

Experimental Characterization of Cryogenic Heat Pipe Evaporator for Lunar Ice Collection

M. Hasan, M. Valdiviez, M. Hernandez, M. Ahmad,
A. R. Choudhuri & M. M. Rahman

UTEP Aerospace Center

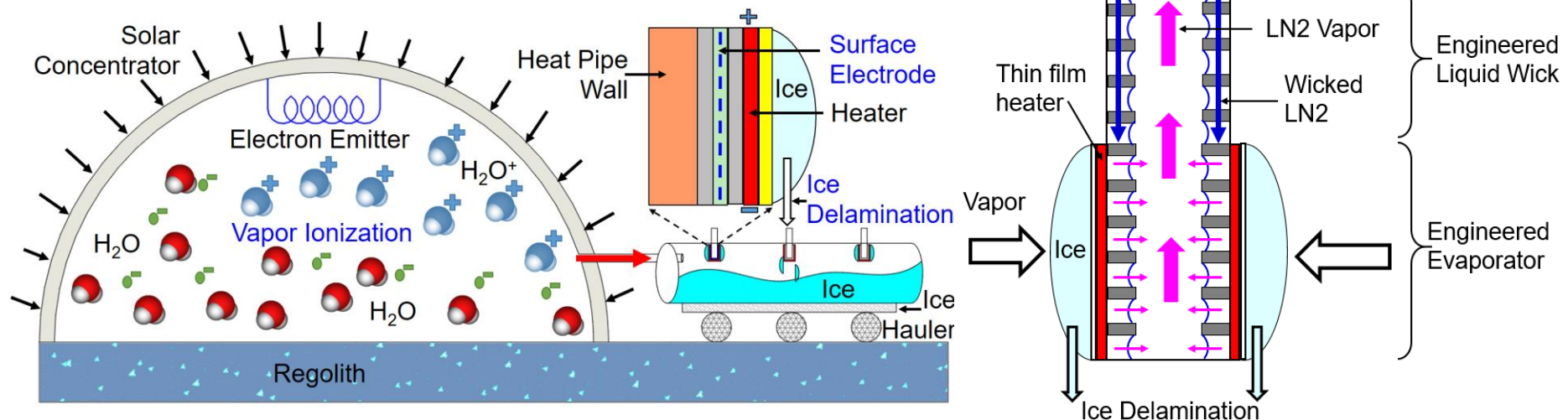


Presented By
M. Hernandez

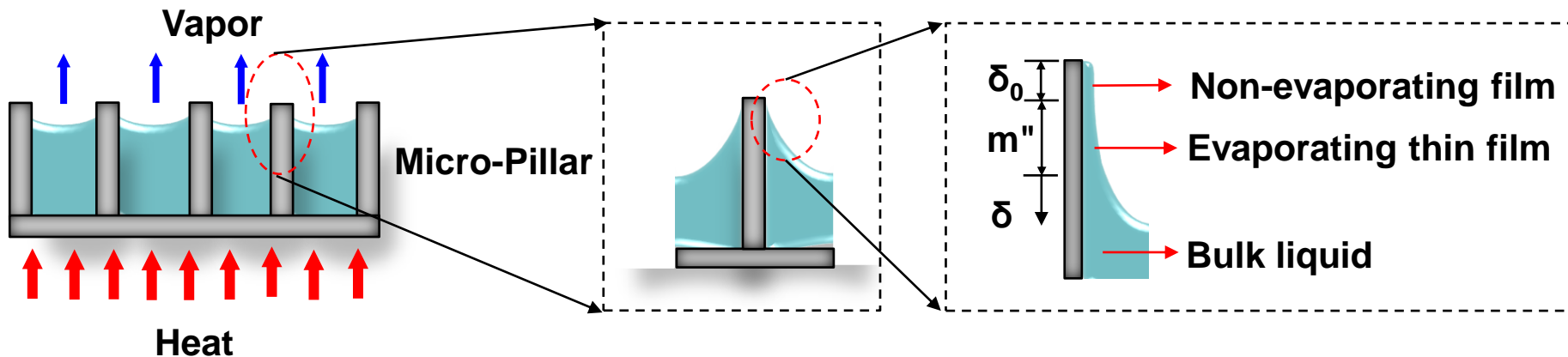
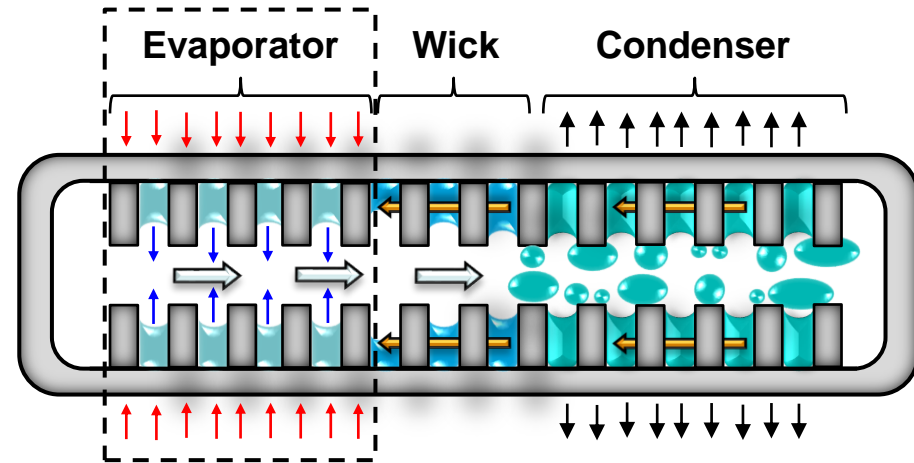
Thermal & Fluids Analysis Workshop
TFAWS 2023
August 21-25, 2023
NASA Goddard Space Flight Center
College Park, MD

Research Goal: To develop and demonstrate an advanced thermal mining technology of 1 kg ice collection prototype in approximately 11 hours from icy lunar regolith that integrates engineered

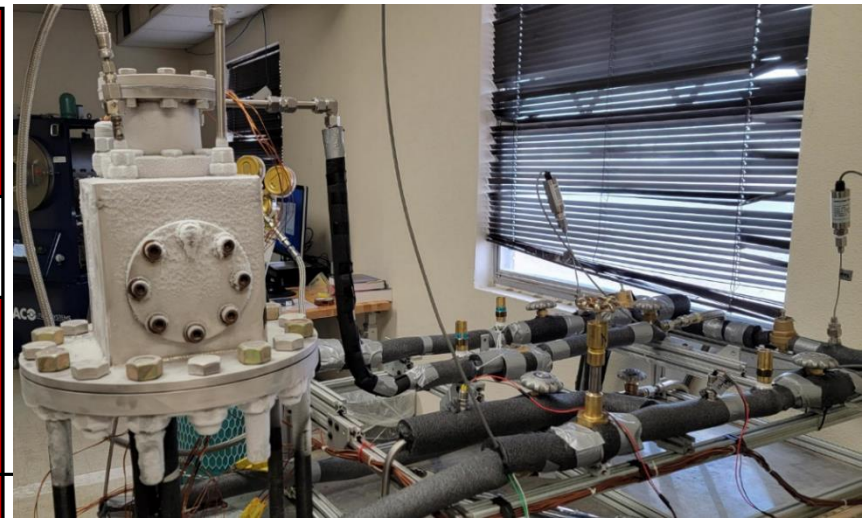
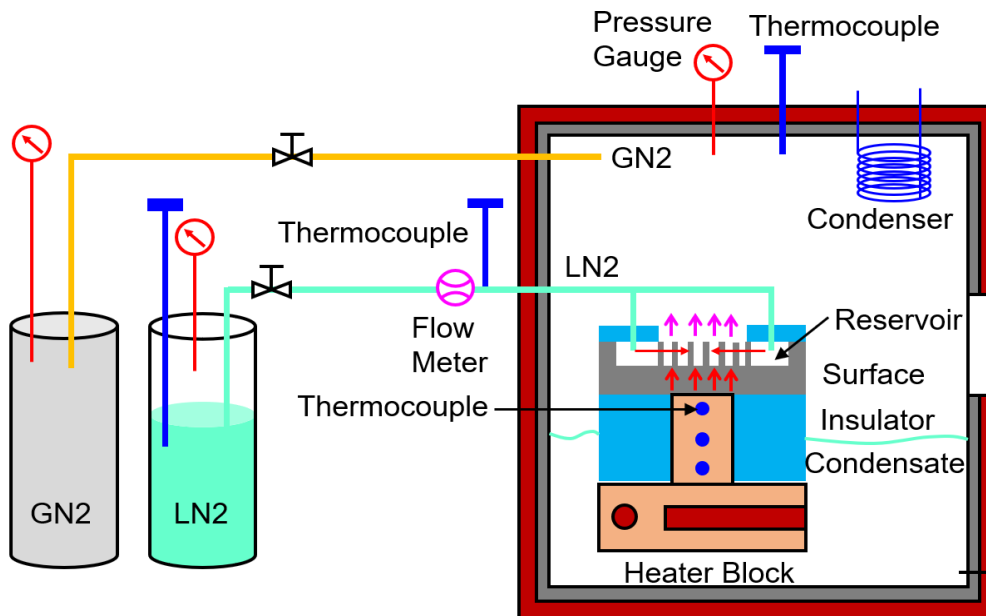
- i. Extraction (thermal drill and capture tent)
- ii. Vapor ionization and transportation
- iii. Re-collection of water vapor using pulsed delamination of ice on an engineered cryogenic heat pipe
- iv. System-level scale-up analysis of the proposed thermal mining technology



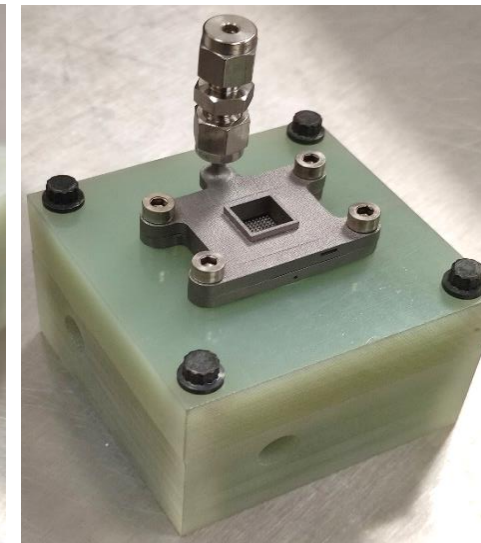
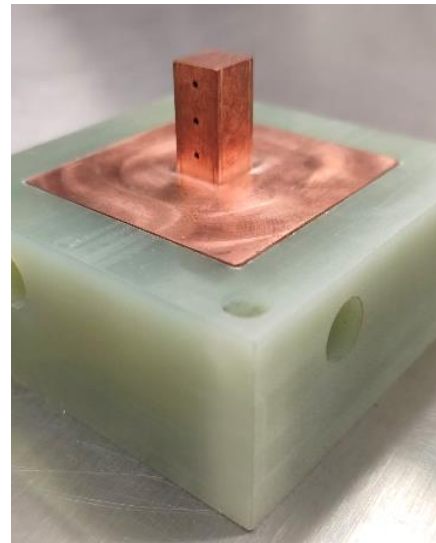
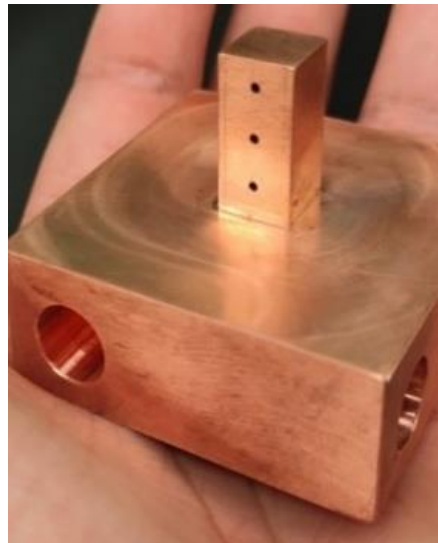
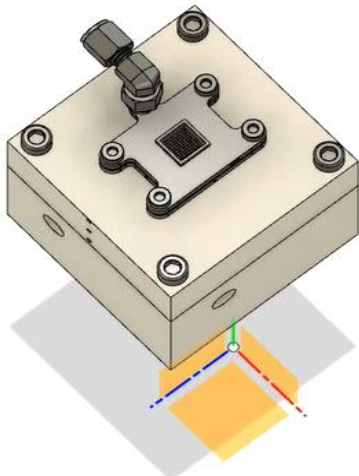
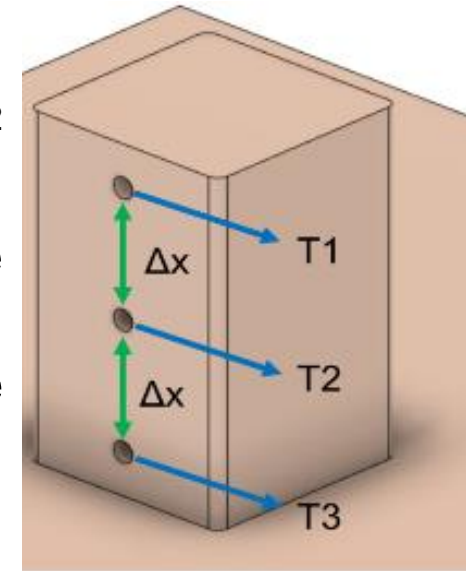
- New technique to enhance the heat pipe evaporator performance.
- During capillary rise, the extended meniscus forms non-evaporating, transition and intrinsic meniscus.
- Phase change occurs through transition region of extended meniscus of micro-pillar walls.
- Improves heat transfer by increasing evaporation area and decreasing conduction resistance.



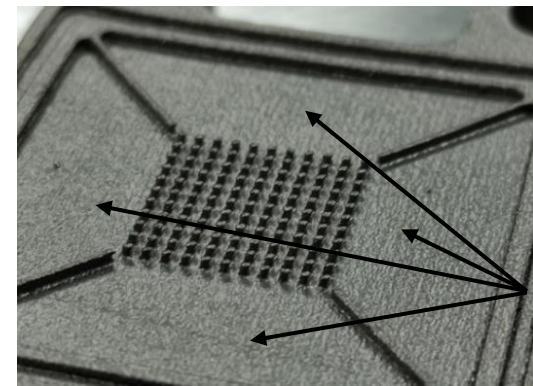
- Nitrogen gas (GN2) is used to pressurize the test chamber (14 bar).
- Liquid Nitrogen (LN2) is used to cool the chamber (110 K).
- LN2 is the working fluid for thin film evaporation.
- A copper condenser coil is used to achieve the operating cryogenic condition.
- One-dimensional heat conduction through copper heater block.
- All surfaces tested up to **dry-out** critical heat flux.



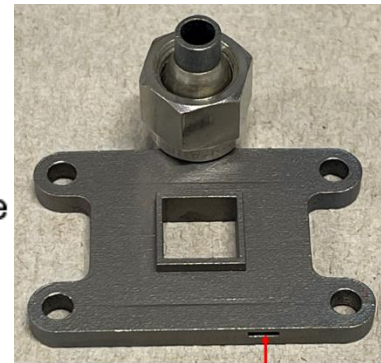
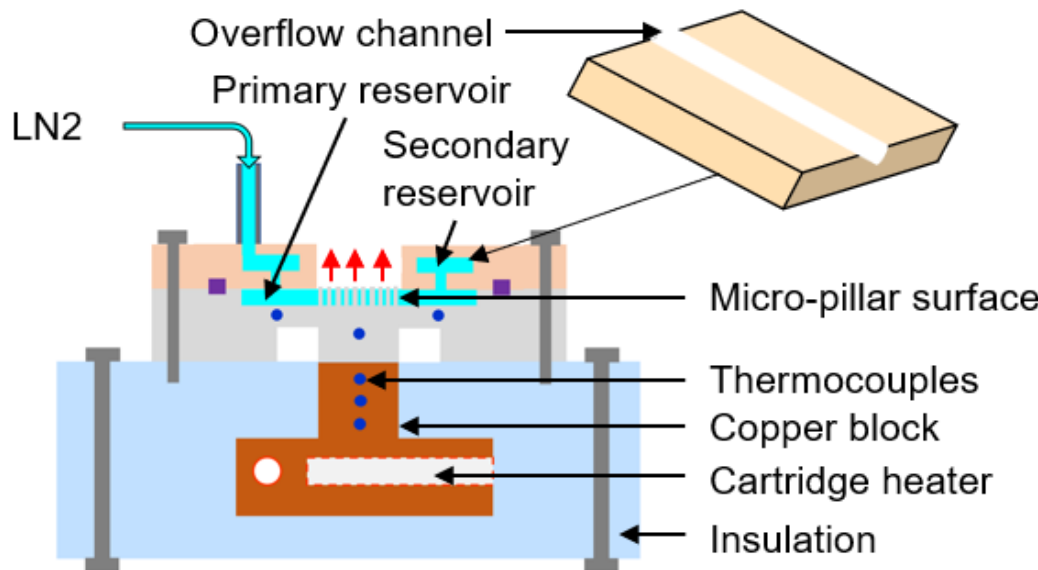
- A 50.8 mm x 50.8 mm x 38.1 mm copper heater block.
- The heater block has a 2.5 cm long neck and 1×1 cm² area to heat the test surfaces.
- Four cartridge heaters are used which can generate 1600 W.
- Three 1 mm holes for thermocouples to calculate the given heat flux.
- G10 insulation to ensure 1-D heat conduction.



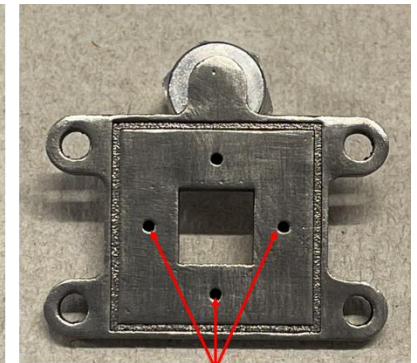
- Secondary reservoir is continuously filled with LN2 supply.
- Primary reservoir supplies LN2 to micro-pillars through capillary action.
- The drip holes in the secondary reservoir fills the primary reservoir through gravity.
- The excess LN2 flow is drained through an excess port in secondary reservoir ensuring the test procedure is not forced convection driven.



Primary reservoir



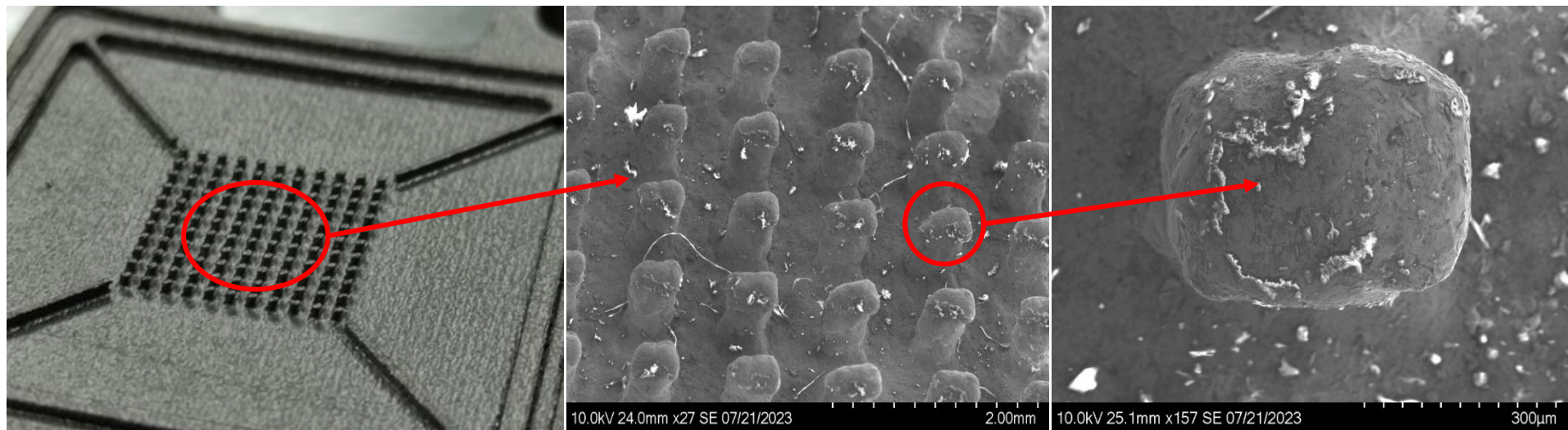
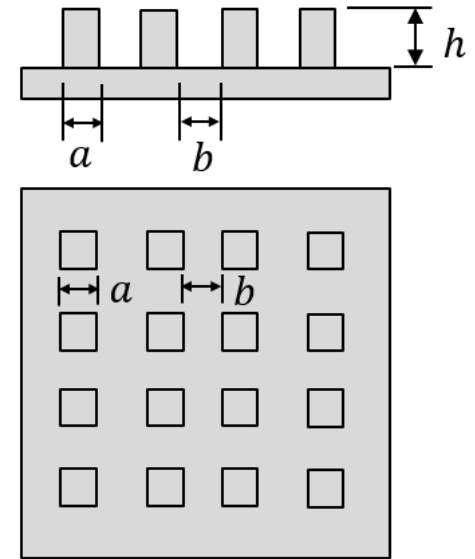
Excess Port



Secondary reservoir outlet

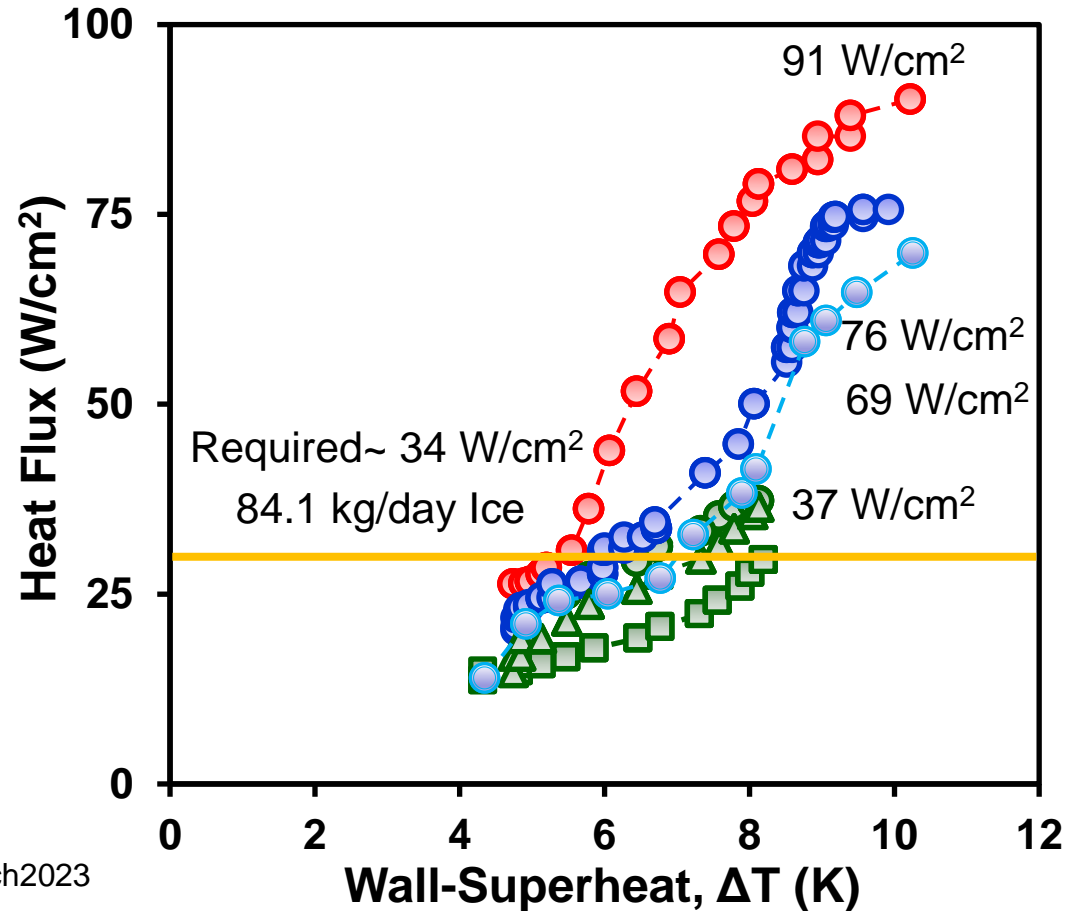
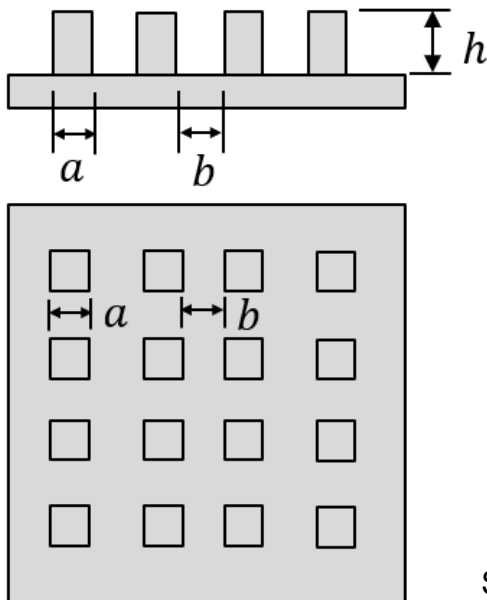
Additively Manufactured Top Cover

Material	Manufacturing Process	Width, a [μm]	Spacing, b [μm]	Height, h [μm]
Titanium Ti-64	Additive	400	500	600
Stainless Steel	CNC	400	500	600
Titanium Ti-64	Additive	400	500	800



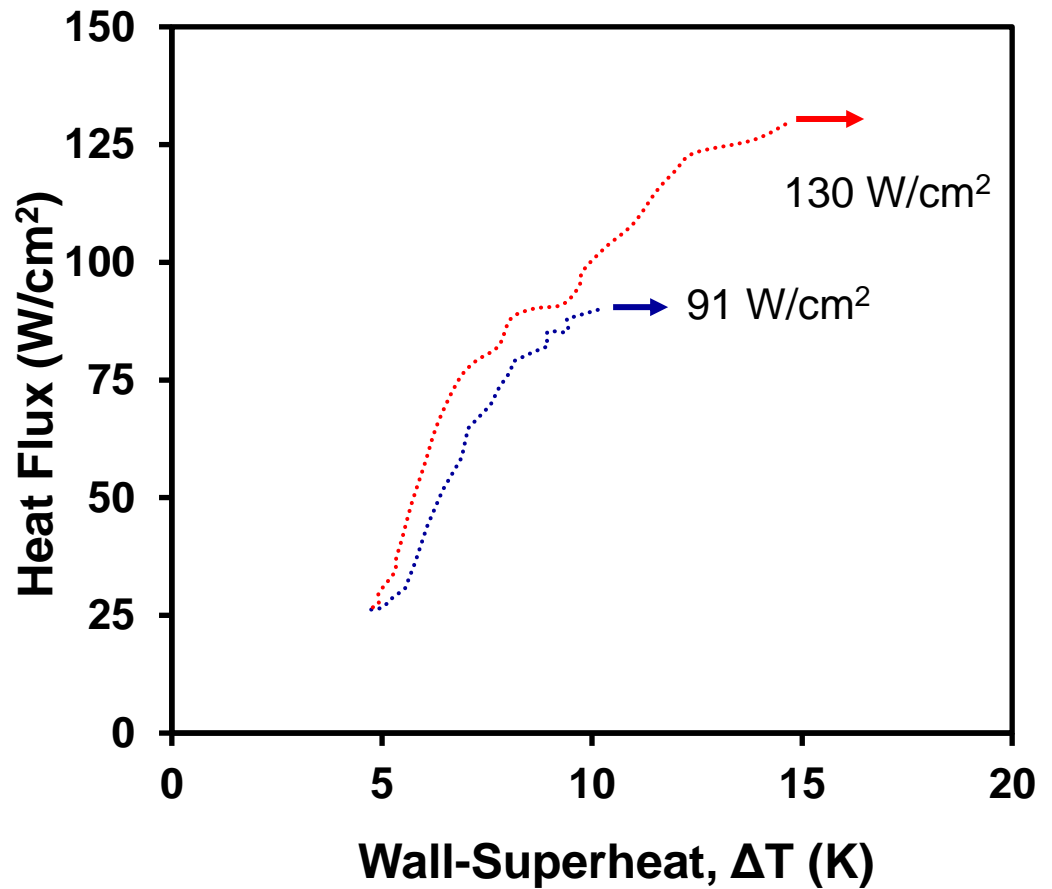
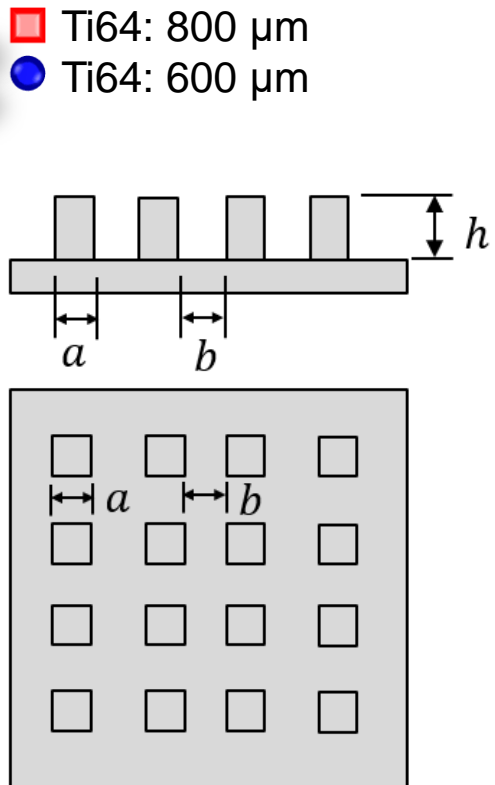
- More than 140% increase in dry-out for additively manufactured surfaces.
- Maximum dry-out heat flux $\sim 91 \text{ W/cm}^2$
- More than 167% higher capacity as compared to mission requirement.

- Ti64: 400 μm
- Ti64: 500 μm
- Ti64: 600 μm
- SS (CNC): 500 μm



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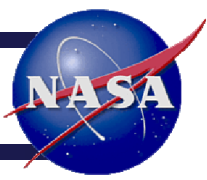
- Additively manufactured Ti-64 micro-structured evaporator.
- More than 40% increase in dry-out heat flux with increasing the height of the micro-pillars.
- Maximum dry-out heat flux $\sim 130 \text{ W/cm}^2$



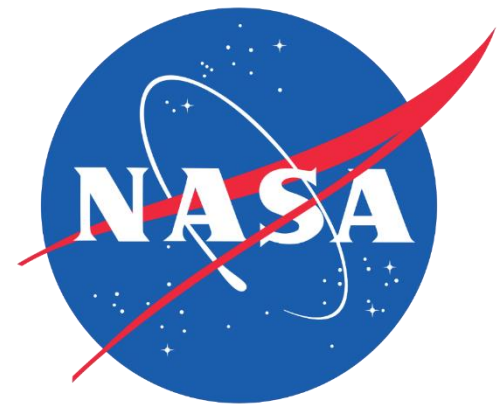
- Additively manufactured cryogenic heat pipe evaporators with micro-structured surfaces have been fabricated for enhanced heat collection from the water vapor re-capture process.
- From four different additively manufactured micro-structure samples, maximum dry-out heat flux was achieved as $\sim 130 \text{ W/cm}^2$ for $800 \mu\text{m}$ micro-pillar with wall-to-wall spacing of $500 \mu\text{m}$ and square pillar width of $400 \mu\text{m}$.
- For the same spacing, whenever the micro-pillar height was increased, the maximum dry-out heat flux was also increased by $\sim 50\%$.
- More than 200% increased heat flux has been achieved as compared to the lunar ice mining requirements.



Acknowledgement



The materials presented in this work is based upon the work supported by National Aeronautics and Space Administration (NASA) under Grant#80NSSC21K0768 and under NASA MIRO Agreement#NNH18ZHA008CMIROG6R.



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