TFAWS Passive Thermal Paper Session





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Frequency response measurements of an oscillating heat pipe using strain gauges

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Oscillating heat pipes



K. Odagiri et al., Appl. Therm. Eng. (2021)

- Lightweight
- Cheap
- Good manufacturability
- Excellent heat transport capabilities



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R. Wilcoxon et al., (SEMI-THERM) (2022)

Measuring the frequency of slug/plug oscillations









Measuring the frequency of slug/plug oscillations



Advantages and disadvantages of typical experimental techniques. Experimental Advantages Disadvantages procedure Straightforward Poor insight into the Temperature sensors placed on the outer installation. devices working behaviour. wall Visible light imaging Clear observation of the High cost of high-speed and inner fluid dynamics. high-resolution cameras, great expertise required especially for temperature measurements. The need for transparent inserts will additionally increase the complexity of the experimental set-up. Absent or poor outcomes regarding the inner thermo-dynamics. Neutron radiography Extremely high cost of Clear observation of the inner fluid dynamics, even peripheral facilities. without any transparent inserts. High cost of IR cameras. IR visualization Better description of the devices in terms of The inner fluid dynamics cannot be satisfactorily temperature distributions and operational behaviour. observed when dealing with opaque walls. Clear insight into the local Sensors may locally perturb Temperature and thermos-fluid dvnamic the fluid stream. Possible pressure sensors behaviour of the working fluid leaks through the inserted in the fluid fluid. added junctions. stream L. Pagliarini et al., Exp. Therm. Fluid Sci. (2023)



Measuring the frequency of slug/plug oscillations







Testbed for thermal and strain measurements





Notes on test parameters

- 34-turn closed-loop Al OHP filled with ammonia produced by ThermAvant
- Strain and temperature data acquired at 1000 S/s and 75 S/s rates, respectively, by NI DAQ modules and chassis
- Voltage data acquired by separate DAQ unit at ~0.3 Hz

Representative thermal resistance data



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Frequency response evolution with *Q*



Quantifying the frequency response





$$S(f) = \frac{a}{1 + \left(\frac{f}{c}\right)^{b}}$$

- *a* represents the upper plateau value of the curve, which reflects the characteristic signal-to-noise ratio
- b scales the slope of the curve at its midpoint, which corresponds to how fast the frequency response drops off
- *c* is frequency corresponding to the midpoint of the curve, and indicates a characteristic frequency

Quantifying the frequency response





$a, b, c, and R_{th}$ as functions of Q





$a, b, c, and R_{th}$ as functions of Q









Ref. 1: J.G. Monroe et al., *Exp. Therm. Fluid Sci.* (2017) Ref. 2: T. Daimaru & H. Nagai, *J. Thermophys. Heat Transf.* (2015) Ref. 3: Y. Yasuda et al., *Int. J. Heat Mass Transf.* (2022)



Intermittent and stable operating regimes



Intermittent spikes in the frequency response at low *Q*

Intermittent and stable operating regimes



Intermittent spikes in the frequency response at low *Q*

Stationary (temporally stable) response at high *Q*





Intermittent spikes in the frequency response at low *Q*

Stationary (temporally stable) response at high *Q*



Different behavior at the evaporator and condenser



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Different behavior at the evaporator and condenser



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Summary





- Identified three parameters to quantify frequency response in start up and stable operation ranges
 - a: characteristic signal-to-noise ratio
 - *b*: rate of frequency response decay
 - c: characteristic frequency
- Intermittency is reduced as operation transitions from the start-up (Q < 10 W) to the stable operating regime (Q > 10 W)
- Stronger strain signals indicating pressure fluctuations at the evaporator section may be indicative of nucleate boiling

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