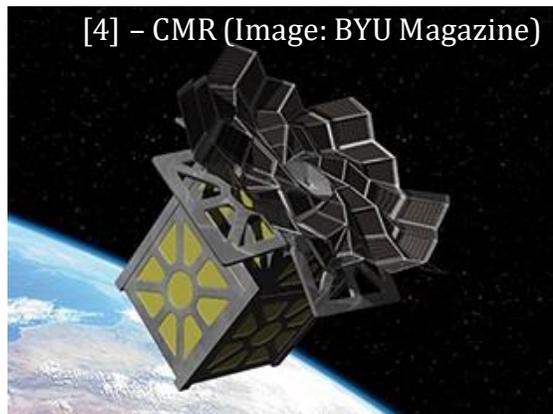
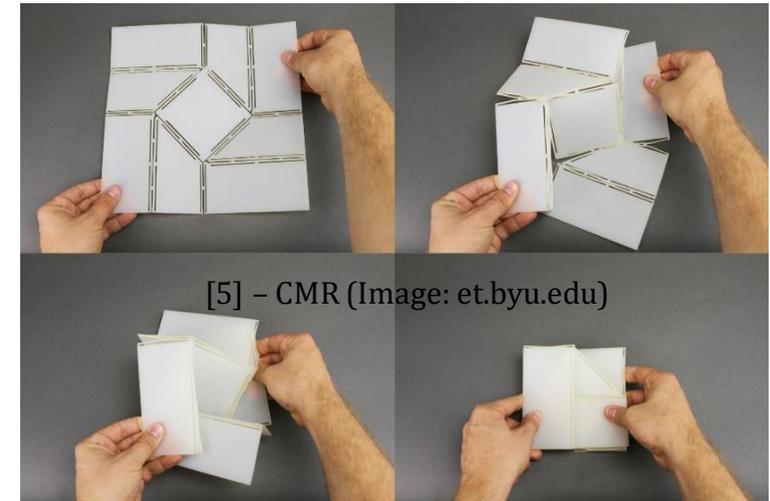
Introduction – Innovation

- Increase radiative surface area and effective emissivity
- 200% more radiative heat loss than body mounted radiators
- NASA Technology Roadmap target turndown ratio: 6
 - Turndown ratio: maximum / minimum radiative heat loss



Introduction – Innovation

- Origami controls both emitting area and surface properties
- Large variations in emitting area
- Passive actuation possible



Introduction – Objectives

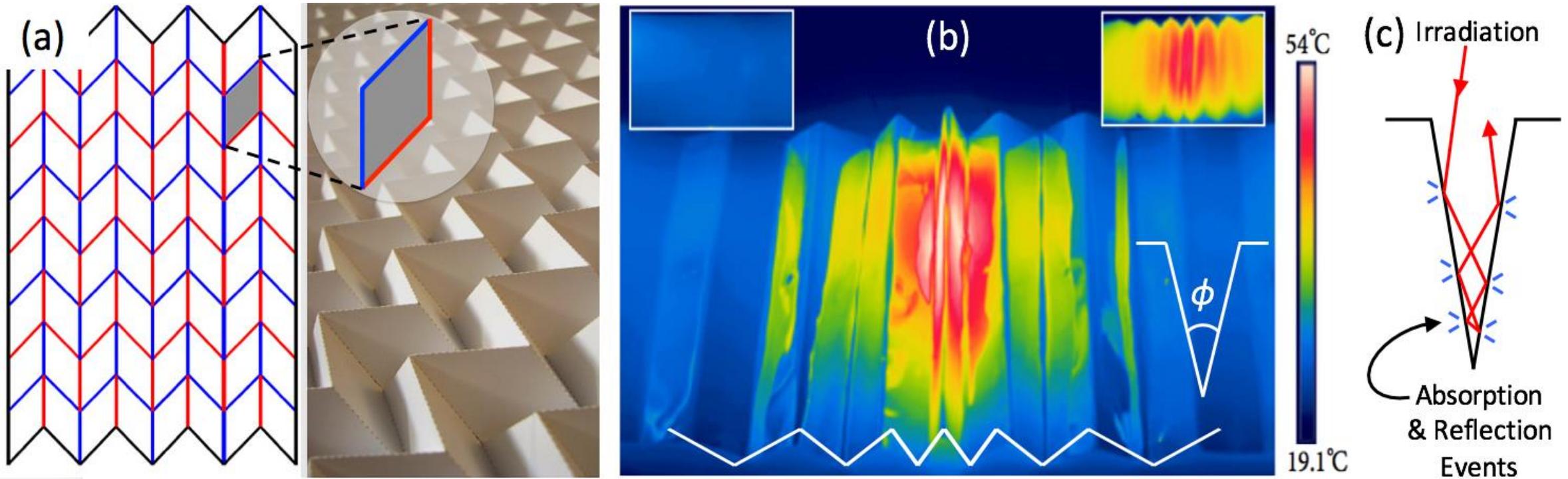
- **Concept** - Explore the fundamental behavior of heat transfer in geometrically-dynamic radiator systems (TRL 1 – 2)
- **Develop** - Develop technologies based on geometric manipulation for control of radiative heat transfer (TRL 3 – 5)
- **Demonstrate** - Implement and demonstrate dynamic technologies implemented into spacecraft systems (TRL \geq 6)



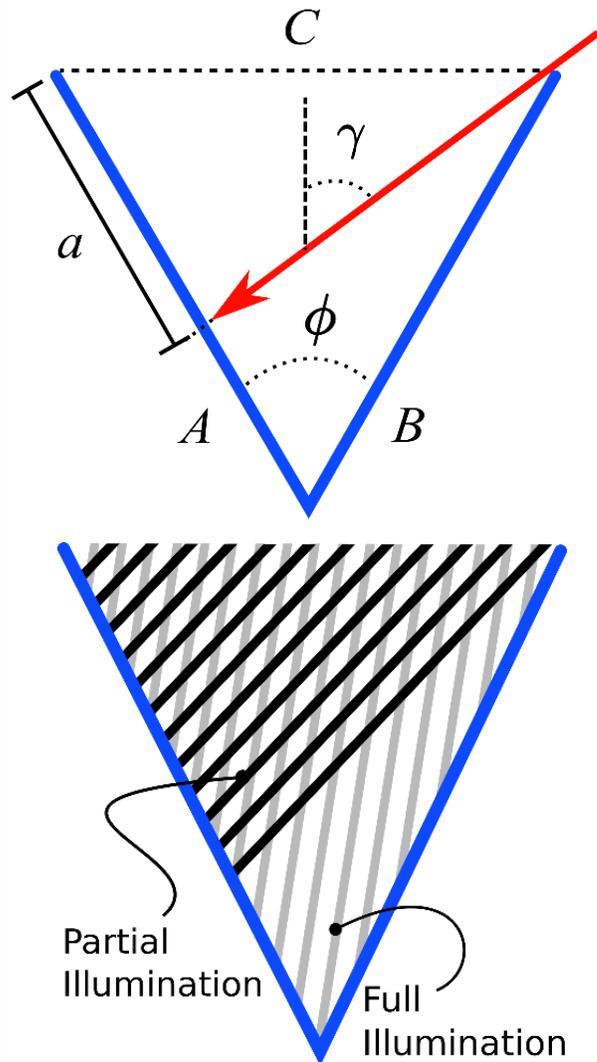
Concept



Concept – Cavity Effect

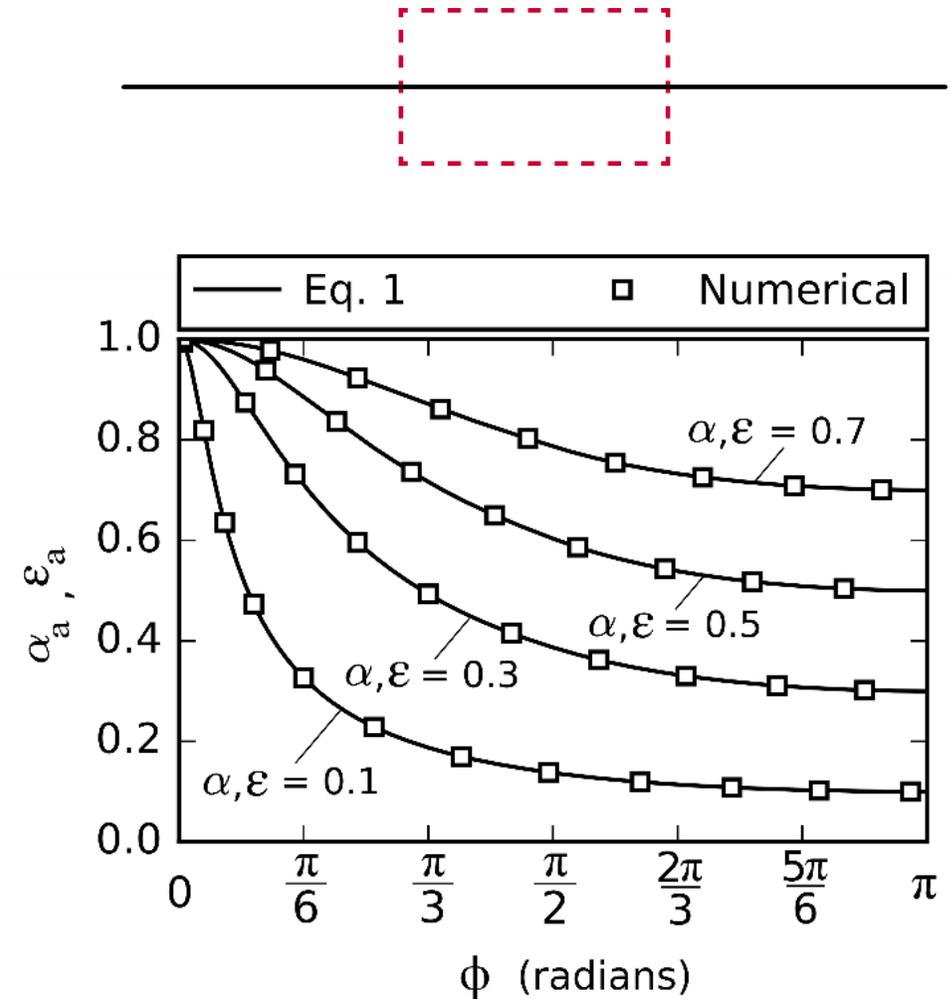


Concept – Cavity Effect



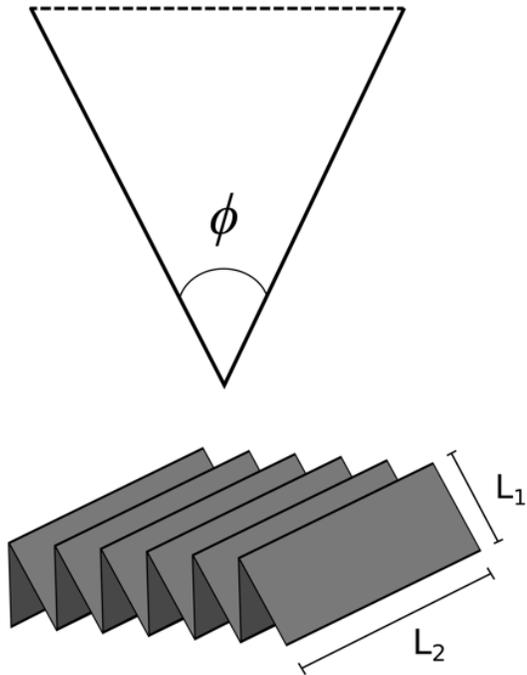
Conditions

- Diffuse/specular surfaces
- Geometry
- Full/partial illumination
- Normal/off-normal irradiation

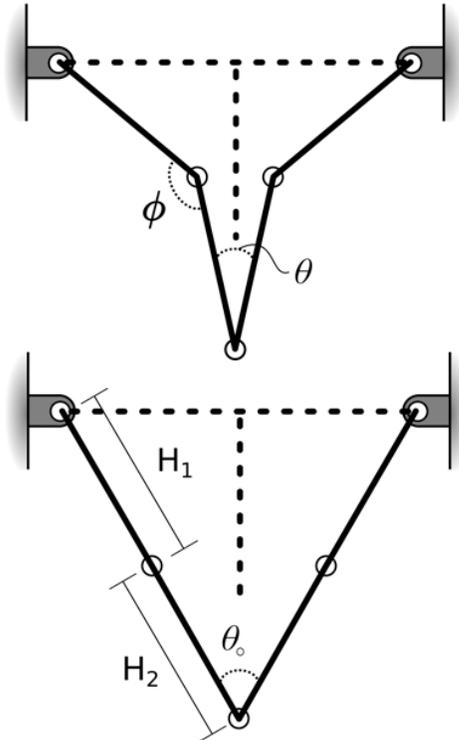


Concept – Cavity Effect

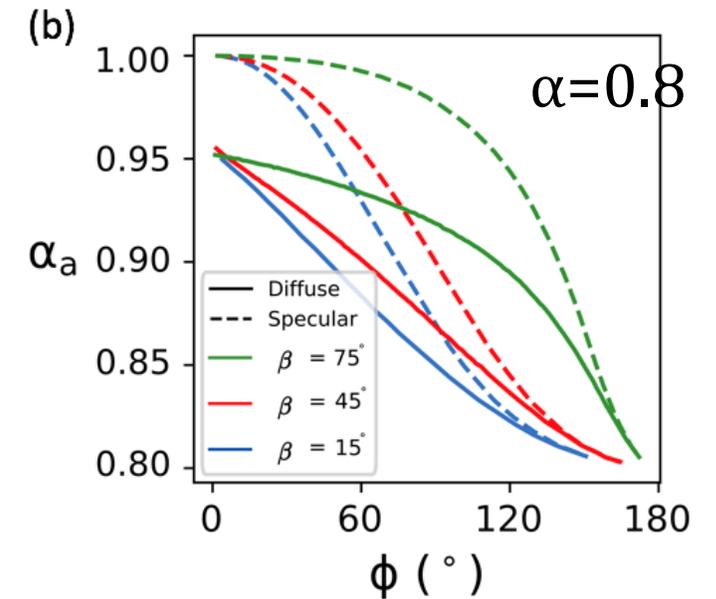
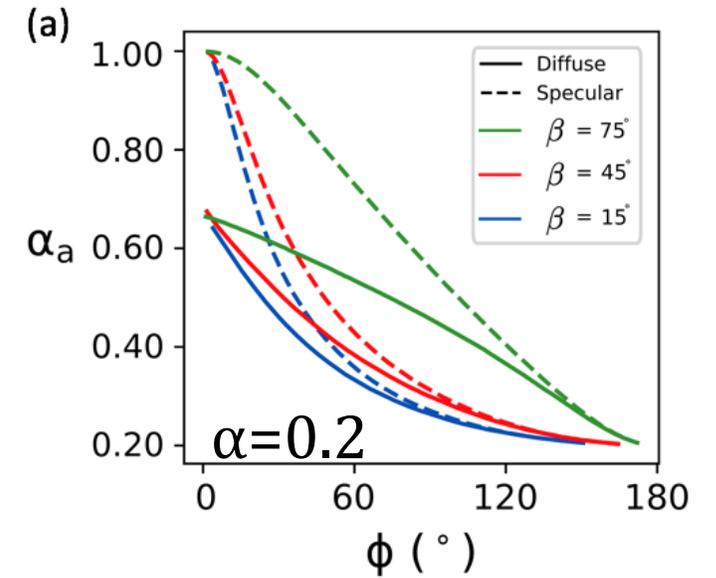
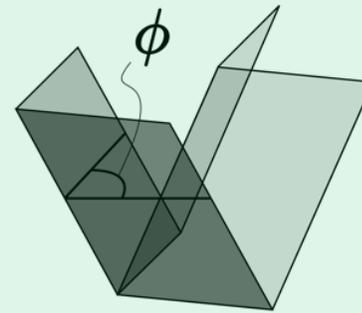
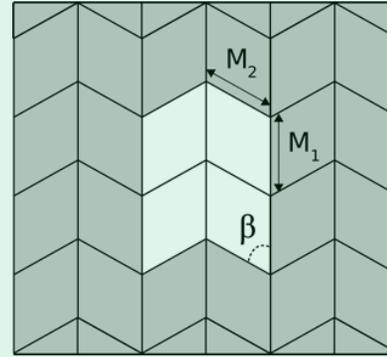
(a) Finite V-groove



(b) Hinged V-groove



(c) Miura-ori



Concept - Takeaways

- Radiative surface properties can be controlled through actuation
- Surface property variations behave opposite the behavior of the surface area, reducing overall heat transfer effectiveness
- Various tessellations generally feature similar behavior
- “Conceal and Reveal” systems provide a means of increasing the emissivity and the area at the same time

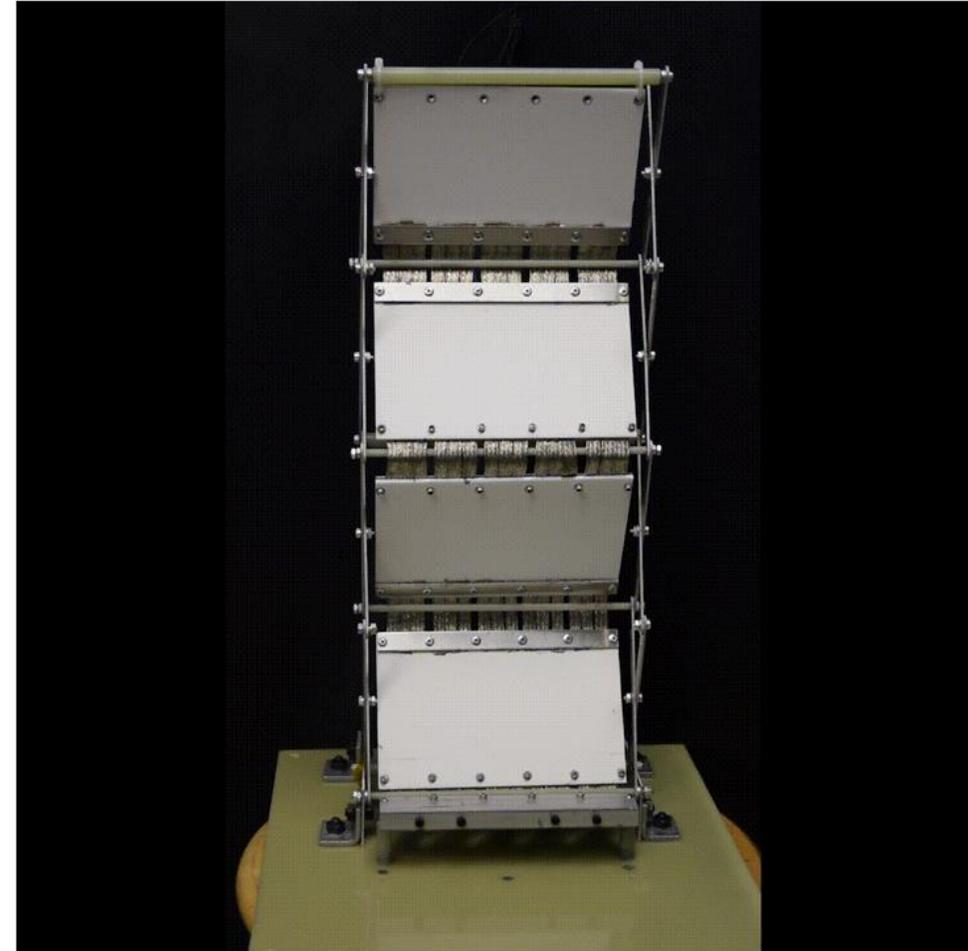


Develop



Initial Development – Accordion Radiator

- An active dynamic radiator uses motorized methods to actuate and retract radiator panels.
- Theoretical Turn Down Ratio: 8
- Issues identified from beginning
 - Panels in series results in significant conduction losses
 - Active actuation is not ideal

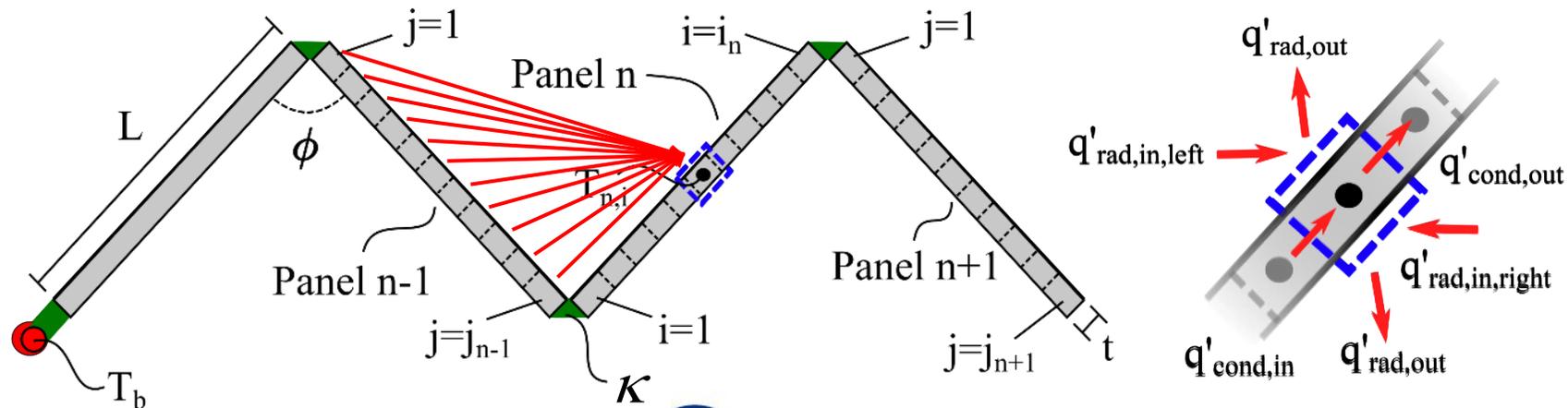


Initial Development – Accordion Radiator Model

$$q'_{cond,in} - q'_{cond,out} + q'_{rad,in,left} + q'_{rad,in,right} - q'_{rad,out} = 0$$

$$-kt \frac{T_{n,i} - T_{n,i-1}}{\Delta x} + kt \frac{T_{n,i+1} - T_{n,i}}{\Delta x} + \alpha \sum_{j=1}^{j=j_{n-1}} J_{n-1,j} F_{j-i} \Delta x + \alpha \sum_{j=1}^{j=j_{n+1}} J_{n+1,j} F_{j-i} \Delta x - 2\Delta \epsilon x \sigma T_{n,i}^4 = 0$$

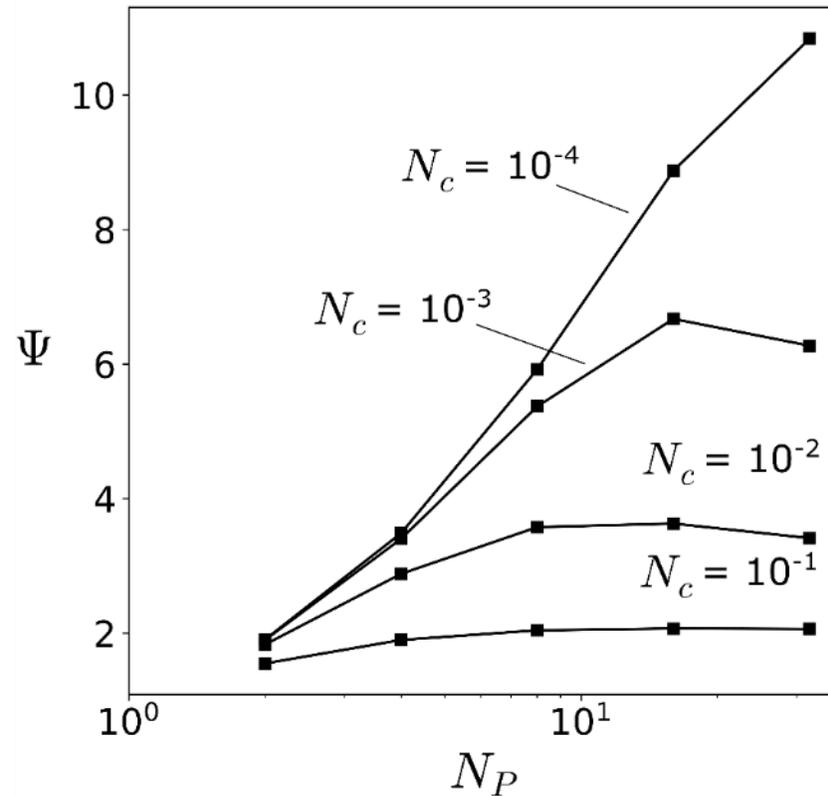
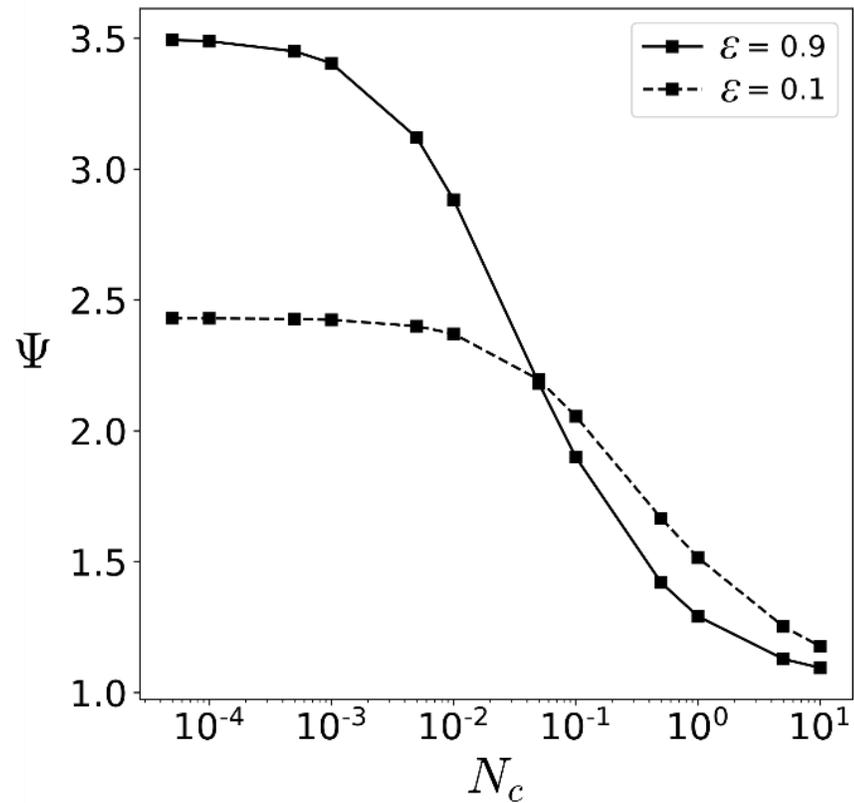
$$J_{n,i} = \epsilon \sigma T_{n,i}^4 + (1 - \epsilon) \sum_{j=1}^{j=j_{n+1}} J_{n+1,j} F_{j-i}$$



Initial Development – Model Results

$$\Psi = \frac{q_{\max}}{q_{\min}} \quad N_c = \frac{R_{\text{conduction}}}{R_{\text{radiation}}}$$

$\uparrow \Psi$ Improved Heat Transfer Control
 $\downarrow \Psi$ Poor Heat Transfer Control



Initial Development – Model Results

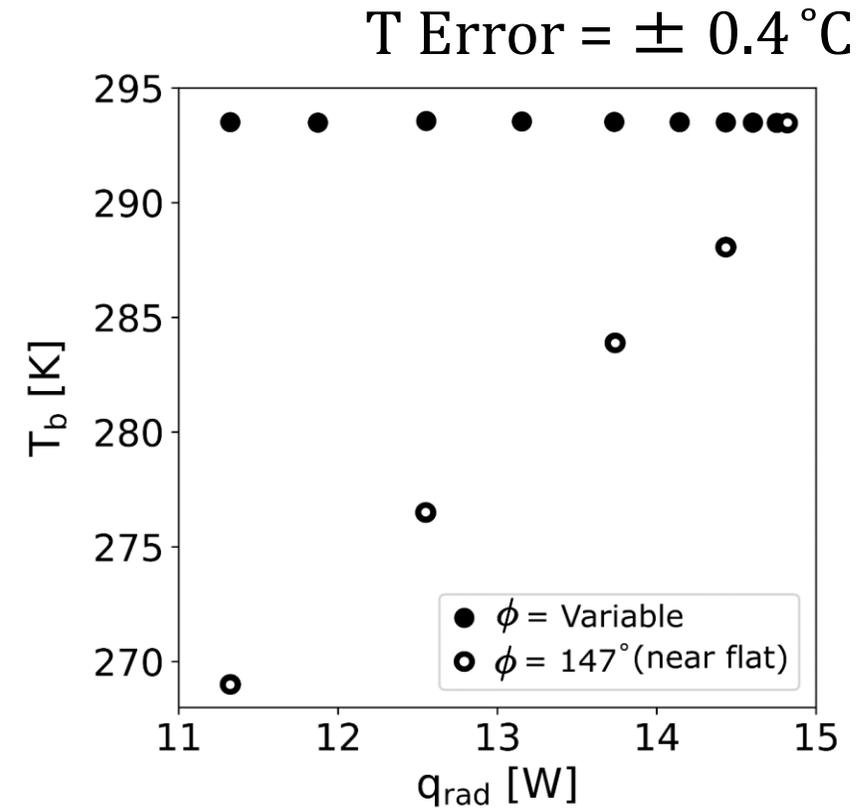
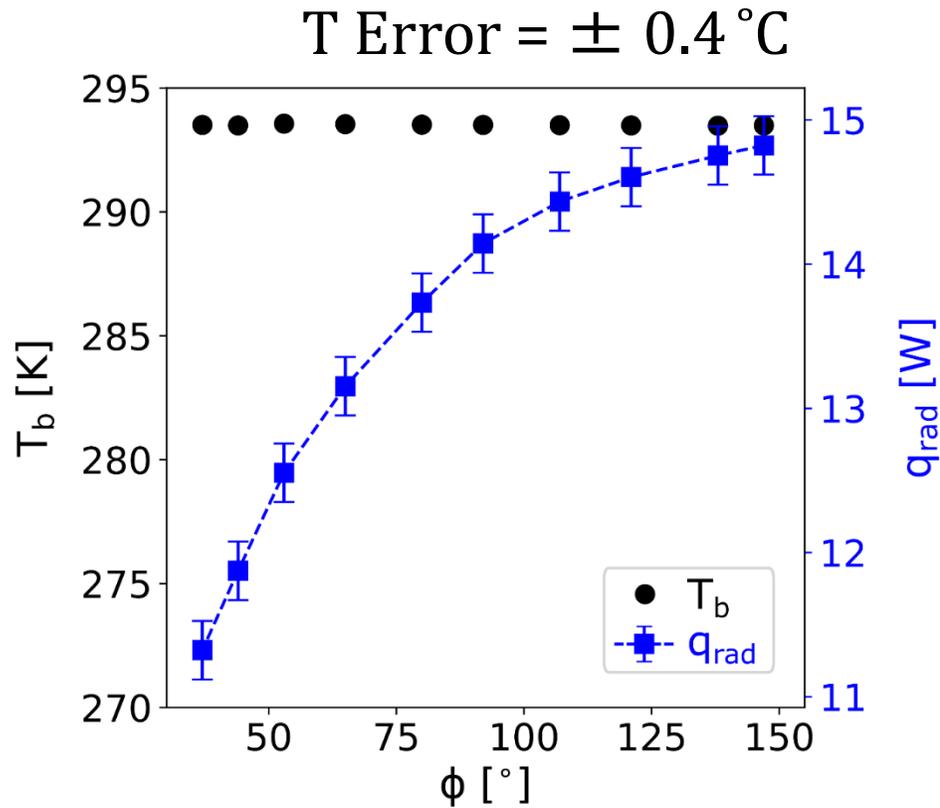
κ [W K ⁻¹]		0.6			6			60			∞		
Panels		2	4	8	2	4	8	2	4	8	2	4	8
k_p [W m ⁻¹ K ⁻¹]	237	1.81	2.27	2.46	1.95	2.82	3.34	1.97	2.93	3.55	1.97	2.95	3.58
	401	1.82	2.32	2.55	1.96	3.02	3.77	1.98	3.19	4.14	1.99	3.21	4.19
	1950	1.82	2.39	2.67	1.97	3.38	4.82	1.99	3.70	6.01	1.99	3.74	6.22
	∞	1.82	2.41	2.71	1.97	3.52	5.37	1.99	3.92	7.46	2.00	3.98	7.92

Highest Turn-Down Ratio (Achievable): 6.01

Highest Turn-Down Ratio (Theoretical): 7.92



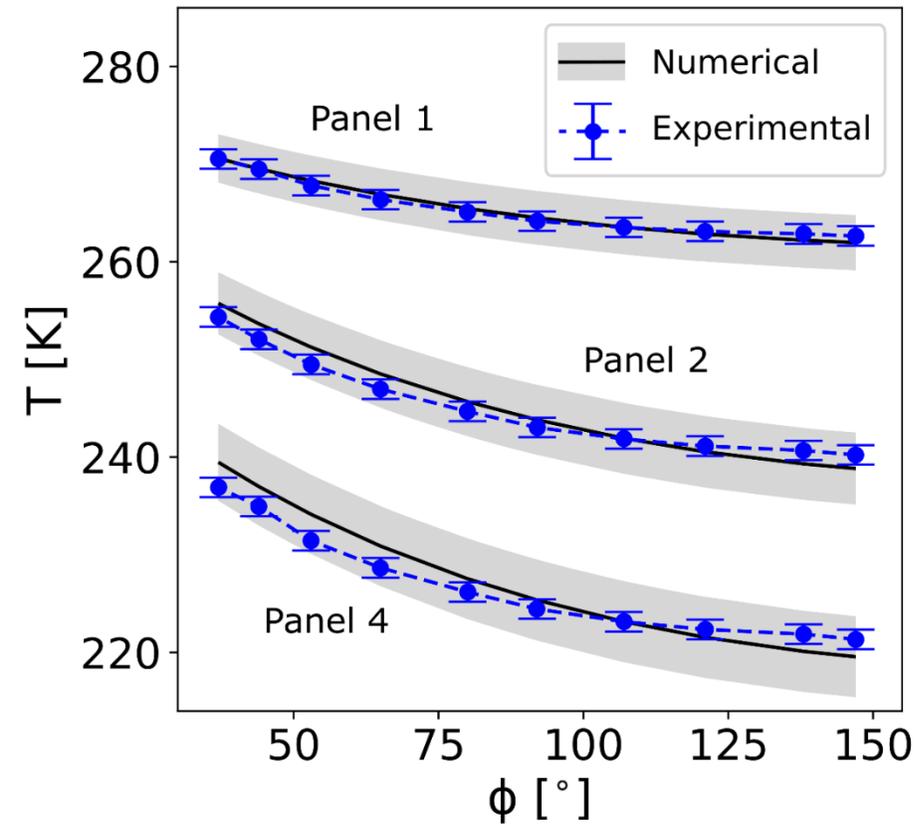
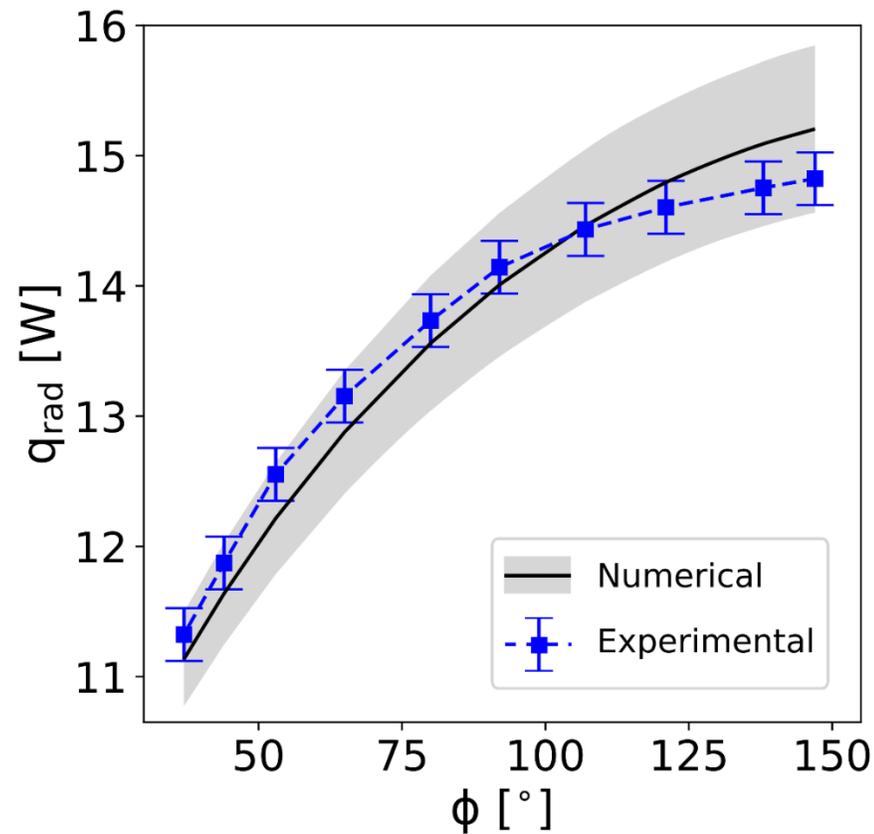
Initial Development – Model Results



$$\Psi = 1.31 \quad 35^\circ < \phi < 160^\circ$$



Initial Development – Model Results



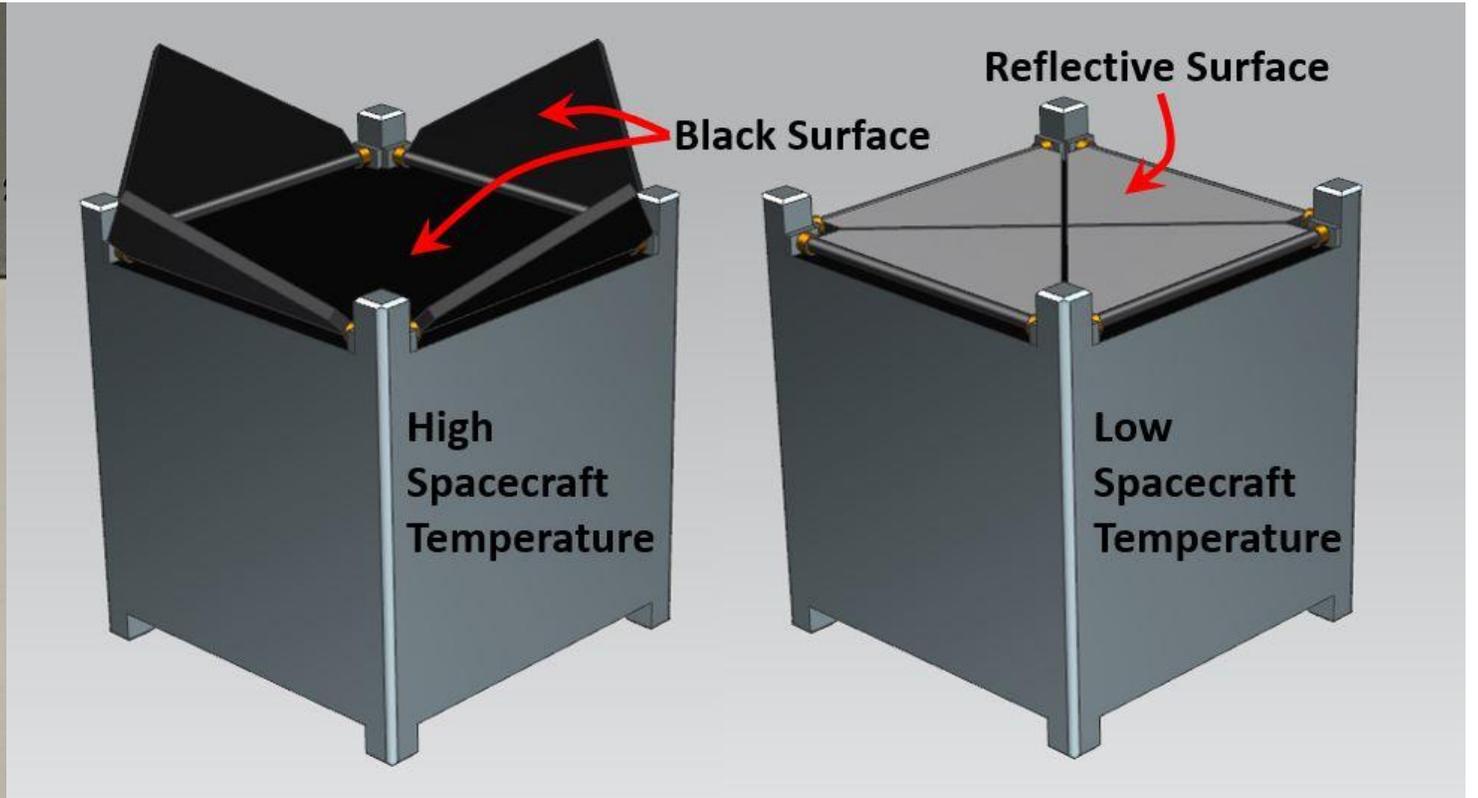
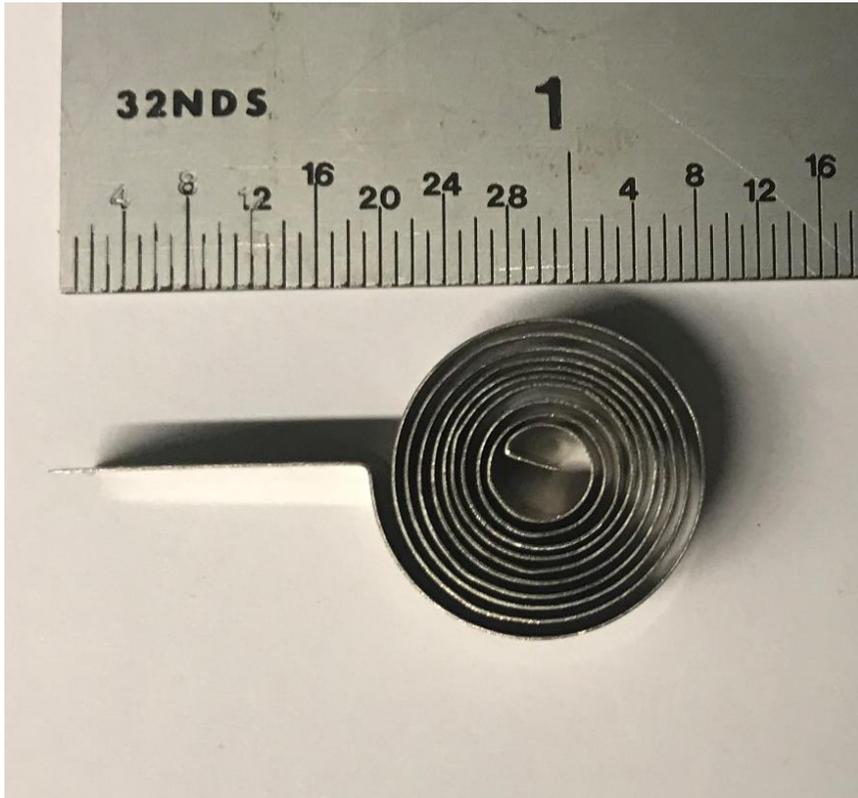
Numerical Uncertainty = Uncertainty in hinge conductance, panel emissivity
panel dimensions, and radiator angle

Initial Development - Takeaways

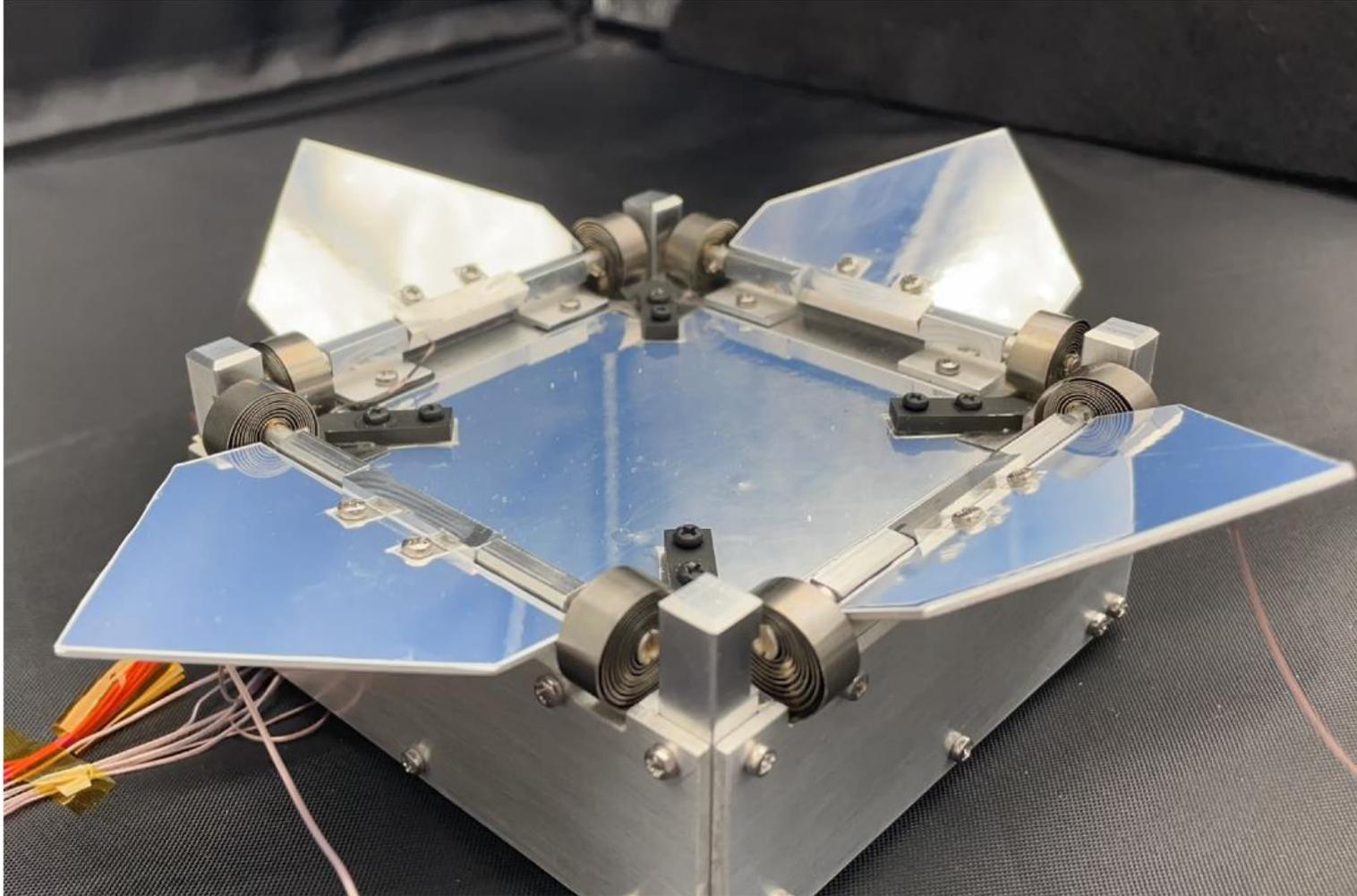
- Panels in series are not effective
- Passive actuation is preferred by the thermal control community
- Smaller form-factor spacecraft (CubeSats) require simplicity but need the most variation



CubeSat Development – Ideation



CubeSat Development - Prototype

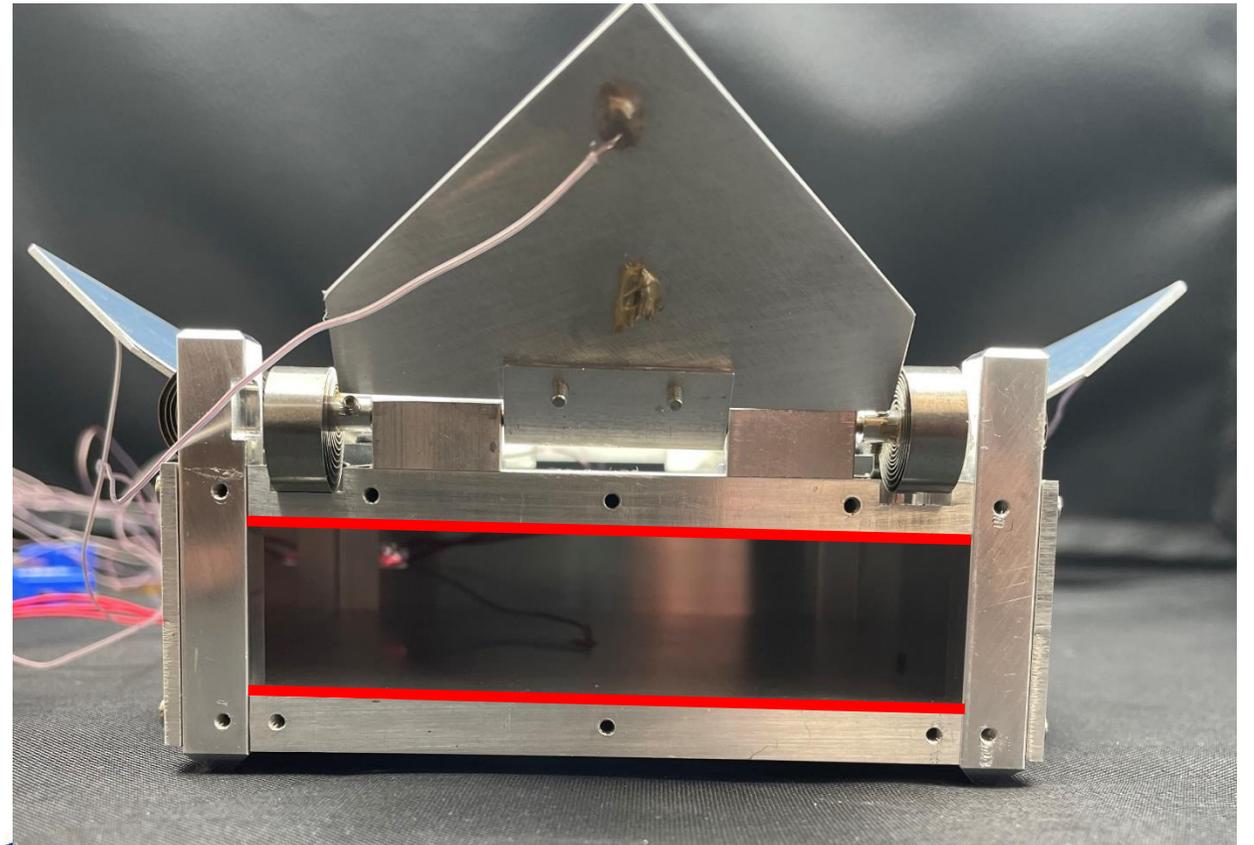
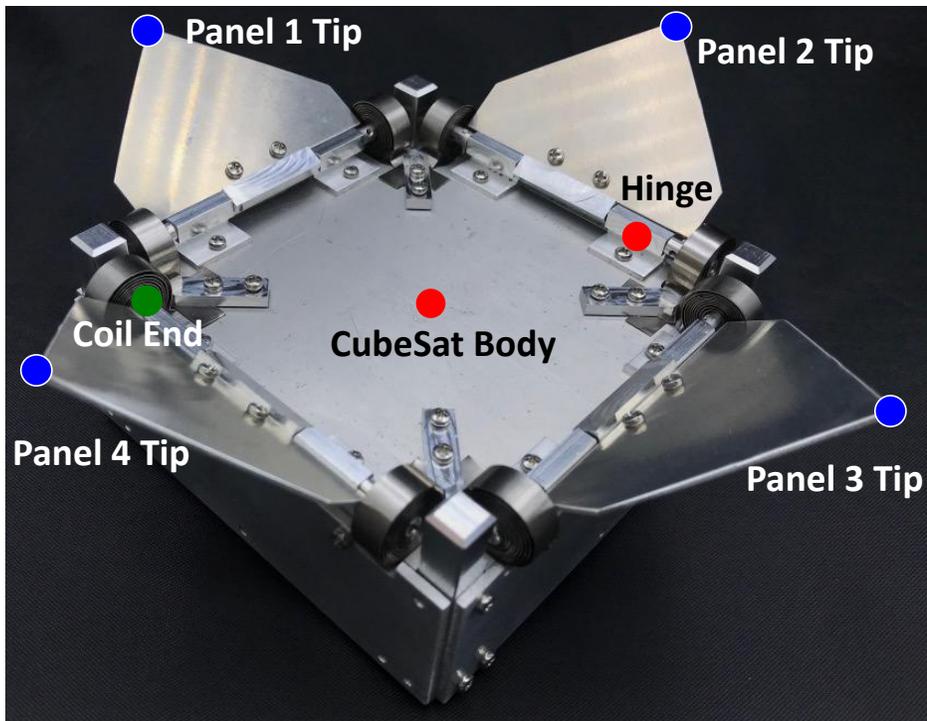


- Bimetallic coil actuation
 - Crest P675R
 - 4° of angular rotation per 1 °C (unloaded)
 - Temperature responsive
 - Intermediate positioning
 - Tunable actuation T
- CalPoly CubeSat design standard
- Sheldhal surface coating (149598)
- Contactless rotary magnetic encoders



CubeSat Development - Testing

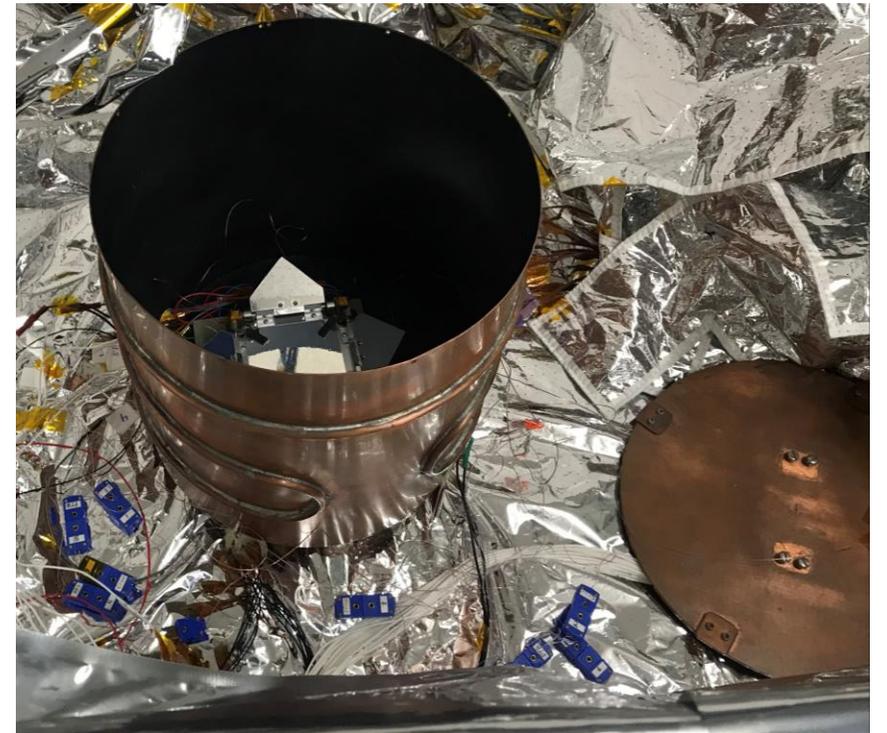
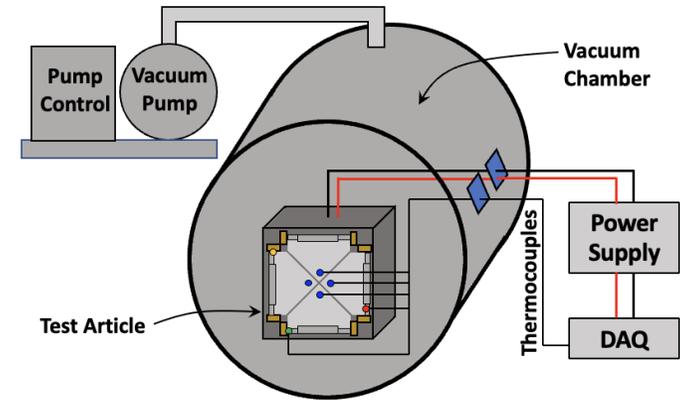
- Truncated CubeSat body
- Chamfered base contact
- Kapton heaters (red)



CubeSat Development - Testing

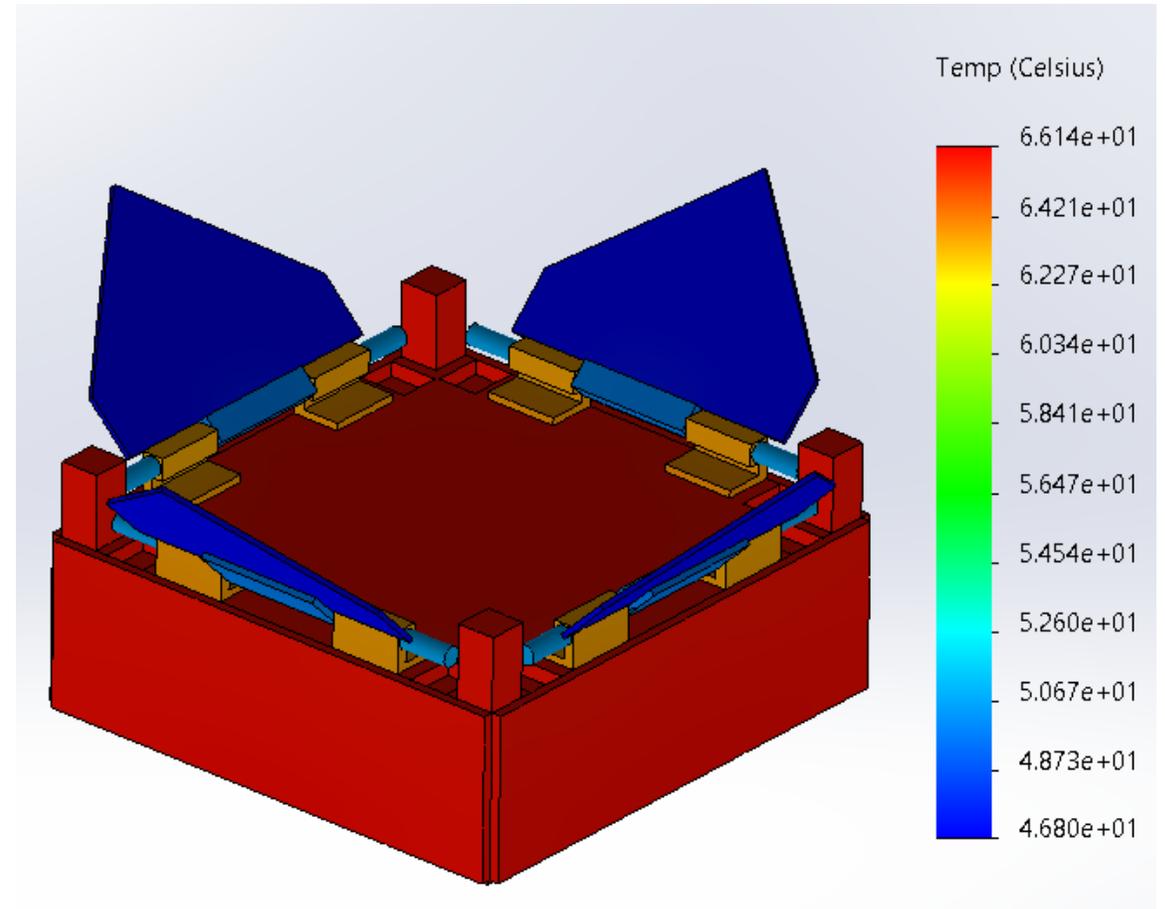
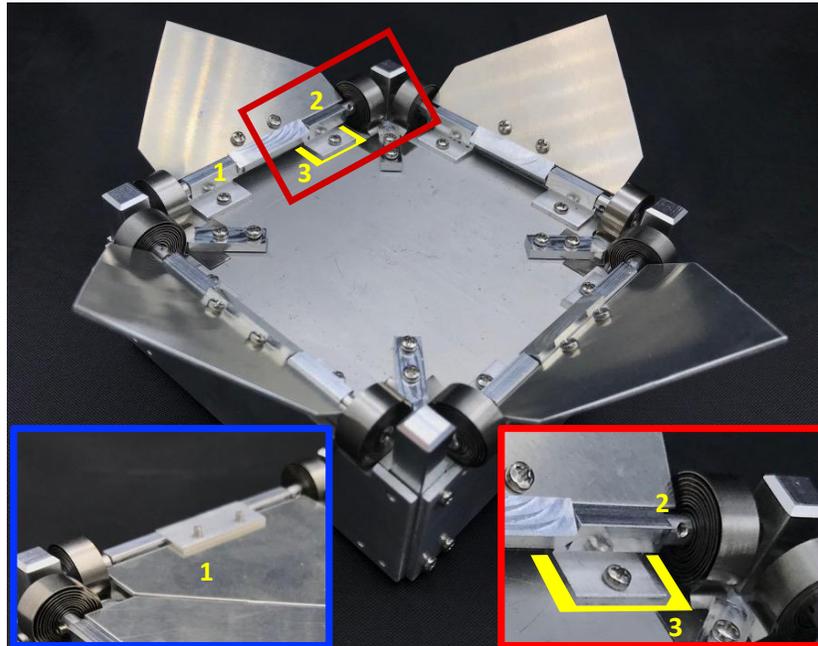
Vacuum chamber (JPL)

- Pressure: 10^{-6} Torr
- Temperature and power feedthroughs
- Test article on insulating G10
- Liquid N₂ shroud (83 K)



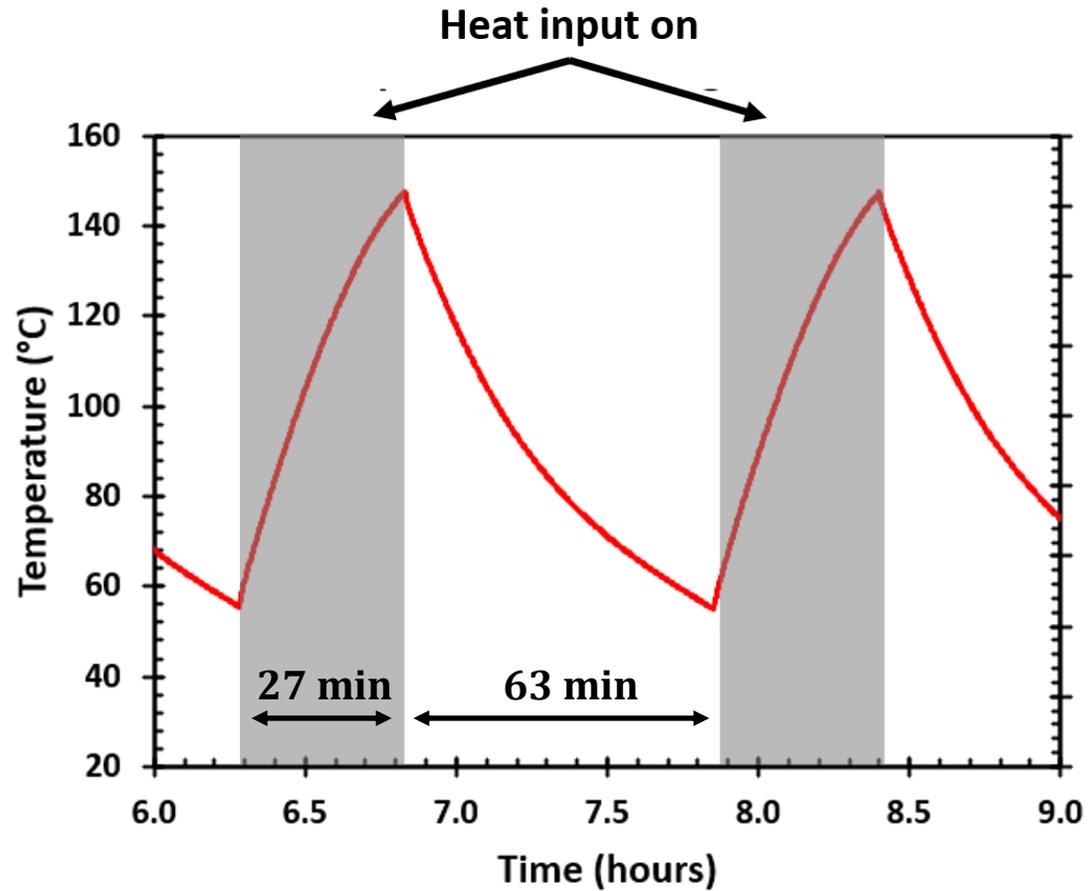
CubeSat Development - Model

- Fixed deployment angle (135°)
- Heating: 2.5 and 5 W (ambient T_{surr})
- Thermal resistance tuning
- Agreement $< 1\text{ }^{\circ}\text{C}$



CubeSat Development - Results

- 90 min orbit
- 30% duty cycle
- 35 W

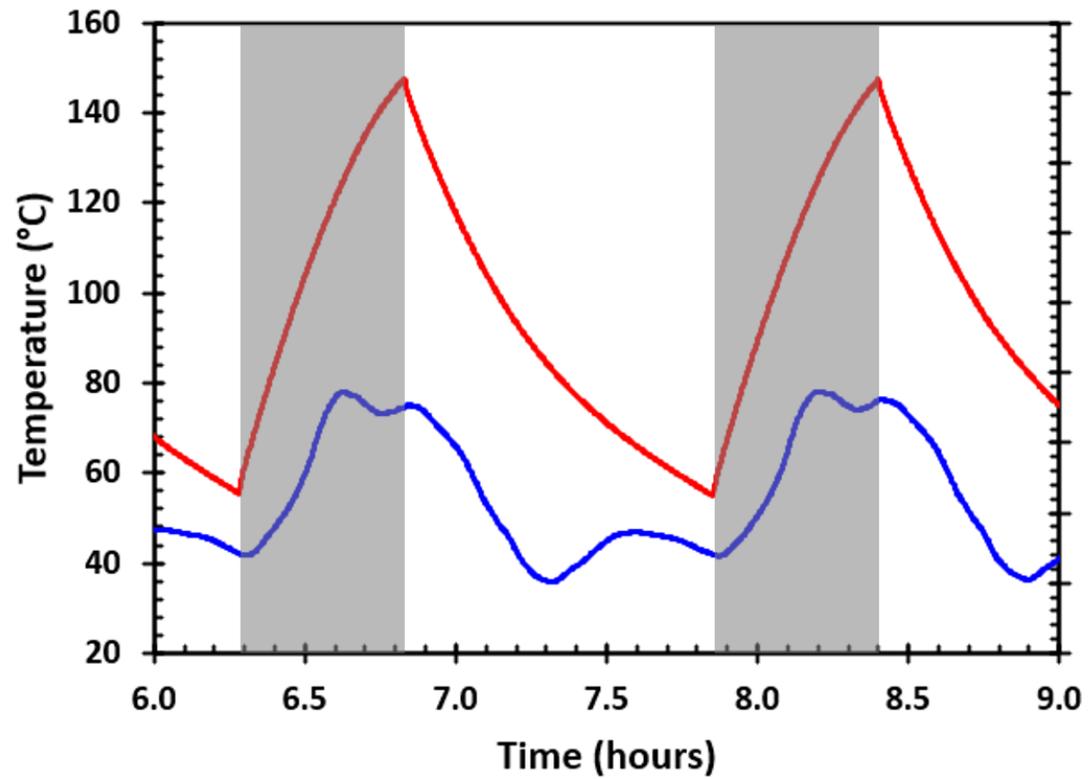


— CubeSat Body

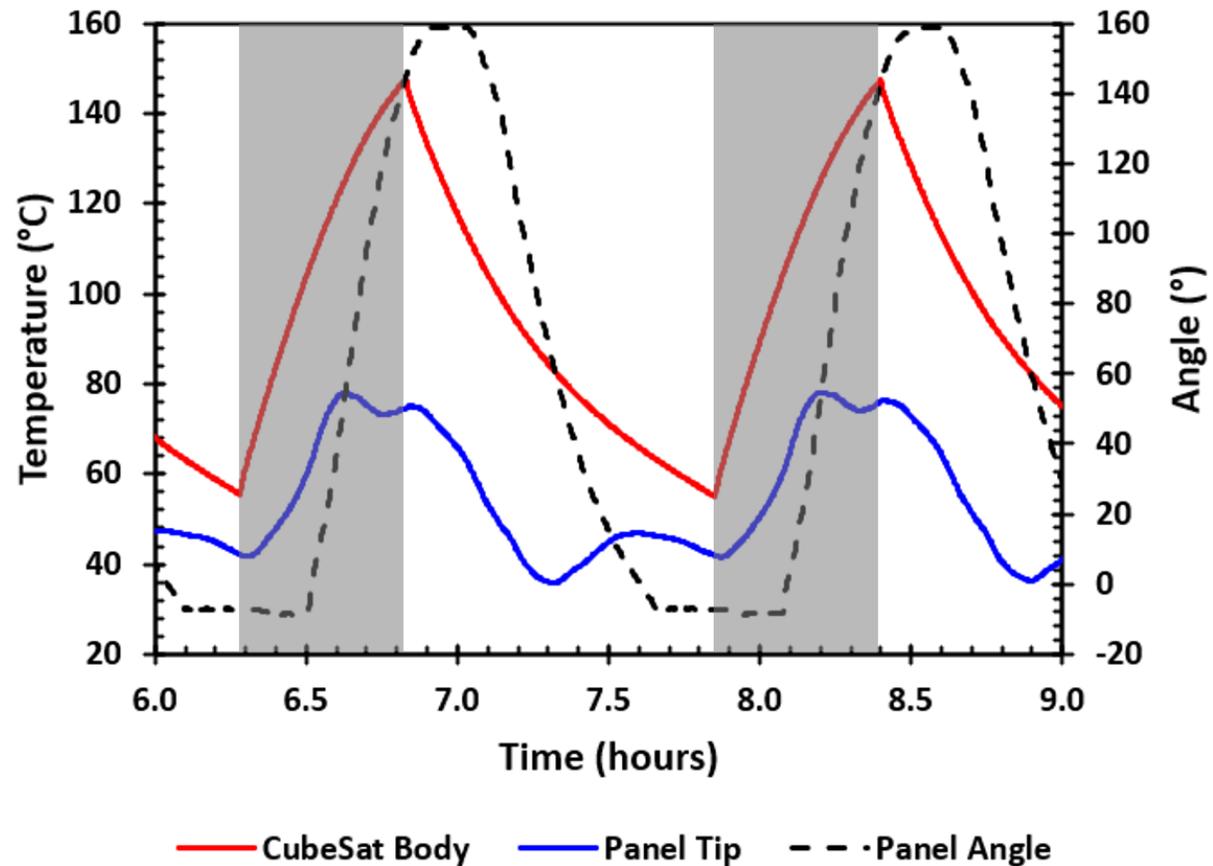


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CubeSat Development - Results

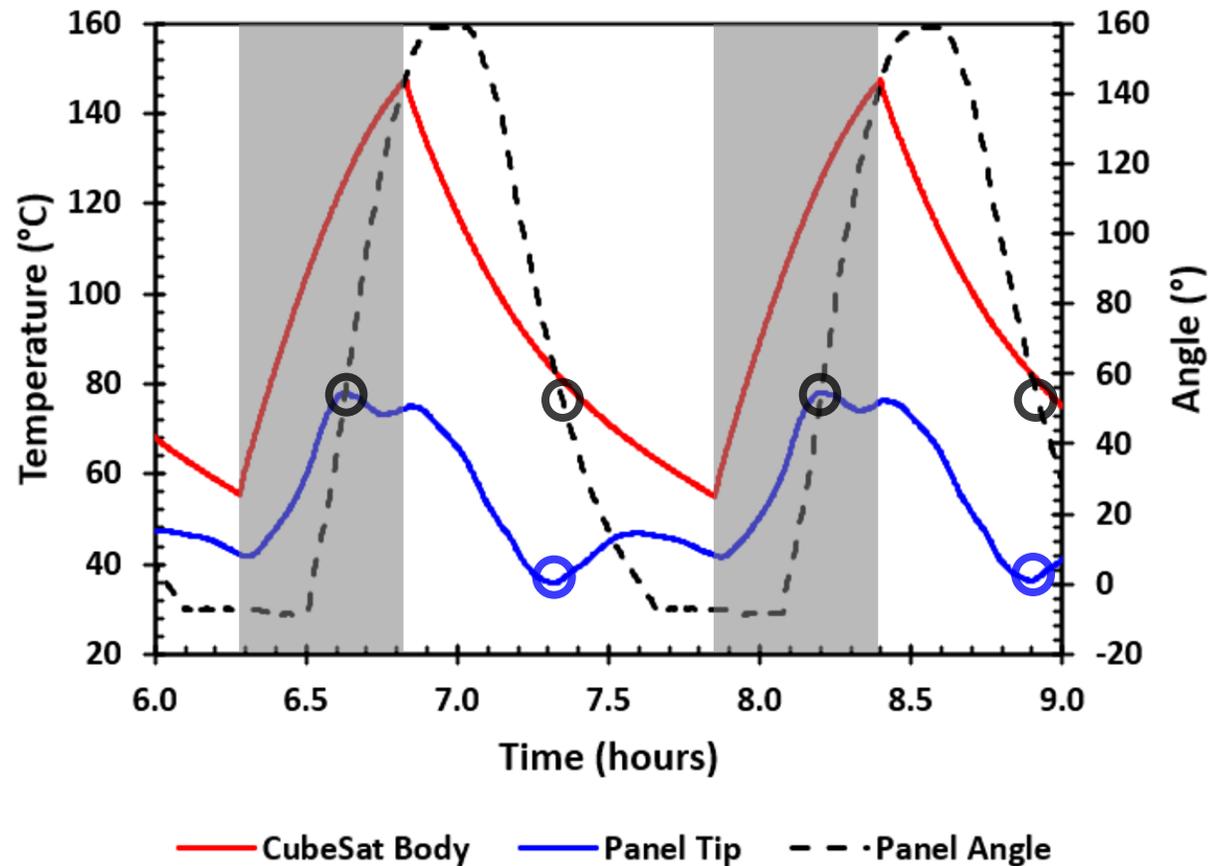


CubeSat Development - Results



CubeSat Development - Results

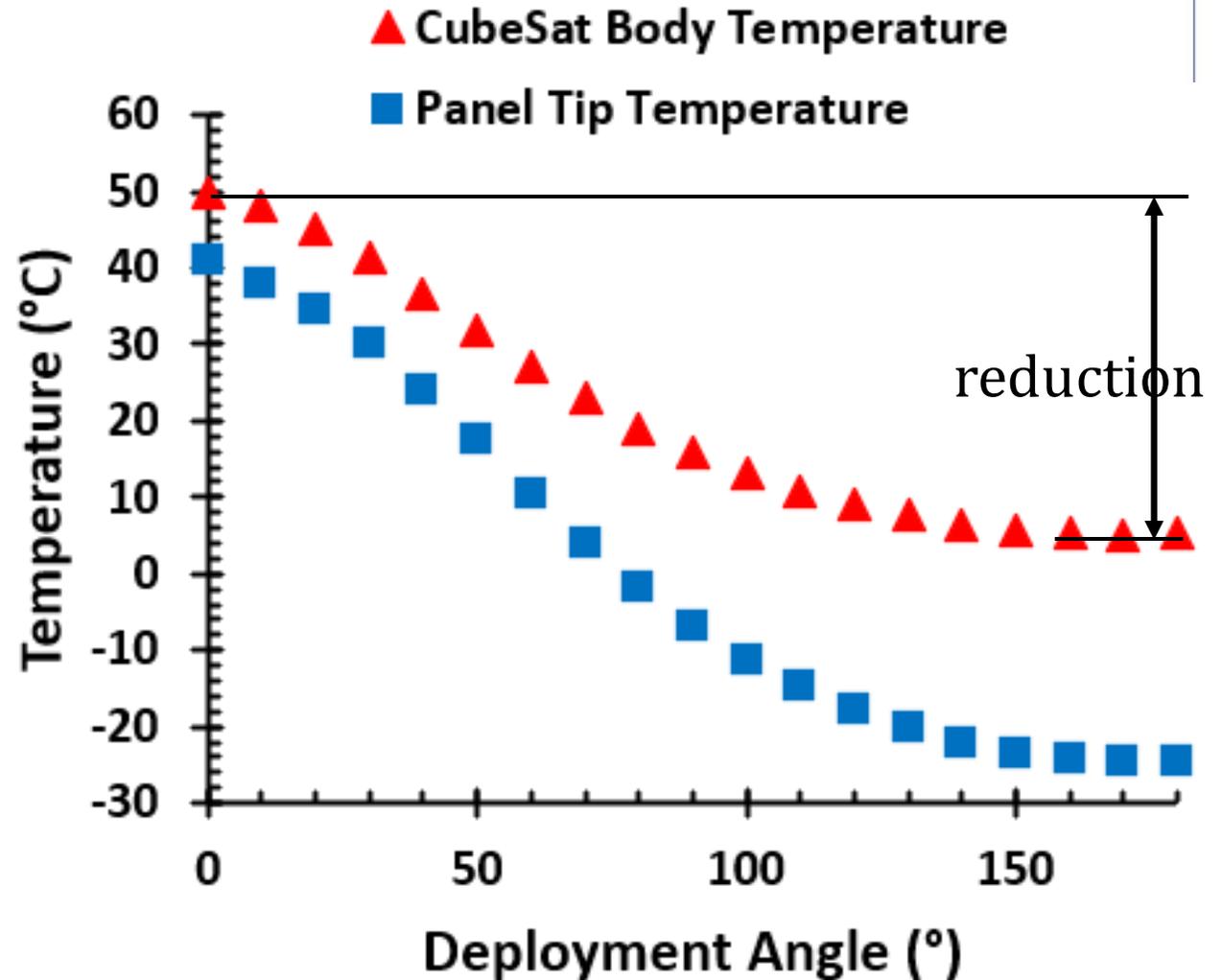
- Transition in heating behavior at 55°



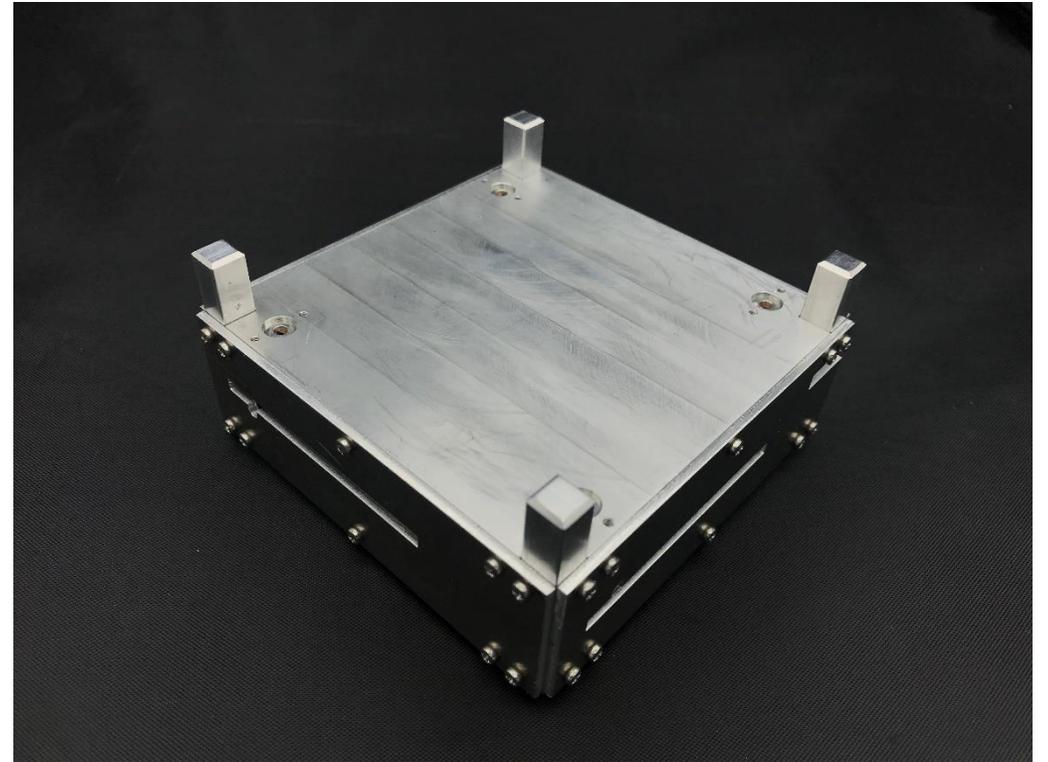
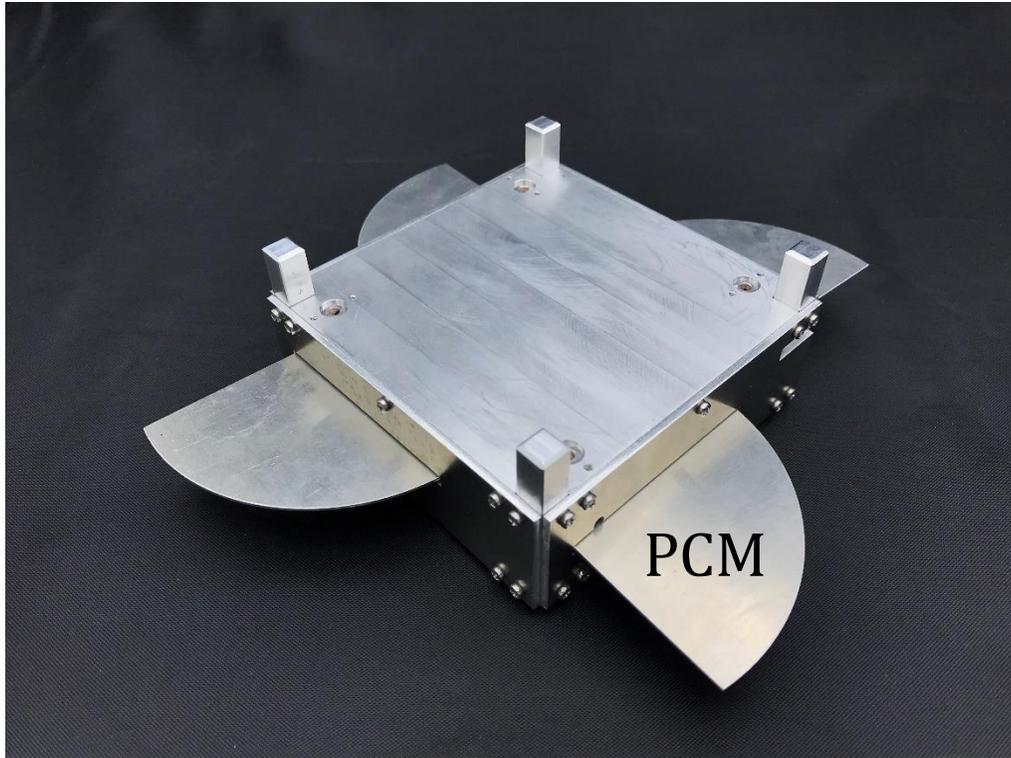
CubeSat Development - Results

- Turndown ratio = 5.4 (experimental)
 - Max heat loss 5.5 W at 180°
 - Min heat loss 1.0 W at 0°
- Temperature decrease (model)
 - Heat rate: 5 W
 - Evaluated over all deployment angles
 - 45 °C temperature reduction
 - 95% benefit by 135°

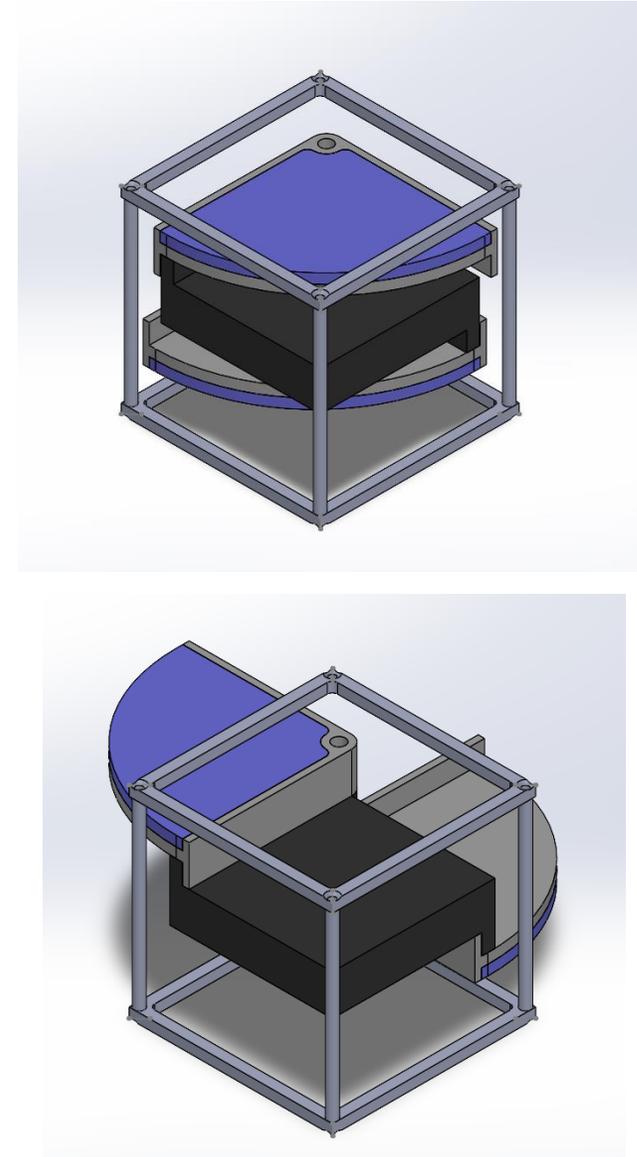
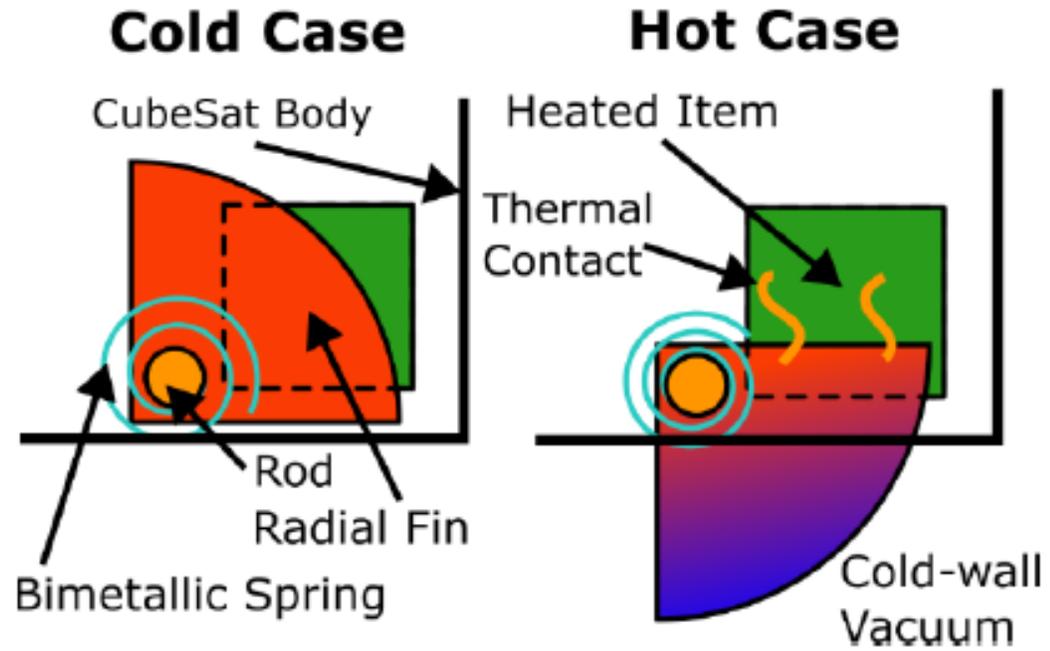
Effectiveness limited by heat transfer path to the radiator fins



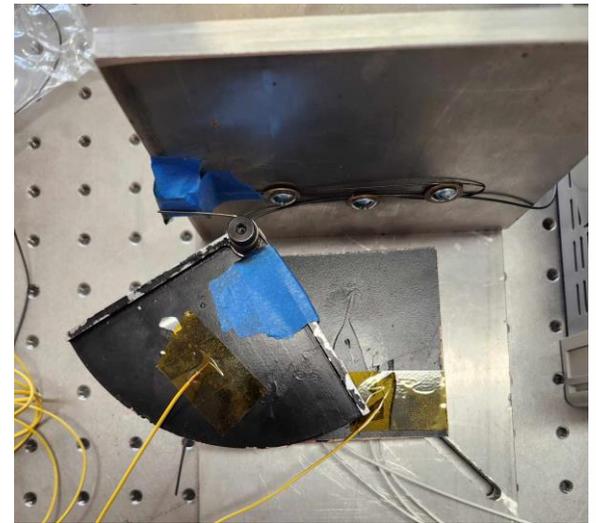
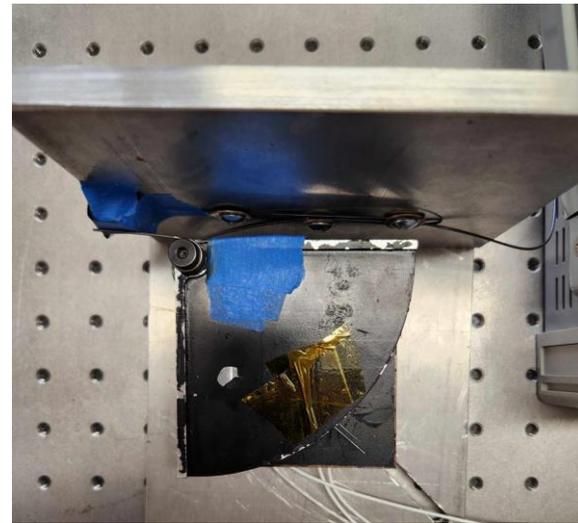
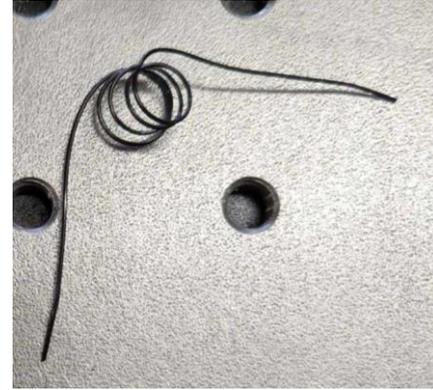
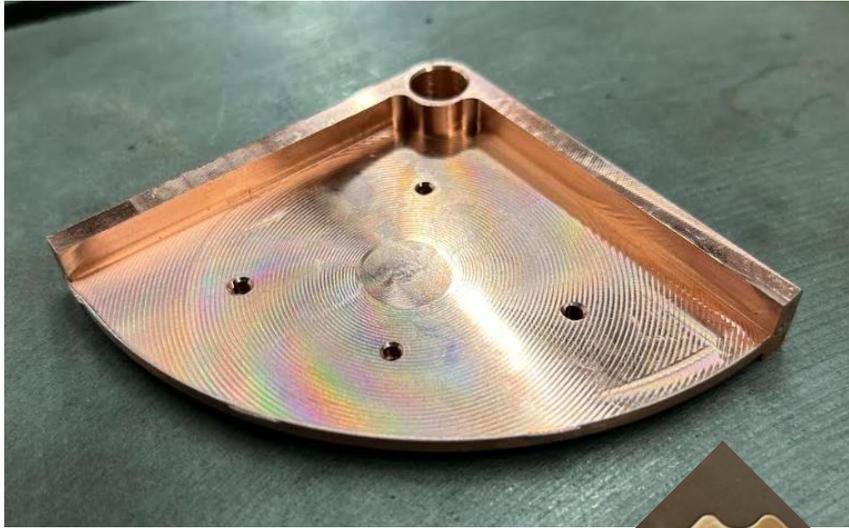
CubeSat Development - Prototype



CubeSat Development - Prototype



CubeSat Development - Prototype

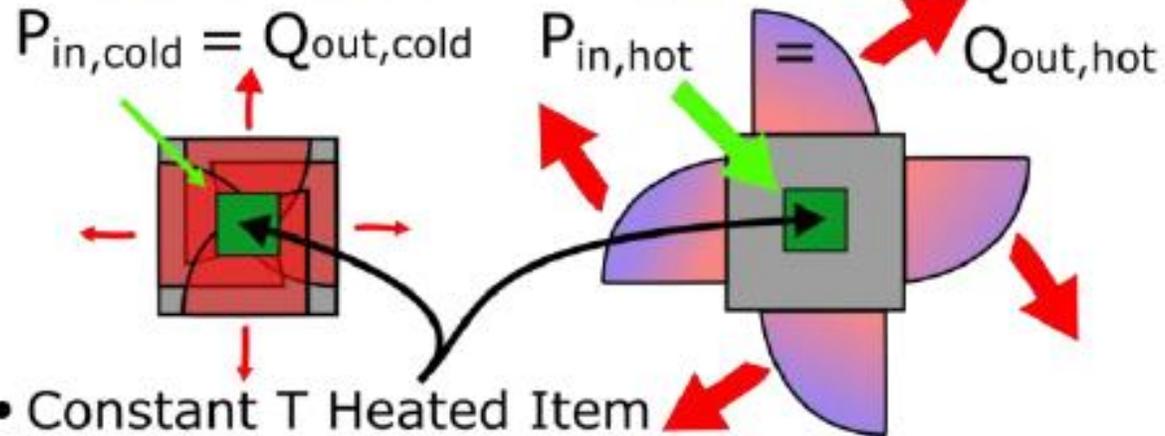


CubeSat Development - Test

Hot and Cold Steady State Test

Cold Case

Hot Case

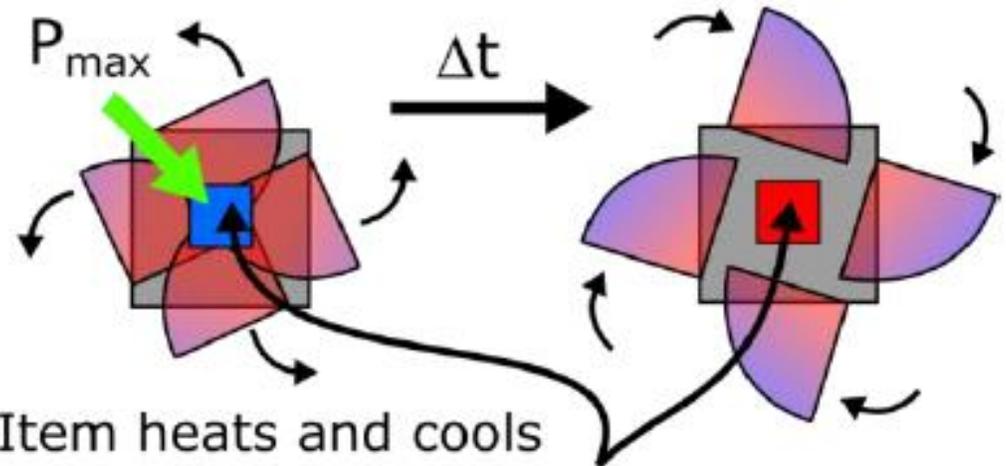


- Constant T Heated Item
- Fins constrained open or shut
- Measure P for Cold and Hot Cases

Transient Test

Power On

Power Off



- Item heats and cools
- Measure T variation of Heated Item

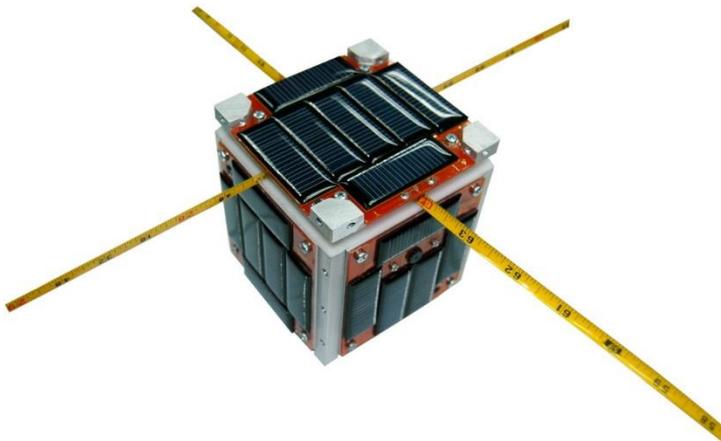


Demonstrate



Demonstrate – Flight Opportunity?

- Currently coordinating with Dr. Alex Rattner at Penn State to launch a demonstration platform hosting a variety of passive thermal control technologies.
- Possible platform – CubeSat, ISS, Varda Space Industries, etc.
- Targeting NASA Flight Opportunities and the CubeSat Launch Initiative for this work



Acknowledgements

- The Deployable PCM CubeSat work is currently funded by a NASA SmallSat Technology Partnership Grant (Grant Number: 80NSSC23M0235)



Questions?

FYI: Currently hiring PhD student to start in January 2025.
Please send me any interested applicants.



References and Image Credits

- [1] Nagano, H., Ohnishi, A., & Nagasaka, Y. (2011). Development of a lightweight deployable/stowable radiator for interplanetary exploration. *Applied Thermal Engineering*, 31(16), 3322–3331.
- [2] NASA. https://www.nasa.gov/mission_pages/station/structure/elements/radiators.html#.W-HbzZNKi70
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